### 1985

### STATE OF CONNECTICUT ANNUAL AIR QUALITY SUMMARY



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William A. O'Neill Governor

Leslie Carothers Commissioner

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### I. INTRODUCTION

The 1985 Air Quality Summary of Ambient Air Quality in Connecticut is a compilation of all air pollutant measurements made at the Department of Environmental Protection (DEP) air monitoring network sites.

### A. OVERVIEW OF AIR POLLUTANT CONCENTRATIONS IN CONNECTICUT

The assessment of ambient air quality in Connecticut is made by comparing the measured concentrations of a pollutant to each of two Federal air quality standards. The first is the primary standard which is established to protect public health with an adequate margin of safety. The second is the secondary standard which is established to protect plants and animals and to prevent economic damage. The specific air quality standards are listed in Table 1 along with the time constraints imposed on each.

The following section briefly describes the status of Connecticut's air quality for the year 1985. More detailed discussions of each of the six pollutants are provided in subsequent sections of this Air Quality Summary.

### 1. TOTAL SUSPENDED PARTICULATES (TSP)

Measured total suspended particulate (TSP) levels did not exceed the primary annual standard of 75  $\mu$ g/m<sup>3</sup> or the secondary annual standard of 60  $\mu$ g/m<sup>3</sup> in Connecticut during 1985. The primary 24-hour standard of 260  $\mu$ g/m<sup>3</sup> was not exceeded at any site in 1985. However, the secondary 24-hour standard of 150  $\mu$ g/m<sup>3</sup> was exceeded at two sites (see Table 2). Two exceedances of a standard are required at a particular site for the standard to be violated. No site recorded violations of any particulate standard in 1985.

In general, measured TSP levels in Connecticut were higher in 1985, in terms of annual average concentration values, than they were in 1984 (see Table 3).

### 2. SULFUR DIOXIDE $(SO_2)$

None of the air quality standards for sulfur dioxide were exceeded in Connecticut in 1985. Measured concentrations were below the 80  $\mu$ g/m<sup>3</sup> primary annual standard, the 365  $\mu$ g/m<sup>3</sup> primary 24-hour standard, and the 1300  $\mu$ g/m<sup>3</sup> secondary 3-hour standard.

The results of continuous  $SO_2$  monitoring indicate that sulfur dioxide levels in 1985 were not significantly different from those in 1984 (see Table 4). Temperature is an important factor in determining  $SO_2$  emissions. The lack of change in measured  $SO_2$  levels may have been due to the fact that, for coastal Connecticut, 1985 was not appreciably warmer than 1984. This can be shown by the number of "degree days" : a measure of heating requirement (see Tables 31 and 32). As the number of degree days increases, the amount of fuel that must be burned to heat buildings also increases. Consequently, as more fossil fuel is burned, the emissions of sulfur oxides are proportionately increased. There was only about a 1% increase in degree days for Connecticut as a whole from 1984 to 1985.

### 3. $OZONE(O_3)$

National Ambient Air Quality Standards (NAAQS) - On February 8, 1979, the U.S. Environmental Protection Agency (EPA) established an ambient air quality standard for ozone of 0.12 ppm for a one-hour average. That level is not to be exceeded more than once per year. Furthermore, in order to determine compliance with the 0.12 ppm ozone standard, EPA directs the states to record the number of daily exceedances of 0.12 ppm at a given monitoring site over a consecutive 3-year period and then calculate the average number of daily exceedances for this interval. If the resulting average value is less than or equal to 1.0, (that is, if the fourth highest daily value in a consecutive 3-year period is less than or equal to 0.12 ppm), the ozone standard is considered to be attained. The definition of the pollutant was also changed, along with the numerical value of the standard, partly because the instruments used to measure photochemical oxidants in the air really measure only ozone. Ozone is one of a group of chemicals which are formed photochemically in the air and are called photochemical oxidants. In the past, the two terms have often been used interchangeably. This 1985 Air Quality Summary uses the term "ozone" in conjunction with the new NAAQS to reflect the changes in both the numerical value of the NAAQS and the definition of the pollutant.

The primary 1-hour ozone standard was exceeded at all the DEP monitoring sites in 1985 (see Table 2).

The incidence of ozone levels in excess of the 1-hour 0.12 ppm ozone standard decreased significantly from 1984 to 1985 (see Tables 18 and 19). Most of this difference is attributable to the changes in meteorological factors which occur from year-to-year. The formation of ozone is facilitated by high temperatures and strong sunlight in the presence of hydrocarbons and oxides of nitrogen. The prevailing southwest wind transports hydrocarbons and nitrogen oxides generated in the New Jersey - New York City Metropolitan Area into Connecticut. Along the way, these chemicals react in the presence of strong sunlight, forming ozone. Consequently, the ozone levels across Connecticut are highest when the prevailing wind flow is out of the southwest (see Table 21). However, there are recorded exceedences of the NAAQS for ozone on non-southwest wind days. This suggests that pollution control programs currently being implemented in this state are needed to protect the public health of Connecticut's citizenry on days when Connecticut is responsible for its own pollution.

### 4. <u>NITROGEN DIOXIDE</u> (NO<sub>2</sub>)

The annual average NO<sub>2</sub> standard of 100  $\mu$ g/m<sup>3</sup> was not exceeded at any site in Connecticut in 1985.

### 5. CARBON MONOXIDE (CO)

The primary eight-hour standard of 9 ppm was exceeded at three of the five carbon monoxide monitoring sites in Connecticut during 1985 (see Table 2). The standard was exceeded owce three times at Stamford 020, six times at Hartford 017 and once at Bridgeport 004. Two exceedances at a particular site are required for a standard to be violated. This means that the eight-hour standard was violated at Stamford 020 and Hartford 017 in 1985. This was also the case in 1984. AT DETH HARTFORD 017 AND STAMPORD 020.

There were no violations of the primary one-hour standard of 35 ppm in 1985.

TABLE 1

## **ASSESSMENT OF AMBIENT AIR QUALITY**

|                                 |  |                   |                              | AMBIEN      | IT AIR QUA | LITY STAN       | DARDS  |
|---------------------------------|--|-------------------|------------------------------|-------------|------------|-----------------|--|
| POLLITANT                       | SAMPLING PERIOD                            | DATA REDITCTION   | CTATICTICAL BACE             | PRIM        | ARY        | SECON           | DARY   |
|                                 |  |                   |                              | pg/m3       | mqq        | µg/m³           | Mdd  |
|                                 |  |                   |                              |             |            |                 |  |
| Total Suspended                 | 24 Hours                                   |                   | Annual Geometric<br>Mean     | 75          |            | 60*             |  |
| Particulates                    | (every sixth day)                          | 24-mour Average   | 24-Hour Average <sup>3</sup> | 260         |            | 150             |  |
| Sulfur Oxides                   |  |                   | Annual Arithmetic<br>Mean    | 80          | 0.03       |                 |  |
| (measured as sulfur<br>dioxide) | Continuous <sup>2</sup>                    | 1-Hour Average    | 24-Hour Average <sup>3</sup> | 365         | 0.14       |                 |  |
|                                 |  |                   | 3-Hour Average <sup>3</sup>  |             |            | 1300            | <del>, 11. (* 11. (* 11. (* 11. (* 11. (* 11. (* 11. (* 11. (* 11. (* 11. (* 11. (* 11. (* 11. (* 11. (* 11. (* 11</del> |
| Nitrogen Dioxide                | Continuous <sup>2</sup>                    | 1-Hour Average    | Annual Arithmetic<br>Mean    | 100         | 0.05       | 100             | 0.05   |
| Ozone                           | Continuous <sup>2</sup>                    | 1-Hour Average    | 1-Hour Average <sup>4</sup>  | 235         | 0.12       | 235             | 0.12   |
| Lead                            | 24 Hours<br>(every sixth day) <sup>5</sup> | Monthly Composite | Weighted 3-Month<br>Average  | 1.5         |            | <u>ئ</u> .<br>ت |  |
| Carbon Monoxide                 | Continuous <sup>2</sup>                    | 1-Hour Average    | 8-Hour Average <sup>3</sup>  | 10**<br>10* | o          | 10**            | െ  |
|                                 |  | )                 | 1-Hour Average <sup>3</sup>  | 40**        | 35         | 40**            | 35   |

<sup>1</sup> EPA assessment criteria require at least 5 samples per calendar quarter and, if one month has no samples, then the other two months in that quarter must have at least two samples each.

<sup>2</sup> EPA assessment criteria require at least 75% of the possible data to compute a valid average.

<sup>3</sup> Not to be exceeded more than once per year.

<sup>4</sup> Not to be exceeded more than an average of once per year in three years.

<sup>5</sup> State of Connecticut assessment criteria require 75% of the possible data to compute a valid average.

 $^{\star}$  A guide to be used in assessing implementation plans to achieve the 24-hour standard.

\*\* Units are mg/m<sup>3</sup>.

TABLE 2

### **AIR QUALITY STANDARDS EXCEEDED IN CONNECTICUT IN 1985 BASED ON MEASURED CONCENTRATIONS**

|      |                                       |   |  |  |   | ULAIES                                     |
|------|---------------------------------------|---|--|--|---|--|
|      | Level Ex<br>1-H<br>Stano              | cceeding<br>lour<br>dard                  | Level Exce<br>8-Hou<br>Standa  | eding<br>r<br>rd                           | Level Ex<br>Secondar<br>Stan                            | ceeding<br>y 24-Hour<br>dard               |
| SITE | Highest<br>Observed<br>Level<br>(ppm) | Number<br>of Days<br>Standard<br>Exceeded | Highest<br>Observed Level<br>8-Hour / 1-Hour<br>(ppm)  | Number<br>of Times<br>Standard<br>Exceeded | Highest<br>Observed<br>Level<br>( <u>µg/m</u> <u>3)</u> | Number<br>of Times<br>Standard<br>Exceeded |
| 004  | ı                                     | ı   | by the second se | $\succ$                                    | ľ   | ı  |
| 123  | 0.196                                 | ব   | I  | ,<br>1                                     | ·   | •  |
| 123  | 0.149                                 | 4   | ı  | ı  | ł   | 1  |
| 003  | 0.149                                 | m   | ı  | ł  | ·   |  |
| 017  | 0.171                                 | 13  | ·  | ı  | ·   | 1  |
| 008  | 0.184                                 | თ   | ı  | ı  | ı   | ı  |
| 017  | ı                                     | ı   | 12.2   | 10<br>2 <b>9</b>                           | ł   | ı  |
| 002  | 0.204                                 | 7   | ı  | ı  | ı   | ı  |
| 007  | 0.219                                 | 10  | •  | ı  | ı   | ·  |
| 123  | 0.181                                 | 9   | •  | ı  | l   | ı  |
| 002  | ı                                     | ı   |  |  | 159   | <b>6</b>                                   |
| 001  | 0.166                                 | 4   |  | ı  | ı   | I  |
| 001  | ı                                     | ı   | ı  | ı  | 165   |  |
| 020  | I                                     | ı   | 10.2   | Z  | 1   | ı  |
| 007  | 0.189                                 | 13  | ·  | <b>1</b>                                   | ·   | ı  |

- : The pollutant is not monitored at the site.

(

### 6. <u>LEAD</u> (Pb)

The primary and secondary ambient air quality standard for lead is 1.5 µg/m<sup>3</sup>, maximum arithmetic mean averaged over three consecutive calendar months. As was the case in 1984, the lead standard was not exceeded at any site in Connecticut during 1985.

A downward trend in measured concentrations of lead has been observed since 1978. This trend is probably due to the decreasing use of leaded gasoline.

### B. TRENDS

Any attempt to assess statewide trends in air pollution levels must account for the tendency of local changes to obscure the statewide pattern. In order to reach some statistically valid conclusions concerning trends in pollutant levels in Connecticut, the DEP has applied a statistical test called a paired t test (referred to hereafter as the t test) to the annual average data for two pollutants. The t test has been applied to 1975-1985 total suspended particulate (TSP) data and to 1978-1985 continuous SO<sub>2</sub> data.

The t test is a parametric test which can ascertain statistically significant changes (increases or decreases) in the annual average pollutant concentrations at all the monitoring sites in Connecticut. The t test makes it possible to overcome the trend analysis problems which arise due to the changes in the number and location of monitoring sites from year-to-year, as well as problems associated with making equitable comparisons among sites. The annual mean pollutant concentrations for consecutive years are compared at each site; there is no inter-site comparison. Data for two consecutive years are required and the size of the change (increase or decrease) is noted. For example, if a high proportion of sites experienced an increase and/or if the magnitude of the increases at several sites is of much greater importance than the magnitude of the decreases at other sites, the t test will show that the increase was statistically significant for those two years.

The results of the *t* test for TSP and continuous SO2 data are presented in Tables 3 and 4, respectively. These analyses were performed only on data computed for sites at which the EPA's minimum sampling criteria were met. The years of data that were paired, the number of sites used, and the statewide average and standard deviation of the geometric mean pollutant concentrations at the sites are provided in the first four columns of each table. The statistical significance of any change in the statewide pollutant average is provided in the remaining columns. The significance of a change is indicated by an arrow for each confidence limit, and is also given numerically as the number of chances in 10,000 of not occurring under the heading "actual significance of change". For example, the statewide annual average for TSP decreased between 1977 and 1978 from 54.8 to 52.7. This change represented a significant decrease at the 95% confidence level, but it did not represent a significant change at the 99% confidence level. The "actual significance of change" is given as 0.0216, meaning that there are 216 chances in 10,000 that this measured decrease in TSP levels did not occur.

1. <u>TSP</u>

The results of the *t* test for TSP (see Table 3) show that total suspended particulate levels in Connecticut remained relatively constant from 1975 to 1977, decreased from 1977 to 1978, and remained unchanged from 1978 to 1979. Between 1979 and 1980 there was a significant drop in measured TSP levels. This has been attributed to the elimination of passive sampling error through the use of retractable lids on the hi-vol monitors. TSP levels alternately decreased and increased significantly from 1980 to 1984. From 1984 to 1985, TSP levels showed a significant increase at the 95% confidence level.

### TABLE 3

### TSP TRENDS: 1975 - 1985

(PAIRED t TEST)

|                 |                    |   |                                  | <u>S</u>                    | GNIFICA                      | <u>NCE LEVEL</u>                                    |
|-----------------|--------------------|---|----------------------------------|-----------------------------|------------------------------|---|
| PAIRED<br>YEARS | NUMBER<br>OF SITES | OF ANNUAL<br>GEOMETRIC<br>MEANS<br>(µg/m <sup>3</sup> ) | STANDARD<br>DEVIATION<br>(µg/m³) | TREN<br>95%<br><u>LEVEL</u> | ID AT<br>99%<br><u>LEVEL</u> | PROBABILITY<br>THAT CHANGE<br>IS NOT<br>SIGNIFICANT |
| 75<br>76        | 29<br>29           | 53.3<br>53.3  | 9.8<br>9.5                       | N.C.                        | N.C.                         | 0.9588  |
| 76<br>77        | 35<br>35           | 53.6<br>53.7  | 8.8<br>9.2                       | N.C.                        | N.C.                         | 0.8715  |
| 77<br>78        | 30<br>30           | 54.8<br>52.7  | 9.8<br>9.3                       | Ŷ                           | N.C.                         | 0.0216  |
| 78<br>79        | 32<br>32           | 51.4<br>49.9  | 12.1<br>12.5                     | N.C                         | N.C.                         | 0.1530  |
| 79<br>80        | 32<br>32           | 49.3<br>45.4  | 13.2<br>10.0                     | ¥                           | Ŷ                            | 0.0001  |
| 80<br>81        | 26<br>26           | 45.2<br>38.0  | 10.1<br>8.4                      | ↓                           | ¥                            | 0.0001  |
| 81<br>82        | 37<br>37           | 38.3<br>40.5  | 6.8<br>8.0                       | î                           | î                            | 0.0001  |
| 82<br>83        | 36<br>36           | 41.3<br>39.5  | 7.3<br>6.7                       | Ŷ                           | Ŷ                            | 0.0001  |
| 83<br>84        | 38<br>38           | 39.6<br>40.5  | 6.7<br>6.5                       | î                           | î                            | 0.0008  |
| 84<br>85        | 36<br>36           | 40.7<br>41.9  | 6.3<br>7.5                       | î                           | N.C.                         | 0.0141  |

Key to Symbols :  $\psi$  = Significant downward trend

f = Significant upward trend

N.C. = No significant change

### TABLE 4

### SO2 TRENDS FROM CONTINUOUS DATA: 1978 - 1985

### (PAIRED t TEST)

|                 |                    | AVERAGE   |  | S                           | GNIFICA                     | NCE LEVEL   |
|-----------------|--------------------|---|--|-----------------------------|-----------------------------|---|
| PAIRED<br>YEARS | NUMBER<br>OF SITES | OF ANNUAL<br>GEOMETRIC<br>MEANS<br>(µg/m <sup>3</sup> ) | STANDARD<br>DEVIATION<br>(µg/m <u>3)</u> | TREN<br>95%<br><u>LEVEL</u> | D AT<br>99%<br><u>LEVEL</u> | PROBABILITY<br>THAT CHANGE<br>IS NOT<br>SIGNIFICANT |
| 78<br>79        | 9<br>9             | 23.8<br>21.3  | 6.1<br>5.3                               | N.C                         | N.C.                        | 0.1238  |
| 79<br>80        | 10<br>10           | 21.8<br>19.8  | 4.5<br>5.2                               | Ŷ                           | N.C.                        | 0.0215  |
| 80<br>81        | 8<br>8             | 21.1<br>20.9  | 4.1<br>4.4                               | N.C.                        | N.C.                        | 0.9100  |
| 81<br>82        | 8                  | 20.9<br>21.0  | 4.4<br>4.5                               | N.C.                        | N.C.                        | 0.9522  |
| 82<br>83        | 8<br>8             | 20.0<br>18.1  | 5.0<br>5.1                               | Ŷ                           | Ŷ                           | 0.0002  |
| 83<br>84        | 8<br>8             | 18.1<br>18.2  | 5.1<br>4.5                               | N.C.                        | N.C.                        | 0.9237  |
| 84<br>85        | 15 14<br>15 14     | 16.4 16.3<br>16.5 16.7                                  | 4.4.4.5                                  | N.C.                        | N.C.                        | 0.6753<br>- <del>0.965</del> 4                      |

Key to Symbols : 🕴 = Significant downward trend

f = Significant upward trend

N.C. = No significant change

These trend analyses do not account for the uncertainty associated with the individual annual mean computed for each TSP site. Most TSP sampling is conducted only every sixth day, producing a maximum possible total of 61 samples per year. Therefore, the *t* test really compares year-to-year averages of the sampled concentrations, not actual annual averages. However, the every-sixth-day sampling schedule is believed to be sufficient to produce representative annual averages. The every-sixth-day schedule for TSP sampling began in 1971.

Significant changes in annual TSP levels can be caused by a number of things. Among these are simple changes of weather, particularly the wind; changes in annual fuel use associated with conservation efforts or heating demand; the frequency of precipitation events, which wash out particulates from the atmosphere; changes in average wind speed, since higher winds result in greater dilution of emissions; and a change in the frequency of southwesterly winds, which affect the amount of particulate matter transported into Connecticut from the New York City metropolitan area and from other sources of emissions located to the southwest.

Figure 1 shows the long-term trend of TSP concentrations in Connecticut in graphical form. The trend chart is based on data obtained from high volume sampling devices. High volume sampler data at a site are included only if there was a sufficient number of samples taken in a year to compute a valid annual geometric mean concentration.

### 2. <u>SO</u>2

Connecticut has been measuring ambient levels of sulfur dioxide since prior to the inception of the SO<sub>2</sub> standards in 1971. Several monitoring methods have been employed including bubblers, sulfation plates, and various types of continuous instruments. The bubblers became the EPA reference method, but unfortunately the field data have turned out to be very unreliable. The sulfation plates were in use for 15 years, but they do not measure SO<sub>2</sub> directly. Sulfation rate-derived SO<sub>2</sub> values were thought to be reliable, but recent information has cast doubt on their reliability. Continuous monitors presently yield reliable data, but this has not always been the case. The earliest continuous monitors (conductometric and coulometric) were subject to interference from many chemicals other than SO<sub>2</sub> and also had difficulties with quality control. Later generations of instruments (flame photometric and pulsed fluorescent) alleviated these problems, and there has been a corresponding increase in the reliability of the data, especially since 1978.

In order to perform a valid trend analysis, the data for the period of interest must be adequate, reliable and from similar sampling methods. Up until 1978, the only method which consistently fit these criteria was the sulfation plate. Between 1978 and 1982 there were approximately three times as much sulfation rate data as continuous SO<sub>2</sub> data and the former method was used for the purpose of analyzing SO<sub>2</sub> trends. However, recent information now indicates that sulfation rate-derived SO<sub>2</sub> values may not be as accurate as once thought. Sulfation rate data are dependent on relative humidity and wind speed -- being extremely sensitive to the latter -- and the precision of the data suffers even under uniform conditions. Furthermore, EPA has requested that DEP use continuous SO<sub>2</sub> data. The data are restricted to the period 1976-1985 because earlier data are judged not to be adequate or reliable. The results are summarized in Table 4 and Figure 2. Table 4 does not present a trend analysis for the period 1976-1977 or the period 1977-1978 because the number of monitors that operated for the duration of each period was 2 and 3, respectively -- too few to establish an accurate statewide trend.

In response to the skyrocketing prices of low sulfur fuels in the late 1970's, most states relaxed their sulfur-in-fuel requirements to the full extent the law allowed, creating considerable

FIGURE 1

(

## TOTAL SUSPENDED PARTICULATE MATTER TREND "PERCENT OF SITES WITHIN EACH RANGE"



PRIMARY ANNUAL STANDARD = 75 μg/m³ SECONDARY ANNUAL STANDARD = 60 μg/m³ FIGURE 2

# SULFUR DIOXIDE TREND FROM CONTINUOUS DATA "PERCENT OF SITES WITHIN EACH RANGE"



\* ANNUAL ARITHMETIC MEAN ( $\mu g/m^3$ )

PRIMARY ANNUAL STANDARD =  $80 \mu g/m^3$ 

pressure on Connecticut to follow suit. This caused Connecticut to reevaluate its philosophy for controlling sulfur oxide emissions in 1981. To meet the challenge of increased costs of fuel in the economy, DEP restructured its air pollution control requirements for fuel burning sources. Under this new "three-pronged" program Connecticut's businesses and industries are (1) now allowed (effective November 1981) to burn a less expensive grade of oil with a higher sulfur content -- one percent (1.0%) sulfur oil, and (2) allowed to burn higher sulfur content oil in exchange for reductions in energy use. The third aspect of the program is the repeal of the 24-hour secondary air quality standard for sulfur oxides.

This action increased statewide allowable sulfur oxide emissions by almost 60%. (Sulfur oxide emissions were not doubled by going from 0.5% to 1.0% sulfur-in-fuel since residential fuel users, which account for almost one-third of annual statewide sulfur oxide emissions, use distillate fuel oil with a sulfur content of less than 0.5%.) One would expect measured  $SO_2$  levels to increase in 1982 and subsequent years, as compared to 1981, due to the use of 1.0% sulfur oil. However, no significant trend was apparent in 1982; and in 1983  $SO_2$  levels actually declined (see Table 4). This may be attributable to the year-to-year fluctuations in meteorology or the decreased fuel use caused by the increased price of this energy source.

The long-term trend of SO<sub>2</sub> concentrations is shown in graphical form in Figure 2. An improvement in SO<sub>2</sub> levels is demonstrated by the decrease over time of concentrations in excess of 40  $\mu$ g/m<sup>3</sup>. Table 4 shows the year-to-year trend in ambient SO<sub>2</sub> levels. Decreases in SO<sub>2</sub> concentrations from 1979 to 1980 and from 1982 to 1983 are evident.

Continuous  $SO_2$  monitors were operated each year at five (5) sites between 1980 and 1985. Based on measurements at these five (5) locations, mean  $SO_2$  levels are depicted in Figures 2A and 2B. Figure 2A shows  $SO_2$  levels clearly decreasing at the Bridgeport, Danbury and Hartford sites. Figure 2B shows the average of the mean  $SO_2$  concentrations for all the sites steadily decreasing over the 5-year period. Figure 2C is a linear regression analysis of this data which also shows a downward trend in  $SO_2$  levels since 1980. Using the data presented in Figure 2B, Figure 2D shows the three-year running average of the mean  $SO_2$  concentrations. Three-year running averages tend to smooth out the year-to-year effects of meteorology on pollutant levels. Like Figures 2A, 2B and 2C, Figure 2D illustrates again that  $SO_2$  levels appear to be decreasing. This long term trend analysis also demonstrates that  $SO_2$  levels are declining even though fuel burning sources have been allowed to use 1% sulfur oil since 1982.

### C. AIR MONITORING NETWORK

A computerized Air Monitoring Network consisting of an IBM System 7 computer and numerous telemetered monitoring sites has operated in Connecticut for several years. In 1985, this data acquisition system was modernized by installing new data loggers at the monitoring sites and replacing the dedicated IBM System 7 computer with a non-dedicated Data General Eclipse MV/10000 computer. This essentially improved both data accuracy and data capture. As many as 12 measurement parameters are transmitted from a site via telephone lines to the Data General unit located in the DEP Hartford office. The data are then compiled twice daily into 24-hour summaries. The telemetered sites are located in the towns of Bridgeport, Danbury, East Hartford, East Haven, Enfield, Greenwich, Groton, Hartford, Madison, Middletown, Milford, New Britain, New Haven, Norwalk, Preston, Stafford, Stamford, Stratford and Waterbury.

Continuously measured parameters include the pollutants sulfur dioxide, particulates (measured as the coefficient of haze), carbon monoxide, nitrogen dioxide and ozone. Meteorological data consists of wind speed and direction, wind horizontal sigma, temperature, dew point, precipitation, barometric pressure and solar radiation (insolation).

FIGURE 2A

ANNUAL GEOMETRIC MEAN CONCENTRATIONS OF SO2 (PPB) FOR 1980-1985



### **FIGURE 2B**

### THE AVERAGE OF THE ANNUAL GEOMETRIC MEAN SO2 CONCENTRATIONS AT FIVE CONCURRENTLY OPERATING SITES

### SO<sub>2</sub> CONCENTRATION (PPB)



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FIGURE 2C

## TREND OF THE ANNUAL GEOMETRIC MEAN SO2 CONCENTRATIONS AT FIVE CONCURRENTLY OPERATING SITES FOR 1980-1985





### **FIGURE 2D**

### THREE-YEAR RUNNING AVERAGES OF THE ANNUAL GEOMETRIC MEAN SO2 CONCENTRATIONS AT FIVE CONCURRENTLY OPERATING SITES

### SO<sub>2</sub> CONCENTRATION (PPB)



The real-time capabilities of the Data General telemetry network have enabled the Air Monitoring Unit to report the Pollutant Standards Index for a number of towns on a daily basis while continuously keeping a close watch for high pollution levels which may occur during adverse weather conditions.

The complete monitoring network used in 1985 consisted of:

- 40 Total suspended particulate hi-vol sites
- 2 Total suspended particulate lo-vol sites
- 15 Lead hi-vol sites
- 7 Lead lo-vol sites
- 19 Sulfur dioxide sites
- 10 Ozone sites
- 3 Nitrogen dioxide sites
- 5 Carbon monoxide sites

A complete description of all permanent air monitoring sites in Connecticut operated by DEP in 1985 is available from the Department of Environmental Protection, Air Compliance Unit, Monitoring Section, State Office Building, Hartford, Connecticut, 06106.

### D. POLLUTANT STANDARDS INDEX

The Pollutant Standards Index (PSI) is a daily air quality index recommended for common use in state and local agencies by the U.S. Environmental Protection Agency. Starting on November 15, 1976, Connecticut began reporting the PSI on a 7-day basis, but is currently reporting the PSI on a 5-day basis. The PSI incorporates three pollutants : sulfur dioxide, total suspended particulates and ozone. The index converts each air pollutant concentration into a normalized number where the National Ambient Air Quality Standard for each pollutant corresponds to PSI = 100 and the Significant Harm Level corresponds to PSI = 500.

Figure 3 shows the breakdown of index values for the commonly reported pollutants (TSP, SO<sub>2</sub>, and O<sub>3</sub>) in Connecticut. For the winter of 1985, Connecticut reported the total suspended particulate PSI for the towns of Ansonia, Bridgeport, Danbury, Greenwich, Groton, Hartford, Milford, New Britain, New Haven, Norwalk, Norwich, Stamford, Stratford, Wallingford, and Waterbury; and reported the sulfur dioxide PSI for the towns of Bridgeport, Danbury, East Haven, Greenwich, Groton, Hartford, Milford, New Britain, New Haven, Norwalk, Preston, Stamford, and Waterbury. For the summer, the ozone PSI was reported for the towns of Bridgeport, Danbury, East Hartford, Greenwich, Groton, Madison, Middletown, New Haven, Stafford, and Stratford. Each day ,the pollutant with the highest PSI value of all the pollutants being monitored is reported for each town along with the dimensionless PSI number and a descriptor word to characterize the daily air guality.

A telephone recording of the PSI is taped each afternoon at approximately 3 PM, five days a week, and can be heard by dialing 566-3449. Predictions for weekends are included on the Friday recordings. For residents outside of the Hartford telephone exchange, the PSI is now available toll-free from the DEP representative at the Governor's State Information Bureau. The number is 1-800-842-2220. This information is also available to the public during weekday afternoons from the American Lung Association of Connecticut in East Hartford. The number there is 289-5401 or 1-800-992-2263.

FIGURE 3

POLLUTANT STANDARDS INDEX



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### E. QUALITY ASSURANCE

Quality Assurance requirements for State and Local Air Monitoring Stations (SLAMS) and the National Air Monitoring Stations (NAMS), as part of the (SLAMS) network, are specified by the code of Federal Regulations, Title 40, Part 58, Appendix A.

The regulations were enacted to provide a consistent approach to Quality Assurance activities across the country so that ambient data with a defined precision and accuracy is produced.

A Quality Assurance program was initiated in Connecticut with written procedures covering, but not limited to, the following:

Equipment procurement Equipment installation Equipment calibration Equipment operation Sample analysis Maintenance audits Performance audits Data handling and assessment

Quality assurance procedures for the above activities were fully operational on January 1, 1981 for all NAMS monitoring sites. On January 1, 1983 the above procedures were fully operational for all SLAMS monitoring sites.

Data precision and accuracy values are reported in the form of 95% probability limits as defined by equations found in Appendix A of the Federal regulations cited above.

### 1. PRECISION

Precision is a measure of data repeatability (grouping) and is determined in the following manner:

### a. <u>Manual Samplers</u> (TSP and Lead)

A second (co-located) TSP hi-vol sampler is placed alongside a regular TSP network sampler and operated concurrently. The concentration values from the co-located hi-vol sampler are compared to the network sampler and precision values are generated from the comparison.

### b. <u>Manual Samplers</u> (Lead)

Duplicate strips are cut from the hi-vol sampler filters and individually analyzed for lead. The resulting concentration values are compared, and precision values are generated from the comparison.

### c. <u>Automated Analyzers</u> (SO<sub>2</sub>,O<sub>3</sub>,CO and NO<sub>2</sub>)

All NAMS and SLAMS analyzers are challenged with a low level pollutant concentration (.08 to .10 PPM) a minimum of once every two weeks. The

comparison of analyzer response to input concentration is used to generate automated analyzer precision values.

### 2. ACCURACY

Accuracy is an estimate of the closeness of a measured value to a known value and is determined in the following manner:

### a. Manual Methods (TSP)

TSP accuracy is assessed by auditing the flow measurement phase of the TSP sampling method. In Connecticut, this is accomplished by attaching a secondary standard calibrated orifice to the hi-vol inlet and comparing the flow rates. A minimum of 25% of the TSP network samplers are audited each quarter.

### b. <u>Manual Methods</u> (Lead)

Lead accuracy is assessed by analyzing spiked audit strips and comparing the analyzed results to the known spiked values. A low- and a high-valued spike are analyzed during lead filter processing -- approximately once per month.

### c. <u>Automated Analyzers</u> (SO<sub>2</sub>, O<sub>3</sub>, CO and NO<sub>2</sub>)

Automated analyzer data accuracy is determined by challenging each analyzer with three predetermined concentration levels. Accuracy values are calculated for a number of analyzers, in a pollutant sampling network, at each concentration level. Automated analyzer response is audited at three concentration levels and zero. The results for each concentration for a particular pollutant are used to assess automated analyzer accuracy. The audit concentration levels are as follows:

| $SO_2, O_3, and NO_2$ (PPM) | CO (PPM) |
|-----------------------------|----------|
| 0.03 to 0.08                | 3 to 8   |
| 0.15 to 0.20                | 15 to 20 |
| 0.35 to 0.45                | 35 to 45 |
| 0.80 to 0.90 (NO2 only)     |          |

### II. TOTAL SUSPENDED PARTICULATES

### HEALTH EFFECTS

Particulates are solid particles or liquid droplets small enough to remain suspended in air. They include dust, soot, and smoke -- particles that may be irritating but are usually not poisonous -- and bits of solid or liquid substances that may be highly toxic. The smaller the particles, the more likely they are to reach the innermost parts of the lungs and work their damage.

The harm may be physical: clogging the lung sacs, as in anthracosis, or coal miners' "black lung" from inhaling coal dust; asbestosis or silicosis in people exposed to asbestos fibers or dusts from silicate rocks; and byssinosis, or textile workers' "brown lung" from inhaling cotton fibers.

The harm may also be chemical: changes in the human body caused by chemical reactions with pollution particles that pass through the lung membranes to poison the blood or be carried by the blood to other organs. This can happen with inhaled lead, cadmium, beryllium, and other metals, and with certain complex organic compounds that can cause cancer.

Many studies indicate that particulates and sulfur oxides (they often occur together) increase the incidence and severity of respiratory disease.

### **CONCLUSIONS**

Measured TSP levels did not exceed the primary annual standard of 75  $\mu$ g/m<sup>3</sup> or the secondary annual standard of 60  $\mu$ g/m<sup>3</sup> during 1985. No site had a measured value exceeding the primary 24-hour standard of 260  $\mu$ g/m<sup>3</sup>, but the secondary 24-hour standard of 150  $\mu$ g/m<sup>3</sup> was exceeded at both the Norwich-002 and the Stamford-001 monitoring sites in 1985. In order for the secondary standard to be <u>violated</u>, the second highest TSP level at a site must exceed 150  $\mu$ g/m<sup>3</sup>. No site violated the standard in 1985, which was also the case in 1984.

### SAMPLE COLLECTION AND ANALYSIS

**High Volume Sampler (Hi-vol)** - "Hi-vols" resemble vacuum cleaners in their operation, with an 8" x 10" piece of fiberglass filter paper replacing the vacuum bag. Retractable lids have been installed on the hi-vols in order to eliminate the passive sampling error. The samplers operate (from midnight to midnight) every sixth day at most sites and every third day at certain urban stations.

The matter collected on the filters is analyzed for weight and chemical composition. The air flow through the filter is recorded during sampling. The weight in micrograms ( $\mu$ g) divided by the volume of air in cubic meters (m<sup>3</sup>) yields the pollutant concentration for the day, in micrograms per cubic meter.

The chemical composition of the suspended particulate matter is determined at each hi-vol site as follows. Three standardized strips of every hi-vol filter are cut out and prepared for three different analyses. In the first analysis, a composite sample composed of a strip from each of several filters collected in a quarter-year is digested in acid, and the resulting solution is analyzed for metals by means of an atomic absorption spectrophotometer. The results are reported for each individual metal in  $\mu$ g/m<sup>3</sup>. In the second analysis, a composite sample is dissolved in water, filtered and the resulting solution is analyzed by means of wet chemistry techniques to determine the concentration of the particular water soluble components. The results are reported for each individual constituent of the water soluble

fraction in  $\mu$ g/m<sup>3</sup>. In the third analysis, total sulfates are determined by means of the same procedure used in the second analysis, but each of several samples collected in the quarter-year is analyzed individually and the results from all the samples are averaged. Before 1983 composite, rather than individual, samples were used to determine total sulfates.

Low Volume Sampler (Lo-vol) - The low volume sampler is a 30-day continuous sampler. It is enclosed in a shelter similar to a hi-vol, uses the same glass fiber filter paper, but operates at an air sampling flow rate approximately one-tenth that used by a standard hi-vol (i.e., 4 cfm as opposed to 40-60 cfm). The air flow through the lo-vol is measured by a temperature compensating dry gas meter. The lo-vol measurement is essentially an arithmetic average for the 30-day sampling interval. The filters are chemically analyzed in the same manner as those from the hi-vol sampler.

It should be noted that in 1985 the methods used to analyze the water soluble components of both the hi-vol and lo-vol filters were updated to reflect the latest available technology. Consequently, the accuracy of the analysis methods increased, and the resulting quarterly and monthly concentrations of ammonium, nitrate and sulfate were significantly higher than their counterparts in previous years. This is especially true for sulfate.

### **DISCUSSION OF DATA**

Monitoring Network - In 1985, 40 hi-vol and 2 lo-vol particulate samplers were operated in Connecticut (see Figure 4). Because the Federal EPA does not recognize the lo-vol instrument as an equivalent to the reference (hi-vol) method of sampling for TSP, only hi-vol data are analyzed for compliance with the National Ambient Air Quality Standards (NAAQS).

Precision and Accuracy - Precision checks were conducted at three hi-vol sampling sites which had co-located samplers. On the basis of 166 precision checks, the 95% probability limits for precision ranged from -11% to +9%. Accuracy is based on air flow through the monitor. The 95% probability limits for accuracy, based on 78 audits conducted on the hi-vol monitoring system network, ranged from -6% to +5%. (See section I.E. of this Air Quality Summary for a discussion of precision and accuracy.)

Annual Averages - The Federal EPA has established minimum sampling criteria (see Table 1) for use in determining compliance with either the primary or secondary annual NAAQS for TSP. Using the EPA criteria, one finds that neither the primary annual standard nor the secondary annual standard was exceeded. Of the thirty-six (36) sites that had valid annual geometric means (as determined by EPA minimum sampling criteria) in both 1984 and 1985, ten (10) sites had lower annual geometric means when compared to 1984. Of the twenty-five (25) sites whose annual geometric means increased, the highest increase was 11.4 µg/m<sup>3</sup> at the Stamford-001 site (see Table 5).

Historical Data - A summary of annual average TSP data for 1983-1985 is presented in Table 5. For data going back to 1957, see the 1980 and 1982 versions of the Air Quality Summary. Table 5 also includes an indication of whether the aforementioned EPA minimum sampling criteria were met at each site for each year. If the sampling was insufficient to meet the EPA criteria, an asterisk appears next to the number of samples.

Statistical Projections - The statistical projections presented in Table 5 are prepared by a DEP computer program which analyzes data from all sites operated by DEP. Input to the program includes site location and year, the number of samples (usually a maximum of 61), the annual geometric mean concentration and the geometric standard deviation. The program lists the input and calculates the 95% confidence limits about the mean and the statistical projections of the number of days in each year the primary and secondary 24-hour NAAQS would have been exceeded if sampling had been conducted every day. This analysis, like the ambient standards, is based on the assumption that the particulate data are log-normally distributed. For comparison, Table 5 also shows the number of days at a site when the

secondary 24-hour standard of 150  $\mu$ g/m<sup>3</sup> was exceeded, as demonstrated by actual measurements at the site.

The statistical projections in Table 5 indicate that more frequent TSP sampling in 1985 might have resulted in measured violations (i.e., two or more exceedances) of the secondary 24-hour standard at Bridgeport-123, Naugatuck-001, Stamford-001 and Waterbury-007. Statistical projections regarding the primary 24-hour standard of 260 µg/m<sup>3</sup> are omitted from the table because there were no predicted and no measured exceedances of this standard at any site.

Because manpower and economic limitations dictate that hi-vol sampling for particulate matter cannot be conducted every day, a degree of uncertainty is introduced as to whether the air quality at a site has either met or exceeded the national standards. This uncertainty for the annual standard can be quantified by determining 95% confidence limits about each of the annual geometric means. For example (see Table 5), in Hartford at site 003 in 1985, 58 samples were analyzed and a geometric mean of 50.8 µg/m<sup>3</sup> was then calculated. The columns labeled "95-PCT-LIMITS" show the lower and upper limits of the 95% confidence interval to be 46 and 55 µg/m<sup>3</sup>, respectively. This means that, if a larger sample set (i.e., greater than 58 samples) were collected in 1985 at this site, there is a 95% chance that the geometric mean would fall between these limits. If the upper limit happened to be less than 60 µg/m<sup>3</sup>, the national ambient secondary standard for particulates, then one could be confident that the secondary standard was met at the site. If the upper limit happened to be greater, and the lower limit less, than 60 µg/m<sup>3</sup>, then one could not be confident that the secondary standard was met at the site. If both the upper and lower limits were greater than 60 µg/m<sup>3</sup>, then one could be confident that the standard was exceeded. These three possibilities are illustrated in Table X.

In Table 6, one can examine the 1985 monitoring sites for compliance with air quality standards, using the State's hi-vol confidence limit criteria. The table shows that the DEP is confident that the primary annual standard was achieved at all the sites. With regard to the secondary annual standard, the table also shows that the DEP is confident about compliance at 38 sites and uncertain about compliance at 2 sites: Bridgeport-123 and Stamford-001.

**24-Hour Averages** - Table 7 presents the 1st and 2nd high 24-hour concentrations recorded at each site. There were no violations (i.e., less than two exceedances) of the primary 24-hour standard and no violations of the secondary 24-hour standard at any site in Connecticut in 1985, which was also the case in 1984. The 2nd high 24-hour average increased at 16 of the 36 sites which met the minimum EPA sampling criteria in both 1984 and 1985. Five (5) of these increases were greater than or equal to 20  $\mu$ g/m<sup>3</sup>. The 2nd high 24-hour average decreased at 19 of the sites, and 6 of these decreases were greater than or equal to 15  $\mu$ g/m<sup>3</sup>.

Table 8 summarizes the statistical predictions from Table 5 regarding the number of days exceeding the 24-hour standards. This table shows that, if sampling had been conducted every day in 1985, there would have been no site with a violation of the primary 24-hour standard and four (4) sites with violations of the secondary 24-hour standard. This was also the case in 1984.

**Hi-vol Averages** - Quarterly and annual averages of fourteen components or characteristics of the particulate matter collected at each hi-vol sampling location have been computed for the year 1985 and are presented in Table 9.

Lo-vol Averages - For a number of years, the DEP has been experimenting and gathering data with the lo-vol particulate monitor. Lo-vols, which operate continuously for 30-day periods, have three advantages and one disadvantage in relation to hi-vols. First, the lo-vol's continuous operation can provide annual averages which include every day of the year, rather than the fractional portion of the year sampled by hi-vols every sixth day or every third day. Second, the lo-vol needs less frequent servicing (12 times/year) than the hi-vol (61 times/year for every-sixth-day sampling). Therefore, it is more cost-effective to operate. Third, the lo-vol has a higher collection efficiency than the hi-vol, especially for small, respirable particles. The disadvantage of the lo-vol is that it does not provide daily samples for direct comparison to the 24-hour TSP standards (although 24-hour averages can be obtained by statistical interpolation).

The two lo-vol sites are located at rural locations. One site is in Mansfield and the other is in Putnam. The use of the lo-vols made it possible to continue to obtain data on annual average particulate levels at these rural sites.

Monthly and annual averages of the chemical components from the lo-vol TSP monitors have been computed for 1985 and are presented in Table 10.

10 High Days with Wind Data - Table 11 lists the 10 highest 24-hour average TSP readings with the dates of occurrence for each TSP hi-vol site in Connecticut during 1985. This table also shows the average wind conditions which occurred on each of these dates. The resultant wind direction (DIR, in compass degrees clockwise from north) and velocity (VEL, in mph), the average wind speed (SPD, in mph), and the ratio between the velocity and the speed are presented for each of four National Weather Service stations located in or near Connecticut. The resultant wind direction and velocity are vector quantities and are computed from the individual wind direction and speed readings in each day. The closer the wind speed ratio is to 1.000, the more persistent the wind. Note that the Connecticut stations have local influences which change the speed and shift the direction of the near-surface air flow (e.g., the Bradley Field air flow is channeled north-south by the Connecticut River Valley and the Bridgeport air flow is frequently subject to sea breezes).

On a statewide basis, this table shows that approximately 47% of the high TSP days occur with winds out of the southwest quadrant and most of those days have persistent winds. This relationship between southwest winds and high TSP levels is more prevalent in southwestern Connecticut. However, many of the maximum levels at some urban sites do not occur with southwest winds, indicating that these sites are possibly influenced by local sources or transport from different out-of-state sources. As noted above, a large scale southwesterly air flow is often diverted into a southerly flow up the Connecticut River Valley. At many sites in the Connecticut River Valley most of the highest TSP days occur when the winds at Bradley Airport are from the south.



1983-1985 TSP ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

TABLE 5

DISTRIBUTION--LOGNORMAL

| TOWN NAME  | SITE | YEAR   | SAMPLES | GEOM MEAN | 95-PCT-<br>LOWER | LIMITS<br>UPPER | GEOM<br>STD DEV | PREDICTED<br>DAYS OVER<br>150 UG/M3 | MEASURED<br>DAYS OVER<br>150 UG/M3 |
|------------|------|--------|---------|-----------|------------------|-----------------|-----------------|-------------------------------------|------------------------------------|
| ANS ONT A  | 200  | 7 80 L | 60      | 42 2      | 38               | 47              | 1.540           | -                                   |                                    |
| ANSONIA    | 003  | 1984   | 60      | 42.7      | 0 6<br>1 M       | 47              | 1.503           | I                                   |                                    |
| ANSONIA    | 004  | 1985   | 59      | 39.4      | 35               | 44              | 1.612           | rt.                                 |                                    |
| BRIDGEPORT | 100  | 1983   | 60      | 41.0      | 37               | 46              | 1.594           | ы                                   |                                    |
| BRIDGEPORT | 100  | 1984   | 58      | 42.8      | 39               | 47              | 1.422           |                                     |                                    |
| BRIDGEPORT | 100  | 1985   | 59      | 43.0      | 39               | 47              | 1.479           |                                     |                                    |
| BRIDGEPORT | 600  | 1983   | 57      | 39.1      | 35               | 43              | 1.539           |                                     |                                    |
| BRIDGEPORT | 600  | 1984   | 58      | 41.6      | 37               | 46              | 1.556           | -1                                  |                                    |
| BRIDGEPORT | 600  | 1985   | 57      | 29.7      | 35               | 45<br>5         | 1.615           | гđ                                  |                                    |
| BRIDGEPORT | 123  | 1983   | 59      | 54.1      | 49               | 60              | 1.530           | м                                   |                                    |
| BRIDGEPORT | 123  | 1984   | 57      | 52.6      | 48               | 58              | 1.514           | ~1                                  |                                    |
| BRIDGEPORT | 123  | 1985   | 57      | 59.6      | 53               | 67              | 1.586           | 8                                   |                                    |
| BRISTOL    | 100  | 1983   | 58      | 32.2      | 29               | 36              | 1.528           |                                     |                                    |
| BRISTOL    | 100  | 1984   | 56      | 34.5      | 31               | 39              | 1.554           |                                     |                                    |
| BRISTOL    | 100  | 1985   | 09      | 36.4      | 33               | 40              | 1.487           |                                     |                                    |
| BURLINGTON | 100  | 1983   | 58      | 20.3      | 18               | 23              | 1.797           |                                     |                                    |
| BURLINGTON | 100  | 1984   | 58      | 20.6      | 18               | 24              | 1.778           |                                     |                                    |
| BURLINGTON | 100  | 1985   | 59      | 20.1      | 18               | 22              | 1.589           |                                     |                                    |
| DANBURY    | 002  | 1983   | 56      | 44.6      | 40               | 49              | 1.509           | ľ                                   |                                    |
| DANBURY    | 002  | 1984   | 57      | 43.8      | 39               | 49              | 1.537           | ы                                   |                                    |
| DANBURY    | 002  | 1985   | 61      | 44.3      | 41               | <del>(</del> 8  | 1.445           |                                     |                                    |
| DANBURY    | 123  | 1983   | 53      | 43.1      | 38               | 48              | 1.590           | г                                   |                                    |
| DANBURY    | 123  | 1984   | 57      | 42.8      | 38               | 48              | 1.624           | 2                                   |                                    |
| DANBURY    | 123  | 1985   | 58      | 43.3      | 39               | <del>(</del> †8 | 1.552           | н                                   |                                    |
|            |      |        |         |           |                  |                 |                 |                                     |                                    |

N.B. THE GEOMETRIC MEAN HAS UNITS OF MICROGRAMS PER CUBIC METER.

\* SAMPLING NOT RANDOM OR OF INSUFFICIENT SIZE FOR REPRESENTATIVE ANNUAL STATISTICS.

TABLE 5, CONTINUED

# 1983-1985 TSP ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

DISTRIBUTION--LOGNORMAL

| TOWN NAME     | SITE | YEAR  | SAMPLES                     | GEOM MEAN | 95-PCT-<br>LOWER | LIMITS<br>UPPER | GEOM<br>STD DEV | PREDICTED<br>DAYS OVER<br>150 UG/M3 | MEASURED<br>DAYS OVER<br>150 UG/M3 |
|---------------|------|-------|-----------------------------|-----------|------------------|-----------------|-----------------|-------------------------------------|------------------------------------|
| EAST HARTFORD | 004  | 1983  | υÿ                          | 28<br>28  | 2 6              | 2.7             | 201 F           |                                     |                                    |
| EAST HARTFORD | 004  | 1984  | 57                          | 41.2      | 2 2 2            | 6 4<br>7        | 1 507           |                                     |                                    |
| EAST HARTFORD | 004  | 1985  | 57                          | 41.9      | 38               | 46<br>94        | 1.522           |                                     |                                    |
| GREENWICH     | 008  | 1983  | 494                         | 36.4      | 22               | ψ               | 779 L           |                                     |                                    |
| GREENWICH     | 008  | 1984  | 61                          | 40 o      | 2 4              | u<br>t          | 1 450           |                                     |                                    |
| GREENWICH     | 008  | 1985  | 60                          | 43.8      | 65               | - <del>4</del>  | 1.576           | P                                   |                                    |
| GROTON        | 900  | 1983  | 59                          | 35.8      | 33               | 39              | 1 433           |                                     |                                    |
| GROTON        | 900  | 1984  | 56                          | 37.3      | Ω<br>M           | 42              | 1.659           | ٣                                   |                                    |
| GROTON        | 900  | 1985  | 59                          | 34.1      | 31               | 38              | 1.533           | 4                                   |                                    |
| HADDAM        | 002  | 1 983 | 28*                         | 24.7      | 22               | 28              | 1.440           |                                     |                                    |
| HADDAM        | 002  | 1984  | 60                          | 27.9      | 25               | 31              | 1.554           |                                     |                                    |
| HARTFORD      | 003  | 1983  | 57                          | 46.3      | 42               | 51              | 1.513           | -                                   |                                    |
| HARTFORD      | 003  | 1984  | 60                          | 48.3      | 44               | 53              | 1.509           |                                     |                                    |
| HARTFORD      | 200  | 1985  | 58                          | 50.8      | 46               | 55              | 1.442           | 1                                   |                                    |
| HARTFORD      | 013  | 1983  | 60                          | 42.8      | 38               | <b>6</b> 8      | 1,580           | r                                   |                                    |
| HARTFORD      | 013  | 1984  | 57                          | 44.2      | 40               | 49              | 1.539           | 4                                   |                                    |
| HARTFORD      | 013  | 1985  | <del>4</del> 9 <del>4</del> | 42.5      | 38               | 4 <b>8</b>      | 1.531           | 1                                   |                                    |
| HARTFORD      | 014  | 1983  | 57                          | 40.3      | 36               | 45              | 1.512           |                                     |                                    |
| HARTFORD      | 014  | 1984  | 909                         | 41.7      | 38               | 46              | 1.519           |                                     |                                    |
| HARTFORD      | 014  | 1985  | 58                          | 43.7      | 40               | 48              | 1.453           |                                     |                                    |
| MANCHESTER    | 100  | 1983  | 59                          | 33.7      | 31               | 37              | 1.481           |                                     |                                    |
| MANCHESTER    | 100  | 1984  | 60                          | 31.4      | 28               | 35              | 1.552           |                                     |                                    |
| MANCHESTER    | 001  | 1985  | 55                          | 35.1      | 31               | 39              | 1.565           |                                     |                                    |
| MERIDEN       | 002  | 1983  | 55                          | 40.6      | 36               | 45              | 1.552           |                                     |                                    |
| MERIDEN       | 002  | 1984  | 60                          | 42.4      | 38               | 47              | 1.510           |                                     |                                    |
| MERIDEN       | 002  | 1985  | 59                          | 44.9      | 41               | 50              | 1.519           | Ч                                   |                                    |
| MERIDEN       | 008  | 1983  | 59                          | 37.2      | 34               | 41              | 1.532           |                                     |                                    |
|               |      |       |                             |           |                  |                 |                 |                                     |                                    |

\* SAMPLING NOT RANDOM OR OF INSUFFICIENT SIZE FOR REPRESENTATIVE ANNUAL STATISTICS.

N.B. THE GEOMETRIC MEAN HAS UNITS OF MICROGRAMS PER CUBIC METER.
# 1983-1985 TSP ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

DISTRIBUTION--LOGNORMAL

| MEASURED<br>DAYS OVER<br>150 UG/M3  |  |                                     |                  |                                     |   |   |   |                                     |                                     |
|-------------------------------------|--|-------------------------------------|------------------|-------------------------------------|---|---|---|-------------------------------------|-------------------------------------|
| PREDICTED<br>DAYS OVER<br>150 UG/M3 |  |                                     |                  | 1 0                                 |   |   |   | ннн                                 |                                     |
| GEOM<br>STD DEV                     | 1.484<br>1.509<br>1.481                      | 1.405<br>1.460<br>1.472             | 1.483<br>1.586   | 1.506<br>1.562<br>1.574             | 1.590<br>1.506<br>1.456                   | 1.569<br>1.561<br>1.525                   | 1.537<br>1.555<br>1.517                   | 1.521<br>1.523<br>1.466             | 1.438<br>1.421<br>1.451             |
| -LIMITS<br>UPPER                    | 4 4<br>4 8<br>6 8                            | 44<br>45<br>49                      | 33<br>29         | 44<br>46<br>50                      | 40<br>41                                  | 40<br>41<br>41                            | 41<br>40<br>38                            | 54<br>54                            | 48<br>49<br>48                      |
| 95-PCT-<br>LOMER                    | 38<br>38<br>38<br>38                         | 38<br>37<br>41                      | 22<br>23         | 36<br>37<br>41                      | 32<br>35<br>35                            | 32<br>33<br>34                            | 33<br>32<br>31                            | 41<br>44<br>6                       | 4 4 0<br>4 4 7                      |
| GEOM MEAN                           | 38.2<br>38.8<br>41.7                         | 40.9<br>40.8<br>44.9                | 27.0<br>25.6     | 40.2<br>41.4<br>45.2                | 35.8<br>36.7<br>37.8                      | 35.8<br>37.1<br>37.2                      | 36.6<br>36.0<br>34.5                      | 48.8<br>45.5<br>48.8                | 43.8<br>45.3<br>44.1                |
| SAMPLES                             | 57<br>55<br>57                               | 58<br>61<br>60                      | 15*<br>60        | 59<br>60                            | 59<br>59<br>59                            | 58<br>61<br>59                            | 59<br>56<br>56                            | 52<br>54<br>51                      | 53<br>59<br>55                      |
| YEAR                                | 1983<br>1984<br>1985                         | 1983<br>1984<br>1985                | 1984<br>1985     | 1983<br>1984<br>1985                | 1983<br>1984<br>1985                      | 1983<br>1984<br>1985                      | 1983<br>1984<br>1985                      | 1983<br>1984<br>1985                | 1983<br>1984<br>1985                |
| SITE                                | 003<br>003<br>003                            | 002<br>002<br>002                   | 100              | 100<br>100                          | 007<br>007<br>007                         | 008<br>008<br>008                         | 600<br>600                                | 002<br>002<br>002                   | 013<br>013<br>013                   |
| TOWN NAME                           | 11 DDLE TOWN<br>11 DDLE TOWN<br>11 DDLE TOWN | 11 L FORD<br>11 L FORD<br>11 L FORD | 10RRIS<br>10RRIS | VAUGATUCK<br>NAUGATUCK<br>NAUGATUCK | NEW BRITAIN<br>NEW BRITAIN<br>NEW BRITAIN | NEW BRITAIN<br>NEW BRITAIN<br>NEW BRITAIN | NEW BRITAIN<br>NEW BRITAIN<br>NEW BRITAIN | NEW HAVEN<br>NEM HAVEN<br>NEM HAVEN | NEW HAVEN<br>NEW HAVEN<br>NEW HAVEN |

\* SAMPLING NOT RANDOM OR OF INSUFFICIENT SIZE FOR REPRESENTATIVE ANNUAL STATISTICS.

N.B. THE GEOMETRIC MEAN HAS UNITS OF MICROGRAMS PER CUBIC METER.

1983-1985 TSP ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

DISTRIBUTION--LOGNORMAL

| TOWN NAME                           | SITE              | YEAR                 | SAMPLES  | GEOM MEAN            | 95-PCT-<br>LOWER | LIMITS<br>UPPER    | GEOM<br>STD DEV         | PREDICTED<br>DAYS OVER<br>150 UG/M3 | MEASURED<br>DAYS OVER<br>150 UG/M3 |
|-------------------------------------|-------------------|----------------------|--|----------------------|------------------|--------------------|-------------------------|-------------------------------------|------------------------------------|
| NORMALK<br>NORMALK<br>NORMALK       | 100<br>100        | 1983<br>1984<br>1985 | 58<br>57   | 40.0<br>41.8<br>41.5 | 36<br>37<br>37   | 008<br>777         | 1.491<br>1.506<br>1.527 |                                     |                                    |
| NORWALK<br>NORMALK<br>NORMALK       | 005<br>005<br>005 | 1983<br>1984<br>1985 | 58<br>57   | 45.4<br>45.6<br>46.4 | ここを              | 50<br>51           | 1.506<br>1.475<br>1.502 | ri =                                |                                    |
| NORMALK<br>NORMALK<br>NORMALK       | 012<br>012<br>012 | 1983<br>1984<br>1985 | 60<br>59   | 41.1<br>40.9<br>41.1 | 37<br>37         | 1 4 4 4<br>1 1 1 1 | 1.542<br>1.500<br>1.466 | 4                                   |                                    |
| NORWICH<br>NORWICH                  | 100<br>100        | 1983<br>1984         | 59<br>20*  | 39.6<br>39.6         | 36<br>33         | 43<br>47           | 1.462<br>1.485          |                                     |                                    |
| NORWI CH<br>NORWI CH                | 002<br>002        | 1984<br>1985         | 41*<br>54  | 45.2<br>43.4         | 40<br>39         | 51<br>49           | 1.514<br>1.567          | PH 1-14                             | Н                                  |
| STAMFORD<br>STAMFORD<br>STAMFORD    | 100<br>100        | 1983<br>1984<br>1985 | 59<br>56   | 45.4<br>45.4<br>56.8 | <b>41</b><br>51  | 51<br>53<br>63     | 1.573<br>1.600<br>1.557 | 0 0 U                               | ч                                  |
| STAMFORD<br>STAMFORD<br>STAMFORD    | 007<br>007        | 1983<br>1984<br>1985 | 5<br>5<br>6<br>6<br>7<br>6<br>7<br>6<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7 | 44.7<br>44.8<br>47.1 | 41<br>41<br>3    | 49<br>51           | 1.462<br>1.423<br>1.435 |                                     |                                    |
| STAMFORD<br>STAMFORD<br>STAMFORD    | 021<br>021<br>021 | 1983<br>1984<br>1985 | 59<br>57<br>53   | 45.3<br>49.4<br>44.8 | 41<br>45<br>41   | 50<br>49<br>49     | 1.468<br>1.457<br>1.411 |                                     |                                    |
| STRATFORD<br>STRATFORD<br>STRATFORD | 005<br>005<br>005 | 1983<br>1984<br>1985 | 58<br>60<br>58   | 44.4<br>44.1<br>44.2 | 41<br>40<br>40   | 4 4 8<br>4 9 8     | 1.435<br>1.502<br>1.566 | T                                   |                                    |

N.B. THE GEOMETRIC MEAN HAS UNITS OF MICROGRAMS PER CUBIC METER.

\* SAMPLING NOT RANDOM OR OF INSUFFICIENT SIZE FOR REPRESENTATIVE ANNUAL STATISTICS.

1983-1985 TSP ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

TABLE 5, CONTINUED

(

DISTRIBUTION--LOGNORMAL

 $\left( \right)$ 

| TOWN NAME                                 | SITE              | YEAR                 | SAMPLES                         | GEOM MEAN            | 95-PCT-<br>LOWER      | LIMITS<br>UPPER  | GEOM<br>STD DEV         | PREDICTED<br>DAYS OVER<br>150 UG/M3 | MEASURED<br>DAYS OVER<br>150 UG/M3 |
|---|-------------------|----------------------|---------------------------------|----------------------|-----------------------|--|-------------------------|-------------------------------------|------------------------------------|
| TORRINGTON<br>TORRINGTON<br>TORRINGTON    | 100<br>100        | 1983<br>1984<br>1985 | 56<br>61<br>60                  | 36.8<br>38.0<br>37.6 | 33<br>34<br>34        | 41<br>43   | 1.526<br>1.637<br>1.613 | rot rot                             |                                    |
| VOLUNTOWN<br>VOLUNTOWN<br>VOLUNTOWN       | 100<br>100        | 1983<br>1984<br>1985 | 5<br>5<br>6<br>7<br>6<br>7<br>6 | 23.7<br>23.2<br>23.3 | 21<br>21<br>21        | 27<br>26<br>26   | 1.624<br>1.618<br>1.495 |                                     |                                    |
| WALLINGFORD<br>MALLINGFORD<br>WALLINGFORD | 100<br>100        | 1983<br>1984<br>1985 | 57<br>60<br>59                  | 40.4<br>43.1<br>43.1 | 39<br>39<br>39        | 45<br>48<br>48   | 1.512<br>1.556<br>1.597 | 44                                  |                                    |
| MATERBURY<br>MATERBURY<br>MATERBURY       | 005<br>005<br>005 | 1983<br>1984<br>1985 | 58<br>57<br>56                  | 38.5<br>41.4<br>42.8 | 35<br>37<br>38        | 8<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7 | 1.488<br>1.541<br>1.567 | proj                                |                                    |
| MATERBURY<br>WATERBURY<br>MATERBURY       | 900<br>900        | 1983<br>1984<br>1985 | 60<br>59                        | 34.2<br>37.1<br>35.7 | 31<br>33<br>32        | 38<br>41<br>39   | 1.523<br>1.558<br>1.502 |                                     |                                    |
| MATERBURY<br>MATERBURY<br>MATERBURY       | 007<br>007<br>007 | 1983<br>1984<br>1985 | 60<br>59<br>60                  | 47.4<br>47.5<br>50.6 | 5 5 5<br>5 7 5<br>5 3 | 52<br>53   | 1.472<br>1.545<br>1.581 | ΝM                                  |                                    |
| MATERFORD<br>MATERFORD                    | 100<br>100        | 1983<br>1984         | 55<br>58                        | 25.6<br>29.3         | 23<br>26              | 29<br>33   | 1.646<br>1.693          |                                     |                                    |
| WILLIMANTIC<br>WILLIMANTIC<br>WILLIMANTIC | 002<br>002<br>002 | 1983<br>1984<br>1985 | 60<br>61                        | 35.2<br>37.6<br>37.3 | 44<br>М М М           | ,<br>441<br>41   | 1.505<br>1.491<br>1.559 |                                     |                                    |
|   |                   |                      |                                 |                      |                       |  |                         |                                     |                                    |

\* SAMPLING NOT RANDOM OR OF INSUFFICIENT SIZE FOR REPRESENTATIVE ANNUAL STATISTICS.

N.B. THE GEOMETRIC MEAN HAS UNITS OF MICROGRAMS PER CUBIC METER.

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## **FIGURE X**

## COMPLIANCE WITH THE ANNUAL TSP STANDARDS USING 95% CONFIDENCE LIMITS ABOUT THE ANNUAL GEOMETRIC MEAN CONCENTRATION



- L = The lower limit of the 95% confidence interval about the annual geometric mean concentration.
- U = The upper limit of the 95% confidence interval about the annual geometric mean concentration.

## TABLE 6

# COMPLIANCE WITH ANNUAL TSP STANDARDS DURING 1985

## (95% CONFIDENCE INTERVAL)

|  | EXCEEDED | UNCERTAIN | ACHIEVED  |
|--|----------|-----------|-----------|
| PRIMARY<br>STANDARD<br>(75 μg/m <sup>3</sup> )   | NO SITES | NO SITES  | 40 SITES  |
| SECONDARY<br>STANDARD<br>(60 μg/m <sup>3</sup> ) | NO SITES | 2 SITES*  | 38 SITES* |

\* The upper 95% confidence limit exceeds the secondary annual standard at the Bridgeport-123 site and the Stamford-001 site.

## TABLE 7

#### **1985 MAXIMUM 24-HOUR TSP CONCENTRATIONS**



- \* Database for the site is deficient in number or distribution of observations.
- N.B. When a listed concentration occurs more than once at a site, the earliest date of occurrence is given.



- \* Database for the site is deficient in number or distribution of observations.
- N.B. When a listed concentration occurs more than once at a site, the earliest date of occurrence is given.



\* Database for the site is deficient in number or distribution of observations.

N.B. When a listed concentration occurs more than once at a site, the earliest date of occurrence is given.



STANDARD

**STANDARD** 

\* Database for the site is deficient in number or distribution of observations.

N.B. When a listed concentration occurs more than once at a site, the earliest date of occurrence is given.

## TABLE 8

## SUMMARY OF THE STATISTICALLY PREDICTED NUMBER OF HI-VOL SITES EXCEEDING THE 24-HOUR TSP STANDARDS

|      |                           | SITES WITH<br>EXCEEDING TH<br>STANDARD | $\frac{1}{2} 2 \text{ DAYS}$<br>HE SECONDARY<br>(150 µg/m3) | SITES WITH<br>EXCEEDING<br>STANDARD | l <u>&gt;</u> 2 DAYS<br>THE PRIMARY<br>(260 µg/m3) |
|------|---------------------------|--|---|-------------------------------------|--|
| YEAR | NO. OF SITES <sup>1</sup> | No. of Sites                           | Percentage<br>of All Sites                                  | No. of Sites                        | Percentage<br>of All Sites                         |
| 1971 | 44                        | 37                                     | 84%   | 19                                  | 43%  |
| 1972 | 46                        | 43                                     | 93%   | 13                                  | 28%  |
| 1973 | 44                        | 31                                     | 70%   | 11                                  | 25%  |
| 1974 | 62                        | 49                                     | <b>79</b> %   | 5                                   | 8%   |
| 1975 | 51                        | 38                                     | 75%   | 2                                   | 4%   |
| 1976 | 38                        | 33                                     | 87%   | 1                                   | 3%   |
| 1977 | 37                        | 25                                     | 68%   | 0                                   | 0%   |
| 1978 | 34                        | 20                                     | 59%   | 5                                   | 15%  |
| 1979 | 33                        | 20                                     | 61%   | 2                                   | <b>6</b> %   |
| 1980 | 33                        | 14                                     | 42%   | 0                                   | 0%   |
| 1981 | 40                        | 14                                     | 35%   | 0                                   | 0%   |
| 1982 | 39                        | 11                                     | 28%   | 0                                   | 0%   |
| 1983 | 40                        | 2                                      | 5%  | 0                                   | 0%   |
| 1984 | 40                        | 4                                      | 10%   | 0                                   | 0%   |
| 1985 | 39                        | 4                                      | 10%   | 0                                   | 0%   |

<sup>1</sup> Only those sites are used which have sufficient data to permit the calculation of a valid annual average concentration.

#### TABLE 9

## **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

32.

|                     | TOWN<br>ANSONIA           | A<br>0<br>0   | REA<br>060-<br>008 |          | SITE<br>004 |            |
|---------------------|---------------------------|---------------|--------------------|----------|-------------|------------|
|                     | 1ST                       | QUARTI<br>2ND | ERLY AV<br>3RD     | G<br>4TH | ANNUAL A    | <u>۱۷G</u> |
| <u>METALS</u> (ng/r | m <sup>3</sup> )          |               |                    |          |             |            |
| BERYLLIUM           | <.1                       | <.1           | <.1                | <.1      | <.1         |            |
| CADMIUM             | 19.1                      | 7.6           | 15.3               | 41.2     | 20.7        |            |
| CHROMIUM            | 4                         | 1             | 4                  | 2        | 3           |            |
| COPPER              | 160                       | 100           | 140                | 50       | 110         |            |
| IRON                | 730                       | 460           | 560                | 600      | 580         |            |
| LEAD                | 290                       | 130           | 110                | 100      | 160         |            |
| MANGANESE           | 12                        | 13            | 11                 | 12       | 12          |            |
| NICKEL              | 20                        | 9             | 8                  | 10       | 12          |            |
| VANADIUM            | 60                        | 20            | 20                 | 20       | 30          |            |
| ZINC                | 790                       | 270           | 420                | 310      | 440         |            |
| WATER SOLU          | BLES (ng/m <sup>3</sup> ) |               |                    |          |             |            |
| NITRATE             | 3730                      | 4460          | 2930               | 2540     | 3440        |            |
| SULFATE             | 7700                      | 10020         | 8210               | 7220     | 8330        |            |
| AMMONIUM            | 340                       | 90            | 50                 | 330      | 200         |            |
| <u>TSP</u> (μg/m³)  | 50                        | 47            | 40                 | 39       | 44          |            |
| SAMPLE COU          | <u>NT</u> 14              | 16            | 14                 | 15       |             |            |

|                    | TOWN<br>BRIDGEPORT               | ۵<br>0       | REA<br>060 |          | SITE<br>001 |           |
|--------------------|----------------------------------|--------------|------------|----------|-------------|-----------|
|                    | 1ST                              | QUART<br>2ND | ERLY AV    | G<br>4TH | ANNUAL A    | <u>VG</u> |
| METALS (ng/m       | 13)                              |              |            |          |             |           |
| BERYLLIUM          | <.1                              | <.1          | <.1        | <.1      | <.1         |           |
| CADMIUM            | 3.4                              | 4.0          | 1.4        | 2.6      | 2.9         |           |
| CHROMIUM           | 4                                | 4            | 3          | 2        | 3           |           |
| COPPER             | 70                               | 140          | 150        | 40       | 100         |           |
| IRON               | 620                              | 670          | 600        | 570      | 620         |           |
| LEAD               | 340                              | 220          | 160        | 120      | 210         |           |
| MANGANESE          | 16                               | 19           | 13         | 19       | 17          |           |
| NICKEL             | 20                               | 15           | 9          | 8        | 13          |           |
| VANADIUM           | 60                               | 30           | 20         | 20       | 30          |           |
| ZINC               | 110                              | 80           | 40         | 50       | 70          |           |
| WATER SOLU         | <u>3LES</u> (ng/m <sup>3</sup> ) |              |            |          |             |           |
| NITRATE            | 6350                             | 5130         | 2910       | 2940     | 4310        |           |
| SULFATE            | 8220                             | 9760         | 9220       | 7770     | 8770        |           |
| AMMONIUM           | 220                              | 80           | 90         | 200      | 150         |           |
| <u>TSP</u> (μg/m³) | 50                               | 53           | 42         | 40       | 46          |           |
| SAMPLE COUN        | <u>NT</u> 14                     | 16           | 15         | 15       |             |           |

# **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                    | TOWN<br>BRIDGEPORT        | ب<br>0       | AREA<br>1060   |                 | SITE<br>009 |
|--------------------|---------------------------|--------------|----------------|-----------------|-------------|
|                    | 1ST                       | QUART<br>2ND | ERLY AV<br>3RD | <u>G</u><br>4TH | ANNUAL AVG  |
| METALS (ng/r       | n <sup>3</sup> )          |              |                |                 |             |
| BERYLLIUM          | <.1                       | <.1          | <.1            | <.1             | <.1         |
| CADMIUM            | 4.0                       | 4.8          | 1.6            | 1.7             | 3.0         |
| CHROMIUM           | 3                         | 3            | 4              | 2               | 3           |
| COPPER             | 150                       | 140          | 180            | 170             | 160         |
| IRON               | 550                       | 610          | 550            | 350             | 510         |
| LEAD               | 320                       | 190          | 120            | 80              | 180         |
| MANGANESE          | 18                        | 16           | 10             | - 11            | 14          |
| NICKEL             | 25                        | 14           | 9              | 9               | 14          |
| VANADIUM           | 80                        | 30           | 20             | 20              | 40          |
| ZINC               | 140                       | 80           | 40             | 40              | 70          |
| WATER SOLU         | BLES (ng/m <sup>3</sup> ) |              |                |                 |             |
| NITRATE            | 5870                      | 5810         | 3940           | 2560            | 4510        |
| SULFATE            |                           | 9870         | 10050          | 7490            |             |
| AMMONIUM           | 420                       | 130          | 250            | 230             | 260         |
| <u>TSP</u> (µg/m³) | . 49                      | 53           | 45             | 31              | 44          |
| SAMPLE COUN        | <u>NT</u> 14ª             | <b>14</b> b  | 14             | 15              |             |

<sup>a</sup> For sulfate, the sample count is 0 in the first quarter. <sup>b</sup> For sulfate, the sample count is 9 in the second quarter.

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|                    | TOWN<br>BRIDGEPORT        | A<br>0        | REA<br>060     |                 | SITE<br>123 |            |
|--------------------|---------------------------|---------------|----------------|-----------------|-------------|------------|
|                    | 1ST                       | QUARTI<br>2ND | RLY AVO<br>3RD | <u>3</u><br>4TH | ANNUAL A    | <u>AVG</u> |
| METALS (ng/r       | m <sup>3</sup> )          |               |                |                 |             |            |
| BERYLLIUM          | <.1                       | <.1           | <.1            | <.1             | <.1         |            |
| CADMIUM            | 2.4                       | 6.1           | 1.5            | 1.5             | 2.8         |            |
| CHROMIUM           | 4                         | 8             | 8              | 2               | 5           |            |
| COPPER             | 90                        | 120           | 140            | 80              | 110         |            |
| IRON               | 950                       | 1840          | 1280           | 660             | 1170        |            |
| LEAD               | 350                       | 270           | 170            | 120             | 230         |            |
| MANGANESE          | 24                        | 62            | 21             | 15              | 30          |            |
| NICKEL             | 25                        | 19            | 16             | 11              | 18          |            |
| VANADIUM           | 80                        | 30            | 30             | 20              | 40          |            |
| ZINC               | 150                       | 100           | 60             | 60              | 90          |            |
| WATER SOLU         | BLES (ng/m <sup>3</sup> ) |               |                |                 |             |            |
| NITRATE            | 5210                      | 5730          | 3610           | 2770            | 4320        |            |
| SULFATE            | 9630                      | 10340         | 9870           | 7480            | 9300        |            |
| AMMONIUM           | 200                       | 170           | 420            | 290             | 270         |            |
| <u>TSP</u> (μg/m³) | 68                        | 93            | 73             | 45              | 69          |            |
| SAMPLE COU         | <u>NT</u> 15              | 14            | 14             | 15              |             |            |

# **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

| TOV<br>BRIS                     | VN<br>TOL              | AR<br>00              | REA<br>70      |      | SITE<br>001 |
|---------------------------------|------------------------|-----------------------|----------------|------|-------------|
|                                 | 1ST                    | <u>QUARTEI</u><br>2ND | RLY AVG<br>3RD | 4TH  | ANNUAL AVG  |
| METALS (ng/m <sup>3</sup> )     |                        |                       |                |      |             |
| BERYLLIUM                       | <.1                    | <.1                   | <.1            | <.1  | <.1         |
| CADMIUM                         | 1.1                    | 1.5                   | 1.3            | 0.8  | 1.2         |
| CHROMIUM                        | 3                      | <1                    | 4              | 2    | 2a          |
| COPPER                          | 160                    | 150                   | 140            | 30   | 120         |
| IRON                            | 690                    | 390                   | 420            | 830  | 580         |
| LEAD                            | 230                    | 130                   | 90             | 80   | 130         |
| MANGANESE                       | 14                     | 11                    | 11             | 11   | 12          |
| NICKEL                          | 8                      | 3                     | 4              | 11   | 6           |
| VANADIUM                        | 30                     | 30                    | 10             | 50   | 30          |
| ZINC                            | 70                     | 40                    | 20             | 40   | 40          |
|                                 |                        |                       |                |      |             |
| WATER SOLUBLES                  | 5 (ng/m <sup>3</sup> ) |                       |                |      |             |
| NITRATE                         | 5790                   | 3960                  | 1880           | 2680 | 3610        |
| SULFATE                         | 7460                   | 9550                  | 9220           | 7380 | 8410        |
| AMMONIUM                        | 120                    | 100                   | 120            | 250  | 150         |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 48                     | 40                    | 36             | 32   | 39          |
| SAMPLE COUNT                    | 15                     | 16                    | 14             | 15   |             |

<sup>a</sup> The average was calculated using one quarter of the reportable limit in the second quarter.

#### **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                    | TOWN<br>BURLINGTON               | ۲<br>0            | AREA<br>1085   |          | SITE<br>001     |
|--------------------|----------------------------------|-------------------|----------------|----------|-----------------|
|                    | 1ST                              | QUART<br>2ND      | ERLY AV<br>3RD | G<br>4TH | ANNUAL AVG      |
| METALS (ng/n       | n <sup>3</sup> )                 |                   |                |          |                 |
| BERYLLIUM          | <.1                              | <.1               | <.1            | <.1      | <.1             |
| CADMIUM            | 0.9                              | 0.7               | 2.0            | 0.8      | 1.1             |
| CHROMIUM           | 1                                | . <i>25</i><br>⊂1 | 1              | 1        | 1a              |
| COPPER             | 80                               | 80                | 90             | 60       | 80              |
| IRON               | 180                              | 160               | 200            | 120      | 170             |
| LEAD               | 80                               | 70                | 30             | 30       | 50              |
| MANGANESE          | 4                                | 7                 | 4              | 5        | 5               |
| NICKEL             | 3                                | 2                 | 2              | 3        | 2               |
| VANADIUM           | 10                               | 10                | <10            | 10       | 10 <sup>b</sup> |
| ZINC               | 70                               | 30                | <10            | 20       | 30c             |
| WATER SOLU         | <u>BLES</u> (ng/m <sup>3</sup> ) |                   |                |          |                 |
| NITRATE            | 3030                             | 2470              | 1060           | 1540     | 2060            |
| SULFATE            | 6030                             | 7690              | 6930           | 5760     | 6630            |
| AMMONIUM           | 60                               | 10                | 40             | <10      | <b>30</b> d     |
| <u>TSP</u> (µg/m³) | 22                               | 29                | 23             | 21       | 24              |
| SAMPLE COUI        | <u>NT</u> 15                     | 16                | 14             | 14       |                 |

<sup>a</sup> The average was calculated using one quarter of the reportable limit in the second quarter. <sup>b,c</sup> The average was calculated using one quarter of the reportable limit in the third quarter. <sup>d</sup> The average was calculated using one quarter of the reportable limit in the fourth quarter.

## **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                    | TOWN<br>DANBURY  | م<br>0       | AREA<br>175    |                  | SITE<br>002 |
|--------------------|------------------|--------------|----------------|------------------|-------------|
|                    | <u>15T</u>       | QUART<br>2ND | ERLY AV<br>3RD | <u>'G</u><br>4TH | ANNUAL AVG  |
| METALS (ng/        | m <sup>3</sup> ) |              |                |                  |             |
| BERYLLIUM          | <.1              | <.1          | <.1            | <.1              | <.1         |
| CADMIUM            | 1.1              | 1.1          | 1.6            | 1.0              | 1.2         |
| CHROMIUM           | 1                | 1            | 2              | 3                | 2           |
| COPPER             | 30               | 50           | 90             | 50               | 50          |
| IRON               | 880              | 570          | 770            | 620              | 710         |
| LEAD               | 240              | 140          | 110            | 90               | 140         |
| MANGANES           | E 5 16           | 13           | 12             | 16               | 14          |
| NICKEL             | 11               | 4            | 20             | 8                | 11          |
| VANADIUM           | 30               | ి.5<br><10   | 10             | 10               | 10ª         |
| ZINC               | 70               | 40           | 20             | 40               | 40          |
| WATER SOLU         | JBLES (ng/m³)    |              |                |                  |             |
| NITRATE            | 4300             | 4120         | 2390           | 2290             | 3290        |
| SULFATE            | 7730             | 9330         | 9730           | 7380             | 8560        |
| AMMONIUM           | 1 190            | 70           | 80             | 220              | 140         |
| <u>TSP</u> (µg/m³) | 59               | 46           | 46             | 40               | 48          |
| SAMPLE COL         | <u>JNT</u> 15    | 16           | 15             | 15               |             |

<sup>a</sup> The average was calculated using one quarter of the reportable limit in the second quarter.

|                    | TOWN<br>DANBURY  | AREA<br>0175 |                |                  | SITE<br>123 |
|--------------------|------------------|--------------|----------------|------------------|-------------|
|                    | 1ST              | QUART<br>2ND | ERLY AV<br>3RD | <u>'G</u><br>4TH | ANNUAL AVG  |
| METALS (ng/n       | 1 <sup>3</sup> ) |              |                |                  |             |
| BERYLLIUM          | <.1              | <.1          | <.1            | <.1              | <.1         |
| CADMIUM            | 1.3              | 1.1          | 1.7            | 1.1              | 1.3         |
| CHROMIUM           | 2                | 1            | 3              | 2                | 2           |
| COPPER             | 130              | 130          | 80             | 50               | 100         |
| IRON               | 900              | 640          | 570            | 620              | 690         |
| LEAD               | 250              | 130          | 110            | 80               | 140         |
| MANGANESE          | 17               | 15           | 9              | 12               | 13          |
| NICKEL             | 9                | 4            | 6              | 7                | 7           |
| VANADIUM           | 30               | 10           | 10             | 10               | 20          |
| ZINC               | 80               | 40           | 20             | 30               | 40          |
|                    |                  |              |                |                  |             |
| WATER SOLU         | BLES (ng/m³)     |              |                |                  |             |
| NITRATE            | 4070             | 3880         | 2170           | 2170             | 3100        |
| SULFATE            | 7420             | 9790         | 8330           | 6790             | 8070        |
| AMMONIUM           | 200              | 60           | 50             | 140              | 110         |
| <u>TSP</u> (μg/m³) | 62               | 49           | 40             | 39               | 48          |
| SAMPLE COU         | <u>NT</u> 15     | 15           | 13             | 15               |             |

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|                                 | TOWN<br>EAST HARTFO       | RD 0         | REA<br>220     |          | SITE<br>004 |     |
|---------------------------------|---------------------------|--------------|----------------|----------|-------------|-----|
|                                 | 1ST                       | QUART<br>2ND | ERLY AV<br>3RD | G<br>4TH | ANNUAL      | AVG |
| METALS (ng/n                    | n <sup>3</sup> )          |              |                |          |             |     |
| BERYLLIUM                       | <.1                       | <.1          | <.1            | <.1      | <.1         |     |
| CADMIUM                         | 2.3                       | 3.4          | 1.7            | 1.1      | 2.2         |     |
| CHROMIUM                        | 3                         | 1            | 3              | 4        | 3           |     |
| COPPER                          | 60                        | 70           | 90             | 50       | 70          |     |
| IRON                            | 760                       | 590          | 660            | 870      | 720         |     |
| LEAD                            | 330                       | 210          | 190            | 120      | 210         |     |
| MANGANESE                       | 13                        | 14           | 12             | 14       | 13          |     |
| NICKEL                          | 11                        | 5            | 6              | 12       | 8           |     |
| VANADIUM                        | 30                        | 10           | 10             | 20       | 20          |     |
| ZINC                            | 80                        | 40           | 10             | 60       | 50          |     |
|                                 |                           |              |                |          |             |     |
| WATER SOLU                      | BLES (ng/m <sup>3</sup> ) |              |                |          |             |     |
| NITRATE                         | 4310                      | 3500         | 2420           | 2510     | 3230        |     |
| SULFATE                         | 8010                      | 9480         | 9130           | 6800     | 8370        |     |
| AMMONIUM                        | 210                       | 100          | 70             | 200      | 150         |     |
|                                 |                           |              |                |          |             |     |
| <u>TSP</u> (µg/m <sup>3</sup> ) | 53                        | 48           | 44             | 60       | 51          |     |
| SAMPLE COU                      | <u>NT</u> 15              | 16           | 13             | 14       |             |     |

|                    | TOWN<br>GREENWICH                | AREA<br>0330 |                |          | SITE<br>008 |            |
|--------------------|----------------------------------|--------------|----------------|----------|-------------|------------|
|                    | 1ST                              | QUART<br>2ND | ERLY AV<br>3RD | G<br>4TH | ANNUAL      | <u>AVG</u> |
| METALS (ng/m       | 13)                              |              |                |          |             |            |
| BERYLLIUM          | <.1                              | <.1          | <.1            | <.1      | <.1         |            |
| CADMIUM            | 1.6                              | 1.8          | 2.5            | 1.1      | 1.8         |            |
| CHROMIUM           | 3                                | 1            | 2              | 2        | 2           |            |
| COPPER             | 120                              | 230          | 200            | 90       | 160         |            |
| IRON               | 840                              | 800          | 700            | 580      | 730         |            |
| LEAD               | 240                              | 160          | 110            | 90       | 150         |            |
| MANGANESE          | 12                               | 16           | 12             | 11       | 13          |            |
| NICKEL             | 11                               | 6            | 7              | 9        | 8           |            |
| VANADIUM           | 20                               | 10           | 10             | 10       | 10          |            |
| ZINC               | 70                               | 50           | 20             | 50       | 50          |            |
| WATER SOLU         | <u>3LES</u> (ng/m <sup>3</sup> ) |              |                |          |             |            |
| NITRATE            | 3920                             | 4450         | 2550           | 2800     | 3460        |            |
| SULFATE            | 6860                             | 9250         | 10620          | 7930     | 8690        |            |
| AMMONIUM           | 250                              | 40           | 160            | 160      | 150         |            |
| <u>TSP</u> (µg/m³) | 49                               | 55           | 47             | 41       | 48          |            |
| SAMPLE COUN        | <u>NT</u> 15                     | 16           | 15             | 14       |             |            |

## **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                                 | TOWN<br>GROTON   | ۵<br>0        | REA<br>350     |          | SITE<br>006 |
|---------------------------------|------------------|---------------|----------------|----------|-------------|
|                                 | 1ST              | QUARTI<br>2ND | ERLY AV<br>3RD | G<br>4TH | ANNUAL AVG  |
| METALS (ng/                     | m <sup>3</sup> ) |               |                |          |             |
| BERYLLIUM                       | <.1              | <.1           | <.1            | <.1      | <.1         |
| CADMIUM                         | 0.9              | 0.7           | 0.5            | 0.9      | 0.8         |
| CHROMIUM                        | 3                | 3             | 5              | 2        | 3           |
| COPPER                          | 70               | 120           | 120            | 40       | 90          |
| IRON                            | 440              | 570           | 390            | 580      | 500         |
| LEAD                            | 120              | 80            | 60             | 50       | 80          |
| MANGANES                        | E 10             | 12            | 7              | 10       | 10          |
| NICKEL                          | 23               | 24            | 10             | 21       | 20          |
| VANADIUM                        | 60               | 60            | 20             | 40       | 50          |
| ZINC                            | 60               | 60            | <10            | 50       | 40a         |
| WATER SOLL                      | JBLES (ng/m³)    |               |                |          |             |
| NITRATE                         | 3850             | 3550          | 3000           | 2750     | 3300        |
| SULFATE                         | 7600             | 9200          | 7310           | 7700     | 8000        |
| AMMONIUN                        | l 160            | 40            | 20             | 260      | 120         |
| <u>TSP</u> (µg/m <sup>3</sup> ) | 39               | 41            | 33             | 35       | 37          |
| SAMPLE COL                      | <u>JNT</u> 15    | 16            | 13             | 15       |             |

<sup>a</sup> The average was calculated using one quarter of the reportable limit in the third quarter.

#### **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                    | TOWN<br>HARTFORD          | N AREA<br>FORD 0420 |         |                  | SITE<br>003 | TE<br>)3   |  |
|--------------------|---------------------------|---------------------|---------|------------------|-------------|------------|--|
|                    | <u>15T</u>                |                     | ERLY AV | <u>'G</u><br>4тн | ANNUAL      | <u>AVG</u> |  |
| METALS (ng/m       | 1 <sup>3</sup> )          | 2190                | 5110    | 4111             |             |            |  |
| BERYLLIUM          | <.1                       | <.1                 | <.1     | <.1              | <.1         |            |  |
| CADMIUM            | 1.7                       | 1.4                 | 1.3     | 1.5              | 1.5         |            |  |
| CHROMIUM           | 3                         | 1                   | 3       | 3                | 2           |            |  |
| COPPER             | 140                       | 140                 | 120     | 90               | 120         |            |  |
| IRON               | 730                       | 690                 | 790     | 780              | 750         |            |  |
| LEAD ·             | 410                       | 200                 | 130     | 110              | 220         |            |  |
| MANGANESE          | 14                        | 16                  | 14      | 15               | 15          |            |  |
| NICKEL             | 16                        | 5                   | 6       | 10               | 9           |            |  |
| VANADIUM           | 50                        | 10                  | 10      | 30               | 30          |            |  |
| ZINC               | 210                       | 30                  | 20      | 50               | 80          |            |  |
|                    |                           |                     |         |                  |             |            |  |
| WATER SOLU         | BLES (ng/m <sup>3</sup> ) |                     |         |                  |             |            |  |
| NITRATE            | 4240                      | 3460                | 320     | 2850             | 3450        |            |  |
| SULFATE            |                           | 8180                | 10370   | 7510             |             |            |  |
| AMMONIUM           | 180                       | 70                  | 240     | 280              | 190         |            |  |
| <u>TSP</u> (μg/m³) | 60                        | 54                  | 53      | 49               | 54          |            |  |
| SAMPLE COU         | <u>NT</u> 15ª             | 15 <sup>b</sup>     | 13      | 15               |             |            |  |

<sup>a</sup> For sulfate, the sample count is 0 in the first quarter.
<sup>b</sup> For sulfate, the sample count is 10 in the second quarter.

## **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                                 | TOWN<br>HARTFORD           | ۵<br>۵       | AREA<br>420     |                 | SITE<br>013 |    |
|---------------------------------|----------------------------|--------------|-----------------|-----------------|-------------|----|
|                                 | 1ST                        | QUART<br>2ND | ERLY AVO<br>3RD | <u>3</u><br>4TH | ANNUAL A    | VG |
| METALS (ng/                     | m <sup>3</sup> )           |              |                 |                 |             |    |
| BERYLLIUM                       | <.1                        | <.1          |                 | <.1             |             |    |
| CADMIUM                         | 1.3                        | 4.9          |                 | 8.7             |             |    |
| CHROMIUM                        | 6                          | 5            |                 | 5               |             |    |
| COPPER                          | 60                         | 100          |                 | 80              |             |    |
| IRON                            | 750                        | 790          |                 | 680             |             |    |
| LEAD                            | 240                        | 320          |                 | 120             |             |    |
| MANGANES                        | E 13                       | 19           |                 | 13              |             |    |
| NICKEL                          | 13                         | 6            |                 | 9               |             |    |
| VANADIUM                        | 30                         | 10           |                 | 20              |             |    |
| ZINC                            | 70                         | 50           |                 | 60              |             |    |
|                                 |                            |              |                 |                 |             |    |
| WATER SOLL                      | JBLES (ng/m <sup>3</sup> ) |              |                 |                 |             |    |
| NITRATE                         | 4430                       | 3620         |                 | 2910            |             |    |
| SULFATE                         | 8230                       | 8990         | 19440           | 7040            |             |    |
| AMMONIUM                        | 230                        | 70           |                 | 190             |             |    |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 46                         | 53           |                 | 39              |             |    |
| SAMPLE COL                      | <u>JNT</u> 15              | 16           | ()a             | 14              |             |    |

<sup>a</sup> For sulfate, the sample count is 1 in the third quarter.

## **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                                 | TOWN<br>HARTFORD          | AREA<br>0420 |                |          | SITE<br>014 |            |
|---------------------------------|---------------------------|--------------|----------------|----------|-------------|------------|
|                                 | 1ST                       | QUART<br>2ND | ERLY AV<br>3RD | G<br>4TH | ANNUAL      | <u>AVG</u> |
| METALS (ng/m                    | 1 <sup>3</sup> )          |              |                |          |             |            |
| BERYLLIUM                       | <.1                       | <.1          | <.1            | <.1      | <.1         |            |
| CADMIUM                         | 1.7                       | 1.2          | 0.9            | 1.0      | 1.2         |            |
| CHROMIUM                        | 3                         | 1            | 3              | 2        | 2           |            |
| COPPER                          | 100                       | 120          | 110            | 60       | 100         |            |
| IRON                            | 640                       | 530          | 710            | 570      | 610         |            |
| LEAD                            | 290                       | 170          | 130            | 120      | 180         |            |
| MANGANESE                       | 13                        | 13           | 12             | 12       | 13          |            |
| NICKEL                          | 14                        | 4            | 4              | 7        | 7           |            |
| VANADIUM                        | 50                        | 10           | 10             | 20       | 20          |            |
| ZINC                            | 80                        | 50           | 60             | 50       | 60          |            |
|                                 |                           |              |                |          |             |            |
| WATER SOLU                      | BLES (ng/m <sup>3</sup> ) |              |                |          |             |            |
| NITRATE                         | 4460                      | 3830         | 2770           | 2800     | 3480        |            |
| SULFATE                         | 7890                      | 9270         | 9500           | 7240     | 8500        |            |
| AMMONIUM                        | 210                       | 80           | 110            | 240      | 160         |            |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 53                        | 47           | 46             | 40       | 47          |            |
| SAMPLE COUI                     | <u>NT</u> 14              | 16           | 14             | 14       |             |            |

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## **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

| ר<br>ז                          | FOWN<br>MORRIS           | A<br>0             | REA<br>478     |          | SITE<br>001     |
|---------------------------------|--------------------------|--------------------|----------------|----------|-----------------|
|                                 | 1ST                      | QUARTI<br>2ND      | ERLY AV<br>3RD | G<br>4TH | ANNUAL AVG      |
| METALS (ng/m <sup>3</sup>       | 3)                       |                    |                |          |                 |
| BERYLLIUM                       | <.1                      | <.1                | <.1            | <.1      | <.1             |
| CADMIUM                         | 1.3                      | 1.5                | 2.7            | 0.5      | 1.5             |
| CHROMIUM                        | <sup>,25</sup> <1        | 1                  | 1              | 1        | 1a              |
| COPPER                          | 70                       | 90                 | 90             | 50       | 80              |
| IRON                            | 560                      | 320                | 320            | 160      | 340             |
| LEAD                            | 130                      | 100                | 50             | 30       | 80              |
| MANGANESE                       | 9                        | 10                 | 6              | 5        | 8               |
| NICKEL                          | 4                        | 1                  | 3              | 4        | 3               |
| VANADIUM                        | 10                       | <i>₂.</i> 5<br><10 | <10            | 10       | 10 <sup>b</sup> |
| ZINC                            | 40                       | 20                 | <10            | 20       | 20c             |
|                                 |                          |                    |                |          |                 |
| WATER SOLUB                     | LES (ng/m <sup>3</sup> ) |                    |                |          |                 |
| NITRATE                         | 2830                     | 2350               | 720            | 1600     | 1900            |
| SULFATE                         | 6140                     | 7940               | 8200           | 6120     | 7090            |
| AMMONIUM                        | 90                       | 50                 | 30             | 70       | 60              |
| <u>TSP</u> (µg/m <sup>3</sup> ) | 29                       | 34                 | 30             | 20       | 28              |
| SAMPLE COUN                     | I <u>T</u> 15            | 16                 | 14             | 15       |                 |

<sup>a</sup> The average was calculated using one quarter of the reportable limit in the 1<sup>st</sup> quarter.

<sup>b</sup> The average was calculated using one quarter of the reportable limit in the 2<sup>nd</sup> and 3<sup>rd</sup> quarters. <sup>c</sup> The average was calculated using one quarter of the reportable limit in the 3<sup>rd</sup> quarter.

## **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                                 | TOWN<br>MANCHESTER        | A<br>0!       | AREA<br>0510   |                 | SITE<br>001            |
|---------------------------------|---------------------------|---------------|----------------|-----------------|------------------------|
|                                 | 1ST                       | QUARTE<br>2ND | RLY AVO<br>3RD | <u>G</u><br>4TH | ANNUAL AVG             |
| METALS (ng/m                    | n <sup>3</sup> )          |               |                |                 |                        |
| BERYLLIUM                       | <.1                       | <.1           | <.1            | <.1             | <.1                    |
| CADMIUM                         | 1.2                       | 1.4           | 1.3            | 0.6             | 1.1                    |
| CHROMIUM                        | 2                         | 1             | 4              | 1               | 2                      |
| COPPER                          | 90                        | 80            | 90             | 50              | 80                     |
| IRON                            | 470                       | 410           | 330            | 350             | 390                    |
| LEAD                            | 160                       | 130           | 80             | 70              | 110                    |
| MANGANESE                       | 12                        | 12            | 7              | 9               | 10                     |
| NICKEL                          | 8                         | 3             | 5              | 5               | 5                      |
| VANADIUM                        | 20                        | 10            | < 10           | 10              | 10ª                    |
| ZINC                            | 70                        | 30            | < 10           | 30              | <b>40</b> <sup>b</sup> |
|                                 |                           |               |                |                 |                        |
| WATER SOLU                      | BLES (ng/m <sup>3</sup> ) |               |                |                 |                        |
| NITRATE                         | 3920                      | 2830          | 2190           | 2350            | 2870                   |
| SULFATE                         | 6800                      | 8680          | 9630           | 6890            | 7870                   |
| AMMONIUM                        | 160                       | 110           | 160            | 150             | 140                    |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 45                        | 45            | 36             | 30              | 39                     |
| SAMPLE COU                      | NT 15                     | 14            | 11             | 15              |                        |

<sup>a,b</sup> The average was calculated using one quarter of the reportable limit in the third quarter.

## **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                    | TOWN<br>MERIDEN           | A<br>0        | REA<br>540 |          | SITE<br>002 |    |
|--------------------|---------------------------|---------------|------------|----------|-------------|----|
|                    | 1ST                       | QUARTI<br>2ND | RLY AV     | G<br>4TH | ANNUAL A    | VG |
| METALS (ng/m       | 1 <sup>3</sup> )          |               |            |          |             |    |
| BERYLLIUM          | <.1                       | <.1           | <.1        | <.1      | <.1         |    |
| CADMIUM            | 1.5                       | 1.2           | 2.2        | 2.9      | 1.9         |    |
| CHROMIUM           | 2                         | 2             | 2          | 2        | 2           |    |
| COPPER             | 160                       | 220           | 240        | 140      | 190         |    |
| IRON               | 980                       | 580           | 610        | 490      | 670         |    |
| LEAD               | 280                       | 140           | 120        | 110      | 160         |    |
| MANGANESE          | 16                        | 14            | 11         | 11       | 13          |    |
| NICKEL             | 12                        | 7             | 5          | 10       | 9           |    |
| VANADIUM           | 50                        | 10            | 10         | 20       | 20          |    |
| ZINC               | 190                       | 120           | 150        | 110      | 140         |    |
|                    |                           |               |            |          |             |    |
| WATER SOLU         | BLES (ng/m <sup>3</sup> ) |               |            |          |             |    |
| NITRATE            | 4440                      | 3640          | 2820       | 2410     | 3350        |    |
| SULFATE            | 7890                      | 10170         | 8850       | 7330     | 8580        |    |
| AMMONIUM           | 340                       | 110           | 110        | 320      | 220         |    |
| <u>TSP</u> (µg/m³) | 62                        | 49            | 44         | 39       | 49          |    |
| SAMPLE COU         | <u>NT</u> 15              | 16            | 13         | 15       |             |    |

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## **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                                 | TOWN<br>MIDDLETOWN               | A<br>0!       | REA<br>570     |          | SITE<br>003 |
|---------------------------------|----------------------------------|---------------|----------------|----------|-------------|
|                                 | 1ST                              | QUARTE<br>2ND | RLY AVO<br>3RD | G<br>4TH | ANNUAL AVG  |
| METALS (ng/m                    | 13)                              |               |                |          |             |
| BERYLLIUM                       | <.1                              | <.1           | <.1            | <.1      | <.1         |
| CADMIUM                         | 1.1                              | 1.3           | 0.9            | 1.0      | 1.1         |
| CHROMIUM                        | 2                                | 1             | 2              | 2        | 2           |
| COPPER                          | 90                               | 110           | 70             | 60       | 80          |
| IRON                            | 790                              | 550           | 500            | 450      | 580         |
| LEAD                            | 260                              | 330           | 120            | 100      | 200         |
| MANGANESE                       | 16                               | 15            | 9              | 20       | 15          |
| NICKEL                          | 10                               | 5             | 4              | 8        | 7           |
| VANADIUM                        | 30                               | 10            | <10            | 20       | 20ª         |
| ZINC                            | 100                              | 70            | 10             | 50       | 60          |
| WATER SOLU                      | <u>BLES</u> (ng/m <sup>3</sup> ) |               |                |          |             |
| NITRATE                         | 4070                             | 4170          | 2670           | 2620     | 3390        |
| SULFATE                         | 8240                             | 10020         | 8660           | 7130     | 8510        |
| AMMONIUM                        | 190                              | 100           | 110            | 260      | 170         |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 53                               | 51            | 40             | 39       | 46          |
| SAMPLE COU                      | <u>NT</u> 15                     | 14            | 14             | 14       |             |

<sup>a</sup> The average was calculated using one quarter of the reportable limit in the third quarter.

# **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

| T<br>N                    | 'OWN<br>/IILFORD                | ۲<br>0       | AREA<br>0590   |          | SITE<br>002 |            |  |
|---------------------------|---------------------------------|--------------|----------------|----------|-------------|------------|--|
|                           | 1ST                             | QUART<br>2ND | ERLY AV<br>3RD | G<br>4TH | ANNUAL      | <u>avg</u> |  |
| METALS (ng/m <sup>3</sup> | )                               |              |                |          |             |            |  |
| BERYLLIUM                 | <.1                             | <.1          | <.1            | <.1      | <.1         |            |  |
| CADMIUM                   | 2.7                             | 2.0          | 1.0            | 1.4      | 1.8         |            |  |
| CHROMIUM                  | 2                               | 2            | 3              | 3        | 3           |            |  |
| COPPER                    | 30                              | 60           | 70             | 50       | 50          |            |  |
| IRON                      | 540                             | 590          | 800            | 590      | 630         |            |  |
| LEAD                      | 250                             | 200          | 110            | 110      | 170         |            |  |
| MANGANESE                 | 13                              | 14           | 10             | 10       | 12          |            |  |
| NICKEL                    | 19                              | 18           | 12             | 30       | 20          |            |  |
| VANADIUM                  | 50                              | 40           | 30             | 90       | 50          |            |  |
| ZINC                      | 100                             | 40           | 30             | 60       | 60          |            |  |
| WATER SOLUBL              | <u>_ES</u> (ng/m <sup>3</sup> ) |              |                |          |             |            |  |
| NITRATE                   | 4560                            | 4520         | 3110           | 2440     | 3660        |            |  |
| SULFATE                   | 8860                            | 10290        | 10340          | 9150     | 9660        |            |  |
| AMMONIUM                  | 330                             | 130          | 210            | 260      | 230         |            |  |
| <u>TSP</u> (μg/m³)        | 51                              | 54           | 46             | 42       | 48          |            |  |
| SAMPLE COUNT              | <u> </u>                        | 15           | 15             | 15       |             |            |  |

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|                                 | TOWN<br>NAUGATUCK         | AREA<br>K 0660 |                |          | SITE<br>001 |     |  |
|---------------------------------|---------------------------|----------------|----------------|----------|-------------|-----|--|
|                                 | 1ST                       | QUARTI<br>2ND  | ERLY AV<br>3RD | G<br>4TH | ANNUAL      | AVG |  |
| METALS (ng/m                    | 13)                       |                |                | 4        |             |     |  |
| BERYLLIUM                       | <.1                       | <.1            | <.1            | <.1      | <.1         |     |  |
| CADMIUM                         | 3.3                       | 2.1            | 2.9            | 2.2      | 2.6         |     |  |
| CHROMIUM                        | 3                         | 2              | 4              | 3        | 3           |     |  |
| COPPER                          | 100                       | 100            | 220            | 40       | 110         |     |  |
| IRON                            | 780                       | 620            | 910            | 690      | 750         |     |  |
| LEAD                            | 300                       | 190            | 180            | 170      | 210         |     |  |
| MANGANESE                       | 19                        | 19             | 23             | 15       | 19          |     |  |
| NICKEL                          | 9                         | 4              | 5              | 7        | 6           |     |  |
| VANADIUM                        | 30                        | 10             | 10             | 10       | 20          |     |  |
| ZINC                            | 130                       | 90             | 80             | 90       | 100         |     |  |
| WATER SOLU                      | BLES (ng/m <sup>3</sup> ) |                |                |          |             |     |  |
| NITRATE                         | 4290                      | 4450           | 2490           | 2370     | 3430        |     |  |
| SULFATE                         | 9590                      | 10070          | 10350          | 8260     | 9560        |     |  |
| AMMONIUM                        | 350                       | 110            | 60             | 270      | 200         |     |  |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 54                        | 52             | 51             | 42       | 50          |     |  |
| SAMPLE COUI                     | <u>NT</u> 15              | 16             | 14             | 15       |             | ,   |  |

# **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                                 | TOWN<br>NEW BRITAIN      | AREA<br>0680 |                |          | SITE<br>007 |            |
|---------------------------------|--------------------------|--------------|----------------|----------|-------------|------------|
|                                 | 1ST                      | QUART<br>2ND | ERLY AV<br>3RD | G<br>4TH | ANNUAL .    | <u>AVG</u> |
| <u>METALS</u> (ng/m             | 1 <sup>3</sup> )         |              |                |          |             |            |
| BERYLLIUM                       | <.1                      | <.1          | <.1            | <.1      | <.1         |            |
| CADMIUM                         | 1.1                      | 1.1          | 0.7            | 1.0      | 1.0         |            |
| CHROMIUM                        |                          | 1            | 2              | 2        | ··· 2       |            |
| COPPER                          | 40                       | 60           | 60             | 40       | 50          |            |
| IRON                            | 520                      | 520          | 510            | 420      | 500         |            |
| LEAD                            | 190                      | 130          | 100            | 80       | 130         |            |
| MANGANESE                       | 10                       | 12           | 10             | 11       | 11          |            |
| NICKEL                          | 10                       | 7            | 5              | 7        | 7           |            |
| VANADIUM                        | 30                       | 10           | 10             | 20       | 20          |            |
| ZINC                            | 60                       | 50           | 10             | 30       | 40          |            |
|                                 |                          |              |                |          |             |            |
| WATER SOLU                      | BLES (ng/m <sup>3)</sup> |              |                |          |             |            |
| NITRATE                         | 4200                     | 3880         | 2740           | 2540     | 3380        |            |
| SULFATE                         | 7900                     | 9610         | 9130           | 7100     | 8500        |            |
| AMMONIUM                        | 340                      | 60           | 100            | 240      | 180         |            |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 45                       | 43           | 38             | 35       | 40          |            |
| SAMPLE COU                      | <u>NT</u> 15             | 16           | 15             | 13       |             |            |

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|                                 | TOWN<br>NEW BRITAIN             | AREA<br>ITAIN 0680 |                |          | SITE<br>008 |            |  |
|---------------------------------|---------------------------------|--------------------|----------------|----------|-------------|------------|--|
|                                 | 1ST                             | QUARTI<br>2ND      | ERLY AV<br>3RD | G<br>4TH | ANNUAL      | <u>4VG</u> |  |
| METALS (ng/m                    | 3)                              |                    |                |          |             |            |  |
| BERYLLIUM                       | <.1                             | <.1                | <.1            | <.1      | <.1         |            |  |
| CADMIUM                         | 1.1                             | 1.3                | 0.8            | 0.7      | 1.0         |            |  |
| CHROMIUM                        | 2                               | 1                  | 2              | 2        | 2           |            |  |
| COPPER                          | 210                             | 160                | 180            | 120      | 170         |            |  |
| IRON                            | 510                             | 500                | 650            | 440      | 530         |            |  |
| LEAD                            | 210                             | 140                | 110            | 100      | 140         |            |  |
| MANGANESE                       | 9                               | 12                 | 10             | 10       | 10          |            |  |
| NICKEL                          | 8                               | 6                  | 5              | 6        | 6           |            |  |
| VANADIUM                        | 30                              | 10                 | 10             | 10       | 10          |            |  |
| ZINC                            | 70                              | 40                 | 20             | 30       | 40          |            |  |
|                                 |                                 |                    |                |          |             |            |  |
| WATER SOLU                      | <u>BLES</u> (ng/m <sup>3)</sup> |                    |                |          |             |            |  |
| NITRATE                         | 3760                            | 4000               | 2050           | 2540     | 3100        |            |  |
| SULFATE                         | 6630                            | 9270               | 9430           | 6740     | 8090        |            |  |
| AMMONIUM                        | 220                             | 130                | 110            | 220      | 170         |            |  |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 42                              | 43                 | 42             | 34       | 40          |            |  |
| SAMPLE COUI                     | <u>NT</u> 14                    | 16                 | 15             | 14       |             |            |  |

|                                 | TOWN<br>NEW BRITAIN      | AREA<br>0680  |                 |          | SITE<br>009 |    |
|---------------------------------|--------------------------|---------------|-----------------|----------|-------------|----|
|                                 | 1ST                      | QUARTI<br>2ND | ERLY AVO<br>3RD | G<br>4TH | ANNUAL A    | VG |
| METALS (ng/n                    | n <sup>3</sup> )         |               |                 |          |             |    |
| BERYLLIUM                       | <.1                      | <.1           | <.1             | <.1      | <.1         |    |
| CADMIUM                         | 1.0                      | 1.0           | 0.8             | 1.7      | 1.1         |    |
| CHROMIUM                        | 1                        | 1             | 2               | 2        | 1           |    |
| COPPER                          | 50                       | 110           | 160             | 90       | 100         |    |
| IRON                            | 380                      | 370           | 600             | 390      | 430         |    |
| LEAD                            | 150                      | 100           | 100             | 70       | 110         |    |
| MANGANESE                       | 9                        | 11            | 10              | 9        | 10          |    |
| NICKEL                          | 7                        | 3             | 4               | 6        | 5           |    |
| VANADIUM                        | 30                       | 10            | 10              | 20       | 20          |    |
| ZINC                            | 50                       | 40            | 30              | 40       | 40          |    |
| WATER SOLU                      | BLES (ng/m <sup>3)</sup> |               |                 |          |             |    |
| NITRATE                         | 3520                     | 3500          | 2270            | 2500     | 2970        |    |
| SULFATE                         | 6930                     | 8600          | 8600            | 6500     | 7670        |    |
| AMMONIUM                        | 360                      | 140           | 180             | 310      | 250         |    |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 37                       | 41            | 39              | 32       | 37          |    |
| SAMPLE COU                      | <u>NT</u> 15             | 14            | 14              | 13       |             |    |

|                                 | TOWN<br>NEW HAVEN        | AREA<br>0700 |         |          | SITE<br>002 |    |
|---------------------------------|--------------------------|--------------|---------|----------|-------------|----|
|                                 | 1ST                      | QUART<br>2ND | ERLY AV | G<br>4TH | ANNUAL A    | VG |
| METALS (ng/m                    | 13)                      |              |         |          |             |    |
| BERYLLIUM                       | <.1                      | <.1          | <.1     | <.1      | <.1         |    |
| CADMIUM                         | 1.4                      | 2.0          | 0.9     | 1.6      | 1.5         |    |
| CHROMIUM                        | 2                        | 2            | 3       | 3        | 2           |    |
| COPPER                          | 250                      | 370          | 340     | 110      | 270         |    |
| IRON                            | 570                      | 800          | 1030    | 580      | 740         |    |
| LEAD                            | 320                      | 200          | 170     | 130      | 210         |    |
| MANGANESE                       | 12                       | 16           | 14      | 12       | 13          |    |
| NICKEL                          | 9                        | 13           | 10      | 14       | 11          |    |
| VANADIUM                        | 50                       | 20           | 20      | 40       | 30          |    |
| ZINC                            | 80                       | 50           | 40      | 50       | 60          |    |
|                                 |                          |              |         |          |             |    |
| WATER SOLU                      | BLES (ng/m <sup>3)</sup> |              |         |          |             |    |
| NITRATE                         | 4150                     | 3690         | 3340    | 3140     | 3610        |    |
| SULFATE                         | 8170                     | 8950         | 11430   | 7200     | 8940        |    |
| AMMONIUM                        | 360                      | 90           | 280     | 410      | 290         |    |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 59                       | 53           | 56      | 42       | 53          |    |
| SAMPLE COU                      | <u>NT</u> 15             | 13           | 13      | 12       |             |    |

#### **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                                 | TOWN<br>NEW HAVEN         | AREA<br>0700  |                |                 | SITE<br>013 |     |
|---------------------------------|---------------------------|---------------|----------------|-----------------|-------------|-----|
|                                 | 1ST                       | QUARTI<br>2ND | ERLY AV<br>3RD | <u>G</u><br>4TH | ANNUAL      | AVG |
| METALS (ng/m                    | 1 <sup>3</sup> )          |               |                |                 |             |     |
| BERYLLIUM                       | <.1                       | <.1           | <.1            | <.1             | <.1         |     |
| CADMIUM                         | 1.6                       | 1.4           | 1.2            | 1.0             | 1.3         |     |
| CHROMIUM                        | 3                         | 1             | 3              | 2               | 2           |     |
| COPPER                          | 30                        | 40            | 30             | 70              | 40          |     |
| IRON                            | 610                       | 700           | 660            | 590             | 640         |     |
| LEAD                            | 270                       | 170           | 120            | 100             | 170         |     |
| MANGANESE                       | 13                        | 13            | 10             | 11              | 12          |     |
| NICKEL                          | 22                        | 10            | 10             | 11              | 13          |     |
| VANADIUM                        | 60                        | 20            | 30             | 30              | 40          |     |
| ZINC                            | 70                        | 50            | 20             | 50              | 50          |     |
| WATER SOLU                      | BLES (ng/m <sup>3</sup> ) |               |                |                 |             |     |
| NITRATE                         | 4410                      | 4620          | 2920           | 2250            | 3660        |     |
| SULFATE                         | 8410                      | 9910          | 10060          | 6470            | 8850        |     |
| AMMONIUM                        | 430                       | 110           | 320            | 320             | 290         |     |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 52                        | 51            | 45             | 43              | 48          |     |
| SAMPLE COUI                     | <u>NT</u> 15              | 16            | 13             | 12ª             |             |     |

<sup>a</sup> For sulfate, the sample count is 11 in the fourth quarter.

## **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                                 | TOWN<br>NORWALK                  | AREA<br>0820  |        |          | SITE<br>001 |            |
|---------------------------------|----------------------------------|---------------|--------|----------|-------------|------------|
|                                 | 1ST                              | QUARTE<br>2ND | RLY AV | G<br>4TH | ANNUAL      | <u>AVG</u> |
| <u>METALS</u> (ng/m             | 3)                               |               |        |          |             |            |
| BERYLLIUM                       | <.1                              | <.1           | <.1    | <.1      | <.1         |            |
| CADMIUM                         | 2.2                              | 1.4           | 1.1    | 0.8      | 1.4         |            |
| CHROMIUM                        | 2                                | 1             | 2      | 1        | 2           |            |
| COPPER                          | 50                               | 50            | 180    | 80       | 80          |            |
| IRON                            | 550                              | 800           | 460    | 350      | 550         |            |
| LEAD                            | 190                              | 170           | 90     | 70       | 130         |            |
| MANGANESE                       | 13                               | 18            | 8      | 8        | 12          |            |
| NICKEL                          | 13                               | 8             | 6      | 7        | 9           |            |
| VANADIUM                        | 40                               | 20            | 10     | 20       | 20          |            |
| ZINC                            | 100                              | 90            | 50     | 70       | 80          |            |
|                                 |                                  |               |        |          |             |            |
| WATER SOLU                      | <u>BLES</u> (ng/m <sup>3</sup> ) |               |        |          |             |            |
| NITRATE                         | 3790                             | 4720          | 2790   | 2210     | 3450        |            |
| SULFATE                         | 8550                             | 10070         | 9680   | 7720     | 8980        |            |
| AMMONIUM                        | 220                              | 40            | 30     | 110      | 110         |            |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 48                               | 56            | 40     | 32       | 45          |            |
| SAMPLE COUL                     | <u>NT</u> 14                     | 14            | 10     | 13       |             |            |

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# **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

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|                    | TOWN<br>NORWALK                  | Д<br>С       | AREA<br>1820   |                  | SITE<br>005 |            |
|--------------------|----------------------------------|--------------|----------------|------------------|-------------|------------|
|                    | 1ST                              | QUART<br>2ND | ERLY AV<br>3RD | <u>'G</u><br>4TH | ANNUAL      | <u>AVG</u> |
| METALS (ng/m       | 1 <sup>3</sup> )                 |              |                |                  |             |            |
| BERYLLIUM          | <.1                              | <.1          | <.1            | <.1              | <.1         |            |
| CADMIUM            | 2.1                              | 1.4          | 1.2            | 0.8              | 1.3         |            |
| CHROMIUM           | 3                                | 1            | 2              | 2                | 2           |            |
| COPPER             | 50                               | 90           | 130            | 80               | 90          |            |
| IRON               | 760                              | 770          | 600            | 760              | 720         |            |
| LEAD               | 260                              | 170          | 130            | 100              | 160         |            |
| MANGANESE          | 15                               | 16           | 11             | 13               | 14          |            |
| NICKEL             | 25                               | 6            | 8              | 8                | 11          |            |
| VANADIUM           | 90                               | 10           | 10             | 20               | . 30        |            |
| ZINC               | 110                              | 50           | 40             | 70               | 60          |            |
| WATER SOLUE        | <u>3LES</u> (ng/m <sup>3</sup> ) |              |                |                  |             |            |
| NITRATE            | 4080                             | 3930         | 3120           | 2390             | 3370        |            |
| SULFATE            | 8470                             | 8990         | 9910           | 7270             | 8700        |            |
| AMMONIUM           | 320                              | 50           | 80             | 160              | 140         |            |
| <u>TSP</u> (µg/m³) | 59                               | 55           | 44             | 44               | 50          |            |
| SAMPLE COUN        | <u>NT</u> 12                     | 16           | 15             | 14               |             |            |

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# **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                    | TOWN<br>NORWALK           | A<br>0        | AREA<br>0820 |          | SITE<br>012 |          |  |
|--------------------|---------------------------|---------------|--------------|----------|-------------|----------|--|
|                    | <u>15T</u>                | QUARTI<br>2ND | ERLY AV      | G<br>4TH | ANNUAL A    | <u> </u> |  |
| METALS (ng/m       | 3)                        |               |              |          |             |          |  |
| BERYLLIUM          | <.1                       | <.1           | <.1          | <.1      | <.1         |          |  |
| CADMIUM            | 1.9                       | 3.2           | 1.5          | 3.3      | 2.5         |          |  |
| CHROMIUM           | 2                         | 1             | 2            | 2        | 2           |          |  |
| COPPER             | 70                        | 100           | 110          | 40       | 80          |          |  |
| IRON               | 620                       | 780           | 700          | 450      | 640         |          |  |
| LEAD               | 240                       | 160           | 140          | 80       | 160         |          |  |
| MANGANESE          | 11                        | 18            | 11           | 10       | 13          |          |  |
| NICKEL             | 11                        | 6             | 8            | 6        | 8           |          |  |
| VANADIUM           | 30                        | 10            | 10           | 10       | 20          |          |  |
| ZINC               | 70                        | 70            | 40           | 50       | 60          |          |  |
|                    |                           |               |              |          |             |          |  |
| WATER SOLU         | BLES (ng/m <sup>3</sup> ) |               |              |          |             |          |  |
| NITRATE            | 4310                      | 6330          | 3030         | 2560     | 4080        |          |  |
| SULFATE            | 7860                      | 8460          | 10260        | 7270     | 8480        |          |  |
| AMMONIUM           | 170                       | 50            | 120          | 190      | 130         |          |  |
| <u>TSP</u> (μg/m³) | 48                        | 50            | 43           | 35       | 44          |          |  |
| SAMPLE COU         | <u>NT</u> 15              | 15            | 15           | 14       |             |          |  |

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# **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                                 | TOWN<br>NORWICH           | ۵<br>0       | AREA<br>840    |          | SITE<br>002 |
|---------------------------------|---------------------------|--------------|----------------|----------|-------------|
|                                 | 1ST                       | QUART<br>2ND | ERLY AV<br>3RD | G<br>4TH | ANNUAL AVG  |
| METALS (ng/m                    | 1 <sup>3</sup> )          |              |                |          |             |
| BERYLLIUM                       | <.1                       | <.1          | <.1            | <.1      | <.1         |
| CADMIUM                         | 1.3                       | 1.0          | 4.5            | 0.7      | 1.8         |
| CHROMIUM                        | 2                         | <1           | 5              | 2        | 2a.         |
| COPPER                          | 180                       | 280          | 310            | 160      | 230         |
| IRON                            | 580                       | 540          | 1050           | 490      | 660         |
| LEAD                            | 200                       | 130          | 200            | 90       | 150         |
| MANGANESE                       | 10                        | 12           | 15             | 9        | 11          |
| NICKEL                          | 8                         | 9            | 9              | 6        | 8           |
| VANADIUM                        | 20                        | 20           | 20             | 10       | 20          |
| ZINC                            | 60                        | 50           | 60             | 40       | 50          |
| WATER SOLU                      | BLES (ng/m <sup>3</sup> ) |              |                |          |             |
| NITRATE                         | 3890                      | 3440         | 2420           | 2590     | 3100        |
| SULFATE                         | 6970                      | 8710         | 9790           | 7560     | 8190        |
| AMMONIUM                        | 200                       | 50           | 60             | 240      | 140         |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 53                        | 46           | 69             | 45       | 53          |
| SAMPLE COUI                     | <u>NT</u> 15              | 13           | 13             | 15       |             |

 $\left( \ldots \right)$ 

<sup>a</sup> The average was calculated using one quarter of the reportable limit in the second quarter.

|                                 | TOWN<br>STAMFORD           | ۲<br>1       | AREA<br>1080   |          | SITE<br>001 |            |
|---------------------------------|----------------------------|--------------|----------------|----------|-------------|------------|
|                                 | 1ST                        | QUART<br>2ND | ERLY AV<br>3RD | G<br>4TH | ANNUAL A    | <u>۱VG</u> |
| METALS (ng/r                    | m <sup>3</sup> )           |              |                |          |             |            |
| BERYLLIUM                       | <.1                        | <.1          | <.1            | <.1      | <.1         |            |
| CADMIUM                         | 1.3                        | 1.8          | 1.6            | 0.8      | 1.4         |            |
| CHROMIUM                        | 1                          | 1            | 3              | 2        | 2           |            |
| COPPER                          | 60                         | 230          | 150            | 150      | 150         |            |
| IRON                            | 530                        | 1360         | 990            | 590      | 870         |            |
| LEAD                            | 190                        | 180          | 130            | 90       | 150         |            |
| MANGANESE                       | 12                         | 29           | 17             | 14       | 18          |            |
| NICKEL                          | 13                         | 8            | 9              | 10       | 10          |            |
| VANADIUM                        | 40                         | 10           | 10             | 20       | 20          |            |
| ZINC                            | 80                         | 80           | 50             | 60       | 70          |            |
|                                 |                            |              |                |          |             |            |
| WATER SOLU                      | JBLES (ng/m <sup>3</sup> ) |              |                |          |             |            |
| NITRATE                         | 4180                       | 5090         | 3270           | 2740     | 3790        |            |
| SULFATE                         | 7540                       | 9440         | 9450           | 7510     | 8480        |            |
| AMMONIUM                        | 170                        | 60           | 40             | 180      | 110         |            |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 56                         | 75           | 60             | 54       | 61          |            |
| SAMPLE COU                      | INT 13                     | 14           | 14             | 15       |             |            |

|                    | TOWN<br>STAMFORD          | <u>م</u><br>1 | REA<br>080     |          | SITE<br>007 |    |
|--------------------|---------------------------|---------------|----------------|----------|-------------|----|
|                    | 1ST                       | QUART<br>2ND  | ERLY AV<br>3RD | G<br>4TH | ANNUAL A    | VG |
| METALS (ng/m       | 1 <sup>3</sup> )          |               |                |          |             |    |
| BERYLLIUM          | <.1                       | <.1           | <.1            | <.1      | <.1         |    |
| CADMIUM            | 2.3                       | 2.5           | 2.2            | 2.4      | 2.4         |    |
| CHROMIUM           | 1                         | 1             | 3              | 2        | 2           |    |
| COPPER             | 140                       | 170           | 90             | 50       | 110         |    |
| IRON               | 390                       | 660           | 650            | 630      | 590         |    |
| LEAD               | 240                       | 150           | 120            | 120      | 160         |    |
| MANGANESE          | 12                        | 18            | 15             | 16       | 15          |    |
| NICKEL             | 14                        | 8             | 8              | 9        | 10          |    |
| VANADIUM           | 40                        | 10            | 10             | 20       | 20          |    |
| ZINC               | 120                       | 130           | 100            | 180      | 130         |    |
|                    |                           |               |                |          |             |    |
| WATER SOLU         | BLES (ng/m <sup>3</sup> ) |               |                |          |             |    |
| NITRATE            | 4000                      | 4910          | 3510           | 3290     | 3940        |    |
| SULFATE            | 7140                      | 9780          | 11000          | 8040     | 9040        |    |
| AMMONIUM           | 160                       | 70            | 160            | 240      | 160         |    |
| <u>TSP</u> (μg/m³) | 44                        | 55            | 50             | 51       | 50          |    |
| SAMPLE COU         | <u>NT</u> 14              | 15            | 15             | 14       |             |    |

|                                 | TOWN<br>STAMFORD                 | A<br>1        | AREA<br>1080   |          | SITE<br>021 | -  |  |
|---------------------------------|----------------------------------|---------------|----------------|----------|-------------|----|--|
|                                 | 1ST                              | QUARTI<br>2ND | ERLY AV<br>3RD | G<br>4TH | ANNUAL A    | VG |  |
| <u>METALS</u> (ng/m             | 3)                               |               |                |          |             |    |  |
| BERYLLIUM                       | <.1                              | <.1           | <.1            | <.1      | <.1         |    |  |
| CADMIUM                         | 2.3                              | 3.1           | 0.9            | 1.2      | 1.9         |    |  |
| CHROMIUM                        | 2                                | 1             | 3              | 2        | 2           |    |  |
| COPPER                          | 160                              | 170           | 130            | 40       | 120         |    |  |
| IRON                            | 570                              | 650           | 420            | 790      | 620         |    |  |
| LEAD                            | 220                              | 180           | 100            | 120      | 150         |    |  |
| MANGANESE                       | 12                               | 15            | 11             | 11       | 12          |    |  |
| NICKEL                          | 17                               | 6             | 8              | 10       | 10          |    |  |
| VANADIUM                        | 50                               | 10            | 10             | 10       | 20          |    |  |
| ZINC                            | 90                               | 70            | 40             | 70       | 70          |    |  |
| WATER SOLUE                     | <u>BLES</u> (ng/m <sup>3</sup> ) |               |                |          |             |    |  |
| NITRATE                         | 4520                             | 4720          | 3770           | 3400     | 4090        |    |  |
| SULFATE                         | 7250                             | 9270          | 9460           | 7540     | 8370        |    |  |
| AMMONIUM                        | 250                              | 70            | 50             | 230      | 150         |    |  |
| <u>TSP</u> (µg/m <sup>3</sup> ) | 50                               | 53            | 45             | 43       | 48          |    |  |
| SAMPLE COUN                     | <u>NT</u> 12                     | 14            | 12             | 15       |             |    |  |

|                    | TOWN<br>STRATFORD     | Д<br>1        | REA<br>110     |          | SITE<br>005 |            |  |
|--------------------|-----------------------|---------------|----------------|----------|-------------|------------|--|
|                    | 1ST                   | QUARTI<br>2ND | ERLY AV<br>3RD | G<br>4TH | ANNUAL A    | <u>.VG</u> |  |
| METALS (ng/r       | m <sup>3</sup> )      |               |                |          |             |            |  |
| BERYLLIUM          | <.1                   | <.1           | <.1            | <.1      | <.1         |            |  |
| CADMIUM            | 2.1                   | 2.8           | 1.1            | 1.1      | 1.8         |            |  |
| CHROMIUM           | 5                     | 2             | 2              | 3        | 3           |            |  |
| COPPER             | 180                   | 160           | 200            | 140      | 170         |            |  |
| IRON               | 830                   | 660           | 500            | 510      | 630         |            |  |
| LEAD               | 360                   | 260           | 140            | 160      | 230         |            |  |
| MANGANESE          | 14                    | 15            | 9              | 11       | 12          |            |  |
| NICKEL             | 20                    | 10            | 6              | 9        | 11          |            |  |
| VANADIUM           | 60                    | 20            | 20             | 20       | 30          |            |  |
| ZINC               | 150                   | 70            | 30             | 50       | 80          |            |  |
| WATER SOLU         | I <u>BLES</u> (ng/m³) |               |                |          |             |            |  |
| NITRATE            | 4750                  | 3660          | 2910           | 2860     | 3560        |            |  |
| SULFATE            | 8650                  | 9340          | 9690           | 7710     | 8830        |            |  |
| AMMONIUM           | 300                   | 80            | 260            | 250      | 220         |            |  |
| <u>TSP</u> (μg/m³) | 61                    | 50            | 40             | 40       | 48          |            |  |
| SAMPLE COU         | <u>INT</u> 15         | 15            | 14             | 15       |             |            |  |

|                    | TOWN<br>TORRINGTON               | A<br>1        | REA<br>160     |          | SITE<br>001 |            |
|--------------------|----------------------------------|---------------|----------------|----------|-------------|------------|
|                    | 1ST                              | QUARTI<br>2ND | ERLY AV<br>3RD | G<br>4TH | ANNUAL A    | <u>.VG</u> |
| METALS (ng/m       | 1 <sup>3</sup> )                 |               |                |          |             |            |
| BERYLLIUM          | <.1                              | <.1           | <.1            | <.1      | <.1         |            |
| CADMIUM            | 0.9                              | 1.5           | 0.7            | 0.8      | 1.0         |            |
| CHROMIUM           | 3                                | 2             | 2              | 2        | 2           |            |
| COPPER             | 120                              | 120           | 50             | 40       | 80          |            |
| IRON               | 870                              | 490           | 480            | 400      | 560         |            |
| LEAD               | 290                              | 140           | 80             | 80       | 150         |            |
| MANGANESE          | 13                               | 12            | 8              | 8        | 10          |            |
| NICKEL             | 10                               | . 3           | 4              | 5        | 5           |            |
| VANADIUM           | 30                               | 10            | 10             | 10       | 20          |            |
| ZINC               | 80                               | 40            | 10             | 30       | 40          |            |
|                    |                                  |               |                |          |             |            |
| WATER SOLU         | <u>BLES</u> (ng/m <sup>3</sup> ) |               |                |          |             |            |
| NITRATE            | 3880                             | 3120          | 1710           | 1990     | 2700        |            |
| <b>S</b> ULFATE    | 7430                             | 8780          | 8110           | 7310     | 7920        |            |
| AMMONIUM           | 190                              | 90            | 160            | 150      | 150         |            |
| <u>TSP</u> (µg/m³) | 57                               | 42            | 40             | 33       | 43          |            |
| SAMPLE COU         | <u>NT</u> 15                     | 16            | 14             | 15       |             |            |

### **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                                 | TOWN<br>VOLUNTOWN                | Д<br>1        | REA<br>205 |                 | SITE<br>001     |
|---------------------------------|----------------------------------|---------------|------------|-----------------|-----------------|
|                                 | 1ST                              | QUARTI<br>2ND | ERLY AV    | <u>G</u><br>4TH | ANNUAL AVG      |
| METALS (ng/m                    | 1 <sup>3</sup> )                 |               |            |                 |                 |
| BERYLLIUM                       | <.1                              | <.1           | <.1        | <.1             | <.1             |
| CADMIUM                         | 0.8                              | 1.3           | 1.4        | 0.7             | 1.1             |
| CHROMIUM                        | <1                               | <1            | 1          | 2               | 1a              |
| COPPER                          | 210                              | 180           | 80         | 40              | 130             |
| IRON                            | 130                              | 180           | 340        | 130             | 190             |
| LEAD                            | 70                               | 40            | 30         | 30              | 40              |
| MANGANESE                       | 3                                | 6             | 4          | 3               | 4               |
| NICKEL                          | 3                                | 4             | 2          | 3               | 3               |
| VANADIUM                        | 10                               | 10            | <10        | <10             | 10 <sup>b</sup> |
| ZINC                            | 70                               | 30            | <10        | 20              | <b>30</b> c     |
|                                 |                                  |               |            |                 |                 |
| WATER SOLU                      | <u>BLES</u> (ng/m <sup>3</sup> ) |               |            |                 |                 |
| NITRATE                         | 3110                             | 2090          | 1590       | 1910            | 2210            |
| SULFATE                         | 6300                             | 7280          | 7570       | 5190            | 6630            |
| AMMONIUM                        | 30                               | 10            | 70         | 50              | 40              |
| <u>TSP</u> (µg/m <sup>3</sup> ) | 23                               | 32            | 26         | 19              | 25              |
| SAMPLE COUI                     | <u>NT</u> 15                     | 16            | 13         | 12              |                 |

<sup>a</sup> The average was calculated using one quarter of the reportable limit in the 1<sup>st</sup> and 2<sup>nd</sup> quarters. <sup>b</sup> The average was calculated using one quarter of the reportable limit in the 3<sup>rd</sup> and 4<sup>th</sup> quarters. <sup>c</sup> The average was calculated using one quarter of the reportable limit in the 3<sup>rd</sup> quarter.

|                                 |                           | A<br>) 1      | AREA<br>1210   |                 | SITE<br>001 |     |
|---------------------------------|---------------------------|---------------|----------------|-----------------|-------------|-----|
|                                 | 1ST                       | QUARTI<br>2ND | ERLY AV<br>3RD | <u>G</u><br>4TH | ANNUAL A    | ١VG |
| METALS (ng/m                    | n <sup>3</sup> )          |               |                |                 |             |     |
| BERYLLIUM                       | <.1                       | <.1           | <.1            | <.1             | <.1         |     |
| CADMIUM                         | 1.3                       | 2.3           | 1.3            | 1.0             | 1.5         |     |
| CHROMIUM                        | 4                         | 1             | 2              | 3               | 3           |     |
| COPPER                          | 100                       | 90            | 50             | 40              | 70          |     |
| IRON                            | 840                       | 750           | 530            | 540             | 670         |     |
| LEAD                            | 260                       | 160           | 100            | 100             | 160         |     |
| MANGANESE                       | 12                        | 14            | 9              | 16              | 13          |     |
| NICKEL                          | 13                        | 10            | 5              | 10              | 10          |     |
| VANADIUM                        | 40                        | 20            | 10             | 20              | 20          |     |
| ZINC                            | 80                        | 50            | 20             | 60              | 50          |     |
|                                 |                           |               |                |                 |             |     |
| WATER SOLU                      | BLES (ng/m <sup>3</sup> ) |               |                |                 |             |     |
| NITRATE                         | 4540                      | 3870          | 2060           | 2630            | 3280        |     |
| SULFATE                         | 8250                      | 10080         | 10050          | 7740            | 9030        |     |
| AMMONIUM                        | 270                       | 100           | 100            | 340             | 200         |     |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 61                        | 48            | 41             | 41              | 48          |     |
| SAMPLE COU                      | NT 15                     | 15            | 15             | 15              |             |     |

# **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                    | TOWN<br>WATERBURY         | A<br>12       | REA<br>240    |                 | SITE<br>005 |            |
|--------------------|---------------------------|---------------|---------------|-----------------|-------------|------------|
|                    | 1ST                       | QUARTE<br>2ND | RLY AV<br>3RD | <u>G</u><br>4TH | ANNUAL A    | <u>avg</u> |
| METALS (ng/m       | 13)                       |               |               |                 |             |            |
| BERYLLIUM          | <.1                       | <.1           | <.1           | <.1             | <.1         |            |
| CADMIUM            | 4.2                       | 3.1           | 2.6           | 1.3             | 2.8         |            |
| CHROMIUM           | 12                        | 5             | 6             | 6               | 7           |            |
| COPPER             | 120                       | 140           | 140           | 70              | 120         |            |
| IRON               | 650                       | 530           | 520           | 480             | 550         |            |
| LEAD               | 290                       | 170           | 130           | 120             | 180         |            |
| MANGANESE          | 13                        | 14            | 9             | 11              | 12          |            |
| NICKEL             | 13                        | 5             | 5             | 8               | 8           |            |
| VANADIUM           | 40                        | 10            | 10            | 20              | 20          |            |
| ZINC               | 210                       | 120           | 180           | 140             | 160         |            |
|                    |                           |               |               |                 |             |            |
| WATER SOLU         | BLES (ng/m <sup>3</sup> ) |               |               |                 |             |            |
| NITRATE            | 4430                      | 3650          | 2350          | 2900            | 3330        |            |
| SULFATE            |                           | 8570          | 979 <b>0</b>  | 7450            |             |            |
| AMMONIUM           | 340                       | 100           | 190           | 390             | 260         |            |
| <u>TSP</u> (μg/m³) | 59                        | 46            | 43            | 41              | 47          |            |
| SAMPLE COU         | <u>NT</u> 14ª             | <b>14</b> b   | 14            | 14              |             |            |

<sup>a</sup> For sulfate, the sample count is 0 in the first quarter . <sup>b</sup> For sulfate, the sample count is 10 in the second quarter .

|                                 | TOWN<br>WATERBURY                | <u>م</u><br>1 | AREA<br>240    |          | SITE<br>006 |            |
|---------------------------------|----------------------------------|---------------|----------------|----------|-------------|------------|
|                                 | 1ST                              | QUART<br>2ND  | ERLY AV<br>3RD | G<br>4TH | ANNUAL      | <u>AVG</u> |
| METALS (ng/m                    | 13)                              |               |                |          |             |            |
| BERYLLIUM                       | <.1                              | <.1           | <.1            | <.1      | <.1         |            |
| CADMIUM                         | 1.6                              | 1.0           | 1.6            | 0.8      | 1.3         |            |
| CHROMIUM                        | 11                               | 4             | 3              | 4        | 6           |            |
| COPPER                          | 210                              | 160           | 220            | 140      | 180         |            |
| IRON                            | 420                              | 450           | 370            | 300      | 390         |            |
| LEAD                            | 170                              | 130           | 100            | 70       | 120         |            |
| MANGANESE                       | 10                               | 12            | 7              | 7        | 9           |            |
| NICKEL                          | 9                                | 3             | 5              | 6        | 6           |            |
| VANADIUM                        | 30                               | 10            | 10             | 20       | 20          |            |
| ZINC                            | 120                              | 140           | 80             | 70       | 100         |            |
| WATER SOLUI                     | <u>3LES</u> (ng/m <sup>3</sup> ) |               |                |          |             |            |
| NITRATE                         | 4830                             | 4510          | 1950           | 3100     | 3610        |            |
| SULFATE                         | 8790                             | 9680          | 9000           | 7640     | 8790        |            |
| AMMONIUM                        | 450                              | 100           | 110            | 360      | 250         |            |
| <u>TSP</u> (μg/m <sup>3</sup> ) | 45                               | 45            | 34             | 31       | 39          |            |
| SAMPLE COUN                     | <u>NT</u> 15                     | 15            | 15             | 14       |             |            |

# **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|   |                    | TOWN<br>WATERBURY | Д<br>1        | REA<br>240 |          | SITE<br>007 |    |
|---|--------------------|-------------------|---------------|------------|----------|-------------|----|
|   |                    | 1ST               | QUARTI<br>2ND | ERLY AV    | G<br>4TH | ANNUAL A    | VG |
|   | METALS (ng/        | m <sup>3</sup> )  |               |            |          |             |    |
|   | BERYLLIUM          | <.1               | <.1           | <.1        | <.1      | <.1         |    |
|   | CADMIUM            | 3.3               | 3.7           | 2.4        | 1.5      | 2.7         |    |
|   | CHROMIUM           | 9                 | 7             | 9          | 7        | 8           |    |
|   | COPPER             | 290               | 260           | 180        | 60       | 200         |    |
|   | IRON               | 990               | 710           | 630        | 760      | 770         |    |
|   | LEAD               | 340               | 200           | 170        | 170      | 220         |    |
|   | MANGANESE          | 19                | 15            | 11         | 14       | 15          |    |
|   | NICKEL             | 15                | 6             | 5          | 11       | 9           |    |
|   | VANADIUM           | 50                | 10            | 10         | 30       | 30          |    |
|   | ZINC               | 180               | 130           | 160        | 130      | 150         |    |
|   | WATER SOLU         | IBLES (ng/m³)     |               |            |          |             |    |
|   | NITRATE            | 4610              | 4390          | 2240       | 3090     | 3620        |    |
|   | SULFATE            | 9700              | 9630          | 9900       | 7920     | 9280        |    |
|   | AMMONIUM           | 410               | 170           | 150        | 340      | 270         |    |
| ( | <u>TSP</u> (μg/m³) | 72                | 55            | 47         | 50       | 56          |    |
|   | SAMPLE COU         | <u>NT</u> 15      | 16            | 14         | 15       |             |    |

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### **QUARTERLY CHEMICAL CHARACTERIZATION OF 1985 HI-VOL TSP**

|                    | TOWN<br>WILLIMANTIC       | ۵<br>1       | AREA<br>410    |          | SITE<br>002 |           |
|--------------------|---------------------------|--------------|----------------|----------|-------------|-----------|
|                    | 1ST                       | QUART<br>2ND | ERLY AV<br>3RD | <u>G</u> | ANNUAL AN   | <u>/G</u> |
| METALS (ng/r       | n <sup>3</sup> )          |              |                |          |             |           |
| BERYLLIUM          | <.1                       | <.1          | <.1            | <.1      | <.1         |           |
| CADMIUM            | 1.0                       | 0.5          | 0.9            | 1.0      | 0.8         |           |
| CHROMIUM           | 2                         | <1           | 2              | 1        | 1ª          |           |
| COPPER             | 50                        | 70           | 70             | 40       | 60          |           |
| IRON               | 710                       | 320          | 340            | 430      | 450         |           |
| LEAD               | 190                       | 110          | 80             | 90       | 120         |           |
| MANGANESE          | 10                        | 8            | 5              | 7        | 8           |           |
| NICKEL             | 19                        | 6            | 10             | 19       | 13          |           |
| VANADIUM           | 90                        | 20           | 40             | 40       | 50          |           |
| ZINC               | 60                        | 40           | 10             | 40       | 40          |           |
|                    |                           |              |                |          |             |           |
| WATER SOLU         | BLES (ng/m <sup>3</sup> ) |              |                |          |             |           |
| NITRATE            | 4340                      | 3460         | 2330           | 1970     | 3030        |           |
| SULFATE            | 8180                      | 8790         | 8640           | 8140     | 8440        |           |
| AMMONIUM           | 240                       | 70           | 12 <b>0</b>    | 220      | 160         |           |
| <u>TSP</u> (μg/m³) | 57                        | 37           | 35             | 35       | 41          |           |
| SAMPLE COU         | <u>NT</u> 15              | 16           | 15             | 15       |             |           |

<sup>a</sup> The average was calculated using one quarter of the reportable limit in the second quarter.

TABLE 10

 $\left( \right)$ 

# MONTHLY CHEMICAL CHARACTERIZATION OF 1985 LO-VOL TSP

SITE 001 AREA 0520 TOWN MANSFIELD

|                                    |      |          |      |         | 2    | ΙΟΝΤΗΓΥ | AVERAGE |         |     |         |      | i<br>i  | ANNUAL AVG |
|------------------------------------|------|----------|------|---------|------|---------|---------|---------|-----|---------|------|---------|------------|
|                                    | NAL  | FEB      | MAR  | APR     | MAY  | NNr     | IUL     | AUG     | SEP | 이다      | NON  | DEC     |            |
| <u>METALS</u> (ng/m <sup>3</sup> ) |      |          |      |         |      |         |         |         |     |         |      |         |            |
| BERYLLIUM                          | v.   | ۲.<br>۲. | ٨.1  | ۲.<br>۲ | v.   | v.      | v       | ۲.<br>۷ |     | ۲.<br>۲ | ×.   | ŗ.<br>V | <.1<br>.1  |
| CADMIUM                            | 0.4  | 0.6      | 1.4  | 0.2     | 0.9  | 0.6     | 0.7     | 1.0     |     | 0.5     | 0.3  | 0.4     | 0.6        |
| CHROMIUM                           | 2    | 5        | -    | -       | v    | v       | Ÿ       | -       |     | -       | -    | ~       | 19         |
| COPPER                             | <10  | 10       | <10  | 10      | 10   | 10      | <10     | 10      |     | 10      | <10  | 10      | 10b        |
| IRON                               | 510  | 069      | 580  | 540     | 440  | 380     | 320     | 360     |     | 250     | 170  | 270     | 410        |
| LEAD                               | 100  | 100      | 20   | 60      | 40   | 40      | 40      | 30      |     | 40      | 30   | 40      | 50         |
| MANGANESE                          | ω    | თ        | ø    | 10      | 11   | δ       | S       | Q       |     | 9       | ß    | 9       | œ          |
| NICKEL                             | 9    | 12       | 7    | 7       | 7    | ъ       | თ       | ø       |     | 9       | 9    | 10      | ¢          |
| VANADIUM                           | 20   | 40       | 20   | 20      | 10   | 10      | 20      | 20      |     | 10      | 10   | 20      | 20         |
| ZINC                               | 30   | 50       | 20   | 80      | 20   | 20      | <10     | <10     |     | 30      | 20   | 30      | 30c        |
|                                    |      |          |      |         |      |         |         |         |     |         |      |         |            |
| WATER SOLUBLES (ng/m               | 3)   |          |      |         |      |         |         |         |     |         |      |         |            |
| NITRATE                            | 2670 | 3500     | 2670 | 3100    | 2470 | 2340    | 1340    | 1140    |     | 2150    | 2160 | 2760    | 2390       |
| SULFATE                            | 6260 | 6970     | 6670 | 8710    | 7500 | 7050    | 7500    | 8340    |     | 5120    | 6050 | 6700    | 0669       |
| AMMONIUM                           | 450  | 210      | 150  | 40      | 20   | 20      | 20      | 20      |     | 490     | 400  | 1080    | 260        |
| <u>ТSP</u> (µg/m <sup>3</sup> )    | 45   | 50       | 42   | 45      | 49   | 37      | 26      | 27      |     | 23      | 20   | 35      | 36         |

<sup>a</sup> The average was calculated using one quarter of the reportable limit in May, June and July.

b The average was calculated using one quarter of the reportable limit in January, March, July and November.
c The average was calculated using one quarter of the reportable limit in July, August and September.

# MONTHLY CHEMICAL CHARACTERIZATION OF 1985 LO-VOL TSP

| SITE | 002    |  |
|------|--------|--|
| AREA | 0060   |  |
| TOWN | PUTNAM |  |

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|   |   |                       |   |  | -  | MONTHLY                          | AVERAG                 | ΪĒ             |         |        |      |         | ANNUAL AVG |
|---|---|-----------------------|---|--|--|----------------------------------|------------------------|----------------|---------|--------|------|---------|------------|
|   | NAL   | FEB                   | MAR                                       | APR                                    | MAY  | NUL                              | JUL                    | AUG            | SEP     | 0<br>0 | NON  | DEC     |            |
| METALS (ng/m <sup>3</sup> )   |   |                       |   |  |  |                                  |                        |                |         |        |      |         |            |
| BERYLLIUM   | ۲.<br>۲   | <b>v</b> .1           | <b>1</b> .                                | v                                      | v.   | ۲.<br>۲                          | v.                     | ۲.<br>۲        | ۲.<br>۲ | v.     | v.   | ۲.<br>۲ | ۲.<br>۲    |
| CADMIUM   | 0.5   | 0.5                   | 0.5                                       | 0.6                                    | 0.7  | 0.7                              | 0.5                    | 0.4            | 0.9     | 0.6    | 0.1  | 0.6     | 9.0        |
| CHROMIUM  | Μ   | 4                     | ধ   |  | -  | Ÿ                                | <del></del>            | -              | -       | 2      | 7    | m       | 2a         |
| COPPER  | <10   | 10                    | <10                                       | 10                                     | 10   | 10                               | 10                     | 10             | 10      | 10     | 10   | 10      | 10b        |
| IRON  | 1230  | 750                   | 600                                       | 370                                    | 380  | 360                              | 220                    | 240            | 230     | 220    | 210  | 610     | 450        |
| LEAD  | 120   | 120                   | 70  | 1.00                                   | 60   | 50                               | 50                     | 60             | 50      | 60     | 40   | 70      | 70         |
| MANGANESE   | 13  | 6                     | ø   | ø                                      | 10   | ø                                | S                      | 4              | 4       | S      | ŝ    | σ       | 7          |
| NICKEL  | 7   | 10                    | ŝ   | 4                                      | 9  | ß                                | S                      | 4              | 4       | ŝ      | 4    | 6       | <b>y</b>   |
| VANADIUM  | 20  | 30                    | 10  | 10                                     | 10   | 10                               | 10                     | 10             | 10      | 10     | 20   | 10      | 10         |
| ZINC  | 40  | 40                    | 10  | 50                                     | 20   | 20                               | <10                    | <10            | <10     | 20     | 20   | 30      | 20⊂        |
|   |   |                       |   |  |  |                                  |                        |                |         |        |      |         |            |
| WATER SOLUBLES (n   | g/m <sup>3</sup> )                              |                       |   |  |  |                                  |                        |                |         |        |      |         |            |
| NITRATE   | 2470  | 3350                  | 1990                                      | 2780                                   | 2910   | 2770                             | 1850                   | 2300           | 1970    | 1870   | 1850 | 2610    | 2390       |
| SULFATE   | 5660  | 6580                  | 5510                                      | 6880                                   | 7200   | 7310                             | 7660                   | 8750           | 8860    | 6160   | 8090 | 7480    | 7180       |
| AMMONIUM  | 70  | 70                    | 20  | 10                                     | 20   | 20                               | 10                     | <10            | 60      | 80     | 40   | 470     | 70d        |
| <u>TSP</u> (µg/m <sup>3</sup> )   | 47  | 50                    | 41  | 37                                     | 23   | 38                               | 28                     | 29             | 30      | 25     | 27   | 51      | 38         |
| <sup>a</sup> The average was ca<br><sup>b</sup> The average was ca<br><sup>c</sup> The average was ca | lculated usir<br>Iculated usir<br>Iculated usir | ng one qu<br>g one qu | arter of th<br>arter of th<br>arter of th | e reportal<br>e reportal<br>e reportak | ole limit in<br>ole limit in<br>ole limit in | June.<br>January a<br>July, Augu | nd March<br>Ist and Se | r.<br>ptember. |         |        |      |         |            |
|   |   | · · · · · · · · ·     |   |  |  | · ?                              | ~~~~~~                 |                |         |        |      |         |            |

<sup>d</sup> The average was calculated using one quarter of the reportable limit in August.

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|            |                     |   |                                |                    | Rages .                        | <u>0</u>   |                                   |                     |                                 |       |                     |                       |                        | 5                             | _                  |                                   |   |  |       |        |                     | 2                             | and a state of the |                                 |
|------------|---------------------|---|--------------------------------|--------------------|--------------------------------|--|-----------------------------------|---------------------|---------------------------------|-------|---------------------|-----------------------|------------------------|-------------------------------|--------------------|-----------------------------------|---|--|-------|--------|---------------------|-------------------------------|--|---------------------------------|
| IC METER   | 10                  | 67  | 0/18/85<br>230<br>9.1          | 10.2<br>0.894      | 190                            | 8.2<br>0.989<br>0.000  | 0.7                               | 0.946<br>210        | 7.4<br>7.8<br>0 950             | 2     | 65                  | 3/ 8/85<br>220        | 12.1                   | 240<br>240                    | 8.1<br>0.606       | 240<br>10.7                       | 0.996   | 19.6<br>20.4   | 0.958 | 7,     | 65<br>3/ 8/85       | 11.1                          | 0.921  | 4.9<br>8.1<br>0.606             |
| S PER CUB  | .σ -                | 68<br>10,00   | 10/10/85<br>240<br>13_0        | 13.7               | 230                            | 9.1<br>0.553   | 0.00                              | 0.978<br>250        | 9.6<br>10.1<br>955              |       | 99                  | 6/18/85<br>230<br>230 | 10.2                   | 0.094<br>190<br>8.1           | 8.2<br>0.989       | 220                               | 0.946   | 0-1-C  | 0.950 | 7:     | 68<br>6/18/85       | 9.1<br>10.2                   | 0.894  | 8.1<br>8.2<br>0.989             |
| MI CROGRAM |                     | 689<br>10, 10, 10, 10, 10, 10, 10, 10, 10, 10,                                    | 1/31/85<br>30<br>7_1           | 7.5<br>0.950       | 10                             | 5.3<br>0.966   | 10.5<br>10.8                      | 0.974<br>60         | 0.0<br>72.0<br>72.4             |       | 69                  | 1/19/85<br>240        | 10.1                   | 0.041<br>240<br>5.0           | 0.911              | 260                               | 0.864   | 5.5<br>5.5<br>5.5  | 0.726 | 73     | 69<br>12/27/85      | 12.6<br>13.2                  | 0.952  | 8.2<br>9.2<br>0.893             |
| UNITS : I  | ~                   | 69  | 2/13/85<br>230<br>10.7         | 11.8               | 180                            | $9.1 \\ 0.807 \\ 202 \\ 202 \\ 202 \\ 202 \\ 0.00$ | 7.4                               | 0.916<br>220        | 0.55<br>885                     |       | 70                  | 9/ 4/85<br>250        | 12.5                   | 0.744<br>240<br>5.3           | 8.3<br>0.635       | 260                               | 9.8<br>0.992<br>250   | 11.6   | 0.957 | SE     | 1/ 7/85             | 2.8<br>6.6                    | 0.417  | 6.8<br>7.5<br>0.910             |
| WIND DATA  | 9                   | (NW)  | 300<br>300<br>3.2              | 9.6<br>0.335       | 10                             | 0.717  | 8.00<br>8.00<br>8.00              | 0.341<br>290        | 9.5<br>11.9                     |       | 2)2                 | 1/ 7/85<br>40         | 100                    | 0.41/<br>10<br>6.8            | 7.5                | 40<br>9.6                         | 0.870   | 0.7  | 0.985 | 5      | 16<br>2/24/85       | 10.4                          | 0.924  | 8.2<br>8.6<br>0.949             |
| AYS WITH V | 'n                  | 73  | 2/24/85<br>210<br>10 4         | 11.2               | 190                            | 8.6<br>0.949   | 8.6<br>8.6                        | 0.997<br>260        | 13.6<br>16.0<br>851             |       | 76                  | 5/13/85<br>230        | 11.8                   | 0, 909<br>180<br>7_3          | 9.1<br>0.807       | 200                               | 0.916<br>220  | 0.4<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1 | 0.886 | 21     | 11<br>9/ 4/85       | 11.8<br>12.5                  | 0.944  | 5.3<br>8.3<br>0.635             |
| AGE TSP D  | 4                   | 75  | 4/19/85<br>260<br>8 4          | 11.4               | 340                            | 4.5  | 180<br>3.1<br>7.2                 | 0.438<br>300        | 5.6<br>10.5<br>12.5             |       | 77                  | 12/27/85<br>220       | 13.20                  | 210<br>210<br>2               | 9.2<br>0.893       | 240                               | 14.8<br>0.988<br>220  | 11.8   | 0.957 | > ;    | 85<br>5/13/85       | 230<br>10.7<br>11.8           | 0.909  | 7.3<br>9.1<br>0.807             |
| HOUR AVER  | ε                   | 76  | 1/19/85<br>240<br>8 5          | 10.1<br>0.841      | 240                            | 0.911<br>0.911   | 260<br>9.6<br>11.1                | 0.864<br>260        | 5.3<br>7.3<br>0 726             | 2.1.0 | 83                  | 4/25/85<br>320<br>5   | 0.00<br>4.0.5          | 200<br>200                    | 6.5<br>0.359       | 230                               | 5.3<br>0.620  | 11.0   | 0.955 | i<br>d | 85<br>4/19/85       | 260<br>8.4<br>11.4            | 0.735  | 3.2<br>4.5<br>0.717             |
| GHEST 24-  | 2                   | 28-<br>1-<br>1-<br>1-<br>1-<br>1-<br>1-<br>1-<br>1-<br>1-<br>1-<br>1-<br>1-<br>1- | 270 270 121 270                | 5.8<br>0.848       | 2.8                            | 3.7<br>0.759   | 0.00                              | 0.945<br>280        | 5.7<br>6.3<br>0 00h             |       | 87                  | 4/19/85<br>260<br>2   | 11.4                   | 0. / 350<br>340<br>3 20       | 4.5<br>0.717       | 3.1                               | 1.2<br>0.438<br>200   | 5.6<br>10.5  | 0.534 | 71     | 87<br>4/25/85       | 5.40<br>8.41<br>9.45          | 0.604  | 2.3<br>6.5<br>0.359             |
| 85 TEN HI  | - \                 | 76  | 220<br>220<br>12 6             | 13.2<br>0.952      | 210<br>8.2                     | 9.2<br>0.893   | 240<br>14.6<br>14.8               | 0.988<br>220        | 11.8<br>12.4<br>0 057           | Can.  |                     | 5/ 1/85<br>300        | 200<br>200<br>200      | 0.335<br>7 10<br>4            | 7.5                | 280                               | $ \begin{array}{c} 8.6\\ 0.341\\ 200\\ 200\\ 0.200\\ 0.200\\ 0.00$ | 9.5<br>7.0   | 0.793 | Se     | 91<br>5/_1/85       | 3.20<br>3.20<br>9.20          | 0.335  | 5.4                             |
| 19         | RANK                | TSP   | UATE<br>DIR (DEG)<br>VFI (MPH) | SPD (MPH)<br>RATIO | DIR (DEG)<br>VEL (MPH)         | SPD (MPH)<br>RATIO   | VEL (MPH)<br>SPD (MPH)            | RATIÒ<br>DIR (DEG)  | VEL (MPH)<br>SPD (MPH)<br>RATIO |       | TSP                 | DATE<br>DIR (DEG)     | VEL (MPH)<br>SPD (MPH) | DIR (DEG)<br>VFI (MPH)        | SPD (MPH)<br>RATIO | DIR (DEG)<br>VEL (MPH)            | SPD (MPH)<br>RATIO  | VEL (MPH)  | RATIO |        | TSP<br>DATE         | VEL (MPH)<br>SPD (MPH)        | RATIO  | VEL (MPH)<br>SPD (MPH)<br>RATIO |
|            | TOWN-SITE (SAMPLES) | ANSONIA-004 (59)  | METEOROLOGICAL SITE<br>NEWARK  |                    | METEOROLOGICAL SITE<br>BRADLEY |  | MEIEOROLOGICAL SIIE<br>BRIDGEPORT | METEOROLOGICAL SITE | WORCESTER                       |       | BRIDGEPORT-001 (59) | METEOROLOGICAL SITE   | NEWAKK                 | METEOROLOGICAL SITE<br>RADIFY |                    | METEOROLOGICAL SITE<br>BRIDGEPORT |   | MELEURULUGIUAL STIE<br>WORCESTER   |       |        | BRIDGEPORT-009 (57) | METEOROLOGICAL SIIE<br>NEWARK | METEODOLOCICAL SITE  | BRADLEY                         |

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TABLE 11

 $\left(\begin{array}{c} \\ - \end{array}\right)$ 

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|            |                     |  |  |                        |                                     | 190  |   |                                  |               |                  |                                     | d'   |  |   |
|------------|---------------------|--|--|------------------------|-------------------------------------|--|---|----------------------------------|---------------|------------------|-------------------------------------|--|--|---|
| IC METER   | 10                  | 240<br>10.7<br>10.8                          | 270<br>270<br>20.4<br>0.958                  | 94<br>6/12/85          | 290<br>290<br>12.2                  | 0.517<br>20<br>5.3                           | 0.940<br>40<br>6.1  | 0.761<br>40<br>7.3<br>9.1        | 0.806         | 5/ 1/85          | 300<br>3.2<br>9.6                   | 0.335<br>10<br>7.5                           | 0.717<br>280<br>2.9                          | 0.341<br>290<br>9.5<br>11.9<br>0.793                  |
| s per cue  | 6                   | 220<br>6.7<br>7.0                            | 0.950<br>210<br>7.4<br>7.8<br>0.950          | 96<br>11 / 10 / 85     | 260<br>8.4<br>11.4                  | 0.735<br>340<br>3.2<br>4.5                   | 0.717<br>180<br>3.1                                       | 0.438<br>300<br>5.6              | 0.534         | 60<br>1/31/85    | 30                                  | 0.950<br>5.1<br>5.3                          | 0.966<br>40<br>10.5                          | 0.974<br>60<br>5.2<br>0.763                           |
| MICROGRAM  | ω                   | 240<br>14.6<br>14.8                          | 0.957<br>11.8<br>12.4<br>0.957               | 08<br>98<br>18/85      | 260<br>10.0                         | 0.847<br>270<br>8.8<br>10.1                  | 0.871<br>270<br>10.4                                      | 0.981<br>290<br>16.9             | 0.981         | 61<br>4/19/85    | 260<br>8.4<br>11.4                  | 0.735<br>340<br>3.2<br>4.5                   | 0.717<br>180<br>3.1                          | 0.438<br>5.6<br>10.5<br>0.534                         |
| UNITS : I  | 7                   | 40<br>9.6<br>11.1                            | 0.085<br>70<br>7.9<br>8.1<br>0.985           | 101<br>101<br>12/27/85 | 12.6<br>13.2                        | 0.952<br>8.20<br>9.2                         | 0.893<br>240<br>14.6                                      | 0.988<br>220<br>11.8             | 0.957         | 62<br>9/ 4/85    | 250<br>11.8<br>12.5                 | 0.944<br>240<br>5.3                          | 0.635<br>260<br>9.7                          | 0.992<br>250<br>11.6<br>0.957                         |
| VIND DATA  | 9                   | 240<br>8.6<br>8.6                            | 0.851<br>13.6<br>0.851                       | 102<br>11/25/85        | 5.4<br>8.9                          | 0.604<br>2.3<br>6.5                          | $\begin{array}{c} 0.359 \\ 230 \\ 3.3 \\ 5.3 \end{array}$ | 0.620<br>250<br>11.0             | 0.955         | 62<br>3/ 8/85    | 220                                 | 0.921<br>240<br>4.9<br>8.1                   | 0.606<br>240<br>10.7                         | 0.956<br>19.6<br>20.4<br>0.958                        |
| VS WITH V  | Ъ                   | 9.7<br>9.8<br>9.8                            | 0.957<br>250<br>11.6<br>12.1<br>0.957        | 105<br>5/13/85         | 230<br>230<br>11.8                  | 0.909<br>180<br>7.3<br>9.1                   | 0.807<br>200<br>7.4                                       | 0.916<br>220<br>8.4              | 0.886         | 63<br>5/13/85    | 230<br>10.7<br>11.8                 | 0.909<br>180<br>7.3<br>9.1                   | 0.807<br>200<br>7.4<br>8.1                   | 0.916<br>220<br>8.4<br>0.886                          |
| GE TSP DA  | 4                   | 200<br>7.4<br>8.1                            | 0.886<br>0.886                               | 118<br>272/1/85        | 10.4<br>11.2                        | 0.924<br>190<br>8.2<br>8.6                   | 0.949<br>240<br>8.6                                       | 0.997<br>260<br>13.6             | 0.851<br>(Jb) | 3/20/85          | 250<br>9.5<br>13.9                  | 0.678<br>290<br>6.8<br>10.1                  | 0.674<br>270<br>7.6<br>10.2                  | 0.740<br>280<br>14.0<br>15.2<br>0.916                 |
| Iour aver⊿ | ε                   | 180<br>3.1<br>7.2                            | 0.534<br>0.534                               | (NW)<br>129<br>57 1785 | 3.2                                 | 0.335<br>5.4<br>7.5                          | 0.717<br>280<br>2.9<br>8.6                                | 0.341<br>290<br>9.5              | 0.793         | 65<br>2/27/85    | 220<br>12.6<br>13.2                 | 0.952<br>210<br>8.2                          | 0.893<br>240<br>14.6<br>14.8                 | 0.988<br>220<br>11.8<br>12.4<br>0.957                 |
| HEST 24-H  | 2                   | 230<br>3.3<br>5.3<br>600                     | 250<br>250<br>11.0<br>0.955                  | (NE)<br>137<br>9/22/85 | 4.8                                 | 0.640<br>30<br>5.0<br>6.0                    | 0.831<br>80<br>8.5<br>0.2                                 | 0.921<br>40<br>8.7<br>8.8        | 0.989<br>WW   | 2/18/85 1        | 260<br>10.0                         | 0.847<br>270<br>8.8<br>10.1                  | 0.871<br>270<br>10.4<br>10.6                 | 0.981<br>290<br>16.9<br>17.3<br>0.981                 |
| 5 TEN HIG  | <b>F</b>            | 280<br>2.9<br>311                            | 290<br>290<br>11.9<br>0.793                  | 139<br>139<br>7/ 6/85  | 200<br>7.6<br>8.3                   | 0.913<br>180<br>6.9<br>7.0                   | 0.981<br>190<br>6.7<br>7.0                                | 0.957<br>210<br>8.3<br>8.6       | 0.966<br>(NF) | 79<br>1/ 7/85    | 40<br>2.8<br>6.6                    | 0.417<br>10<br>6.8<br>7.5                    | 0.910<br>40<br>9.6                           | 0.870<br>70<br>7.9<br>8.1<br>0.985                    |
| 198        | RANK                | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>BATLO | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO | TSP<br>Natf            | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (SCG)<br>VEL (MPH)<br>SPD (MPH)              | SPD (MPH)                        | RATIO         | TSP<br>DATE      | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO |
|            | TOWN-SITE (SAMPLES) | METEOROLOGICAL SITE<br>BRIDGEPORT            | METEOROLOGICAL SITE<br>WORCESTER             | BRIDGEPORT-123 (57)    | METEOROLOGICAL SITE<br>NEWARK       | METEOROLOGICAL SITE<br>BRADLEY               | METEOROLOGICAL SITE<br>BRIDGEPORT                         | METEOROLOGICAL SITE<br>WORCESTER |               | BRISTOL-001 (60) | METEOROLOGICAL SITE<br>NEWARK       | METEOROLOGICAL SITE<br>BRADLEY               | METEOROLOGICAL SITE<br>BRIDGEPORT            | METEOROLOGICAL SITE<br>WORCESTER                      |

. (\_\_\_\_\_) 1985 TEN HIGHEST 24-HOUR AVERAGE TSP DAYS WITH WIND DATA UNITS : MICROGRAMS PER CUBIC METER

|                     |  |   |  | _  | $\sim$   |  | N  | <u>]</u> .  |
|---------------------|--|---|--|--|--|--|--|---|
| 10                  | 12/27/85<br>31<br>220<br>12.6<br>13.2                | 0.89.2<br>0.89.2<br>14.6<br>14.6<br>14.8  | 0.988<br>11.8<br>11.8<br>0.957                                 | 62<br>3/ 8/85<br>220<br>11.1<br>12.1<br>0.921      | 0.60.1<br>10.7<br>0.5<br>0.5<br>0.5<br>0.5<br>0.5<br>0.1<br>0.7        | 0.270<br>20.44<br>20.44  | 2.8<br>2.8<br>2.8<br>5.6<br>6.6<br>6.6             | 6.8<br>7.5<br>0.910                                   |
| 2 . 0               | 6/24/85<br>240<br>8.7<br>9.8                         | 0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | 0.802<br>8.0<br>8.0<br>8.0<br>8.0<br>8.0<br>8.0                | 66<br>3/20/85<br>250<br>9.5<br>13.9<br>0.678       | 290<br>629<br>674<br>270<br>7.6  | 0.740<br>280<br>14.0<br>15.2<br>0.916                              | 73<br>4/19/85<br>260<br>8.4<br>11.4                | 0.717<br>340<br>3.2<br>4.5                            |
| 8                   | 4/19/85<br>260<br>260<br>11.4                        | 0.1100  | 0.438<br>300<br>15.6<br>0.534                                  | 67<br>9/ 4/85<br>250<br>11.8<br>12.5<br>0.944      | 0.635<br>240<br>260<br>260<br>0.635<br>260                             | 0.992  | 75<br>2/24/85<br>210<br>11.2<br>11.2               | 0.949<br>0.949  |
|                     | 7/ 6/85<br>200<br>7.6<br>3.3                         | 0.981<br>0.981<br>0.981<br>0.7.0<br>7.0   | 0.955<br>8.3<br>0.966<br>W                                     | 2/18/85<br>260<br>10.0<br>11.8<br>0.847            | 270<br>8.8<br>871<br>270<br>270  | 0.981<br>2290<br>176.9<br>81<br>17.3                               | 1/31/85<br>30<br>7.1<br>7.1<br>7.5                 | 0.906<br>5.3<br>0.966                                 |
| `<br>و              | 6/18/85<br>230<br>230<br>10.2                        | 0.989<br>0.989<br>0.989<br>0.70<br>0.7  | 0.946<br>210<br>7.4<br>0.950                                   | 76<br>270<br>4.9<br>5.8<br>0.848                   | 0.759<br>5.66  | 0.945<br>5.7<br>0.904<br>0.904<br>0.945                            | 5/ 1/85<br>300<br>3.2<br>9.6                       | 5.4<br>0.717<br>0.717                                 |
| 5                   | 5/25/85<br>37<br>120<br>3.3<br>3.3<br>3.3            | 0.420<br>170<br>170<br>170<br>110<br>110<br>4.7   | 0.828<br>210<br>7.7<br>8.9<br>0.861                            | 79<br>260<br>8.4<br>11.4<br>0.735                  | 0.717<br>3.10<br>3.10<br>3.10<br>3.10<br>3.10<br>3.10                  | 0.438<br>550<br>15.6<br>0.534                                      | 270<br>83<br>41.9<br>5.8<br>5.8                    | 0.759<br>330<br>2.8<br>3.7<br>0.759                   |
| ħ                   | 5/31/85<br>190<br>10.2                               | 0.190<br>10.190<br>190<br>190<br>7.5<br>7.5   | 0.967<br>200<br>13.8<br>13.9<br>0.988<br>0.988                 | 65<br>5/ 1/85<br>300<br>3.2<br>9.6<br>9.6          | 0.7.5  | 0.341<br>2.90<br>11.9<br>0.793                                     | 83<br>83<br>250<br>6.9<br>9.6                      | 0.676   |
| ŝ                   | 9/ 4/85<br>250<br>11.8<br>12.5                       | 0.2444<br>0.83.3<br>9.80<br>9.80<br>9.8   | 0.992<br>250<br>11.6<br>0.957                                  |  | 0.55.3<br>0.966<br>10.55   | 0.974<br>60<br>75.2<br>0.763                                       | 90<br>3/ 8/85<br>220<br>11.1<br>12.1               | 0.606   |
| ~                   | 5/ 1/85<br>3.2<br>3.2<br>3.2<br>3.2<br>9.6           | 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0. 0  | 0.341<br>9.5<br>0.703<br>0.703                                 | 1/ 7/85<br>40<br>2.8<br>6.6<br>6.6                 | 0.910<br>9.6   | 0.870<br>70<br>7.9<br>0.985<br>0.985                               | 2/18/85<br>260<br>10.0                             | 0.84/<br>270<br>8.8<br>10.1<br>0.871                  |
| •                   | 5/13/85<br>230<br>11.8                               | 0.909<br>9.1<br>2.0<br>8.1<br>8.1   | 0.916<br>8.4<br>8.5<br>8.6<br>8.6<br>0.886                     | (420)<br>3/ 2/85<br>300<br>13.3<br>15.4            | 0.823<br>9.60<br>9.60  | 0.894<br>3.00<br>16.2<br>0.880<br>0.880<br>0.880                   | 3/ 2/85<br>3/ 2/85<br>13.3<br>15.4                 | 0.864<br>310<br>9.0<br>10.9<br>0.823                  |
| RANK                | TSP<br>DATE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)   | VEL (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>VEL (MPH)<br>SPD (MPH)     | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>RATIO | TSP<br>DATE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH) | SPU (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO | TSP<br>DATE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | KALLU<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO |
| TOWN-SITE (SAMPLES) | BURLINGTON-001 (59)<br>METEOROLOGICAL SITE<br>NEWARK | METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT                         | METEOROLOGICAL SITE<br>WORCESTER                               | DANBURY-002 (61)<br>METEOROLOGICAL SITE<br>NEWARK  | METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT    | METEOROLOGICAL SITE<br>WORCESTER                                   | DANBURY-123 (58)<br>METEOROLOGICAL SITE<br>NEWARK  | METEOROLOGICAL SITE<br>BRADLEY                        |

1985 TEN HIGHEST 24-HOUR AVERAGE TSP DAYS WITH WIND DATA

|            |                     |  | - An   |   | 0-   |
|------------|---------------------|--|--|---|--|
| SIC METER  | 10                  | 40<br>11:10<br>0.870<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70   | 0.575<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.719<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.757<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577<br>0.7577       | 0.288779  | 6/26<br>244/8<br>244/8<br>244/8<br>244/8<br>244/8<br>2306<br>2306<br>2306<br>2306<br>2306<br>2306<br>2306<br>2306  |
| IS PER CUE | - 6                 | 0.538<br>0.538<br>0.556<br>0.556<br>0.534<br>0.556   | 5/13/85<br>2300<br>10.7<br>11.8<br>0.909<br>7.3<br>9.7<br>807  | 0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.89.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.54<br>0.99.5 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3,202<br>3,202<br>250,45<br>250,45<br>0,674<br>1,280<br>0,574<br>1,280<br>0,574<br>1,280<br>0,574<br>1,280<br>0,574<br>1,280<br>0,574<br>1,280<br>0,574<br>1,280<br>0,574<br>1,280<br>0,574<br>1,280<br>0,576<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,280<br>1,20 |
| MICROGRAM  | ω                   | 240<br>8.6<br>0.997<br>15.60<br>0.851<br>0.851<br>0.851  | 0.950<br>0.950<br>0.950<br>0.950<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.10<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.055<br>0.0 | 0.10.5  | 5/13/85<br>5/13/85<br>230/11.8<br>11.8<br>0.9216<br>2200<br>2200<br>2200<br>2200<br>2200<br>2200<br>2200<br>2  |
| UNITS :    | 7                   | 40<br>10.55<br>60<br>474<br>60<br>4.20<br>60<br>763  | 2/169<br>2/18/85<br>260<br>11.8<br>0.847<br>270<br>8.8<br>8.8<br>10.871  | 0.981<br>270<br>0.981<br>2290<br>2290<br>16.9<br>0.981<br>0.981   | 12/27/85<br>12/27/85<br>13:22<br>0.952<br>8.22<br>9.22<br>0.952<br>0.988<br>0.988<br>0.957<br>0.957<br>0.957   |
|            | 9                   | 280<br>286<br>286<br>286<br>290<br>290<br>290<br>290<br>290<br>290<br>290<br>290<br>290  | 12/27/85<br>220<br>13.25<br>0.952<br>8.2<br>8.2<br>9.2<br>9.3  | 0.988<br>0.988<br>114.6<br>0.988<br>1128<br>0.957   | 12/ 12/ 16<br>270 97<br>270 97<br>3320<br>3320<br>3320<br>3320<br>3320<br>3320<br>3320<br>332  |
|            | ŋ                   | 0.904<br>0.945<br>0.904<br>0.904<br>0.904  | 3/ 22<br>3/ 8/85<br>11.1<br>12.1<br>12.1<br>12.1<br>12.1<br>0.240<br>4.9<br>4.9<br>8.1<br>0.606  | 240<br>240<br>10.7<br>240<br>296<br>296<br>20.4<br>0.958  | 10/10/85<br>240<br>240<br>13.7<br>13.7<br>5.0<br>5.0<br>5.0<br>0.553<br>0.978<br>0.978<br>0.978<br>0.955<br>0.955  |
|            | t,                  | 250<br>8.1<br>8.9<br>280<br>5.9<br>0.802<br>0.802  | 4/19/85<br>260<br>2.00<br>2.11.4<br>0.735<br>3.2<br>3.2<br>3.2<br>3.2<br>0.717   | 0.534<br>0.556<br>0.538   | 6/18/85<br>230<br>230<br>230<br>230<br>230<br>230<br>8.1<br>8.1<br>190<br>8.1<br>190<br>8.1<br>0.989<br>0.989<br>0.950<br>0.950<br>0.950   |
|            | ę                   | 240<br>10.7<br>10.8<br>270<br>270<br>270<br>20.4<br>0.95<br>8  | 3/20/85<br>250<br>9.5<br>13.9<br>0.678<br>5.90<br>6.8<br>0.674   | 0.71<br>0.740<br>17.60<br>17.00<br>15.00<br>0.916   | 9/ 4/85<br>250 9/ 4/85<br>250 250<br>2444<br>5.3<br>5.3<br>5.3<br>9.4<br>9.7<br>9.8<br>9.7<br>9.8<br>9.7<br>9.8<br>9.7<br>0.992<br>0.957   |
|            | N                   | 2270<br>2290<br>2290<br>290<br>290<br>290<br>290<br>291<br>290<br>291<br>200<br>200<br>200<br>200<br>200<br>200<br>200<br>200<br>200<br>20 | 12/21/85<br>300<br>7.9<br>8.6<br>0.914<br>4.7<br>4.7<br>0.731  | 310<br>8.0<br>865<br>310<br>5.1<br>5.1<br>0.724   | 4/19/85<br>260<br>260<br>8.4<br>11.4<br>0.717<br>3.2<br>3.2<br>3.2<br>3.2<br>3.2<br>10.7<br>5.6<br>0.534<br>0.534  |
|            | F                   | 0.880<br>16.2<br>0.880<br>16.2<br>0.880<br>0.880<br>0.880<br>0.880<br>0.880  | 5/1/85<br>3.2<br>3.2<br>9.6<br>0.335<br>0.335<br>0.717   | 280<br>2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.90<br>2.9  | 5/1/85<br>300<br>3.2<br>3.2<br>3.2<br>3.2<br>3.2<br>5.4<br>0.717<br>2.9<br>0.717<br>2.9<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.717<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.7777<br>0.7777<br>0.7777<br>0.7777<br>0.7777<br>0.7777<br>0.7777<br>0.7777<br>0.77777<br>0.77777<br>0.77777<br>0.777777<br>0.77777777  |
|            | RANK                | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>VEL (MPH)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO   | TSP<br>DATE<br>DATE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>VEL (MPH)<br>VEL (MPH)<br>SPD (MPH)<br>SPD (MPH)  | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>SAT (0<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO   | TSP<br>DATE<br>DATE<br>DIR (DEG)<br>VEL (MPH)<br>SATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (M   |
|            | TOWN-SITE (SAMPLES) | METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>WORCESTER  | EAST HARTFORD-004 (57)<br>METEOROLOGICAL SITE<br>NEWARK<br>METEOROLOGICAL SITE<br>BRADLEY  | METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>WORCESTER   | GREENWICH-008 (60)<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE   |

| (MPH) 2<br>(MPH) 8<br>(DEG) 22<br>(MPH) 9<br>9<br>11<br>9<br>11  |
|--|
| 0.1733     0.1733       09     92       09     92       01000     5/1/85     4/19/85       (MPH)     3.2     8.4       000     0.335     0.735       000     0.335     0.735       000     0.335     0.735       000     0.335     0.735       000     0.717     0.717       000     0.717     0.717       000     0.717     0.717       000     0.717     0.717       000     0.717     0.717       000     0.717     0.717       000     0.717     0.717       000     0.717     0.717       000     0.717     0.717       000     0.717     0.717       000     0.717     0.717       000     0.717     0.717       000     0.717     0.713       000     0.717     0.713       000     0.717     0.713       000     0.717     0.713       000     0.717     0.713       000     0.717     0.713       000     0.711     0.713       000     0.711     0.713 |
| (DEG) 250 300<br>(DEG) 250 300<br>(MPH) 11.4 9.6<br>(MPH) 11.4 9.6<br>(MPH) 11.4 9.6<br>(DEG) 340 0.735 0.335<br>(DEG) 340 10<br>(MPH) 3.2 5.4<br>(MPH) 4.5 7.5  |

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1985 TEN HIGHEST 24-HOUR AVERAGE TSP DAYS WITH WIND DATA UNITS : MICROGRAMS PER CUBIC METER

| -                   |   | č<br>4-   | S. S.  |
|---------------------|---|---|--|
| 10                  | 240<br>9.5<br>9.56<br>9.56<br>0.978<br>0.955<br>0.10  | 0.955<br>0.955<br>0.955<br>0.953<br>0.953<br>0.953<br>0.953<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.9550<br>0.9550<br>0.9550<br>0.9550<br>0.955000<br>0.9550000000000  | 22<br>27<br>27<br>27<br>27<br>27<br>27<br>27<br>27<br>27   |
| 6                   | 230<br>2520<br>2550<br>0.955<br>0.955   | 2/24/85<br>2/24/85<br>210.4<br>111.2<br>111.2<br>210<br>2240<br>2240<br>2240<br>2240<br>2240<br>2260<br>2240<br>260<br>260<br>260<br>260<br>260<br>260<br>260<br>260<br>260<br>26   | 12/52<br>270<br>270<br>270<br>270<br>270<br>270<br>270<br>270<br>270<br>27   |
| 0000                | 40<br>19.6<br>11.1<br>70<br>7.70<br>8.1<br>0.985  | 0.22/85<br>6.8<br>10.4<br>0.260<br>1.8<br>1.8<br>0.857<br>0.857<br>0.986<br>0.986<br>0.986  | $\begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 $   |
|                     | 240<br>14.6<br>0.988<br>114.8<br>12.2<br>12.4<br>0.957<br>12.4  | 12/21/85<br>7.9<br>7.9<br>0.914<br>0.731<br>0.731<br>0.724<br>0.724<br>0.724<br>0.724   | 57<br>76<br>77<br>76<br>77<br>77<br>77<br>77<br>77<br>76<br>76   |
| 9                   | 0.865<br>9.20<br>5.10<br>0.724  | 5/13/85<br>230<br>11.7<br>11.8<br>11.8<br>11.8<br>11.8<br>11.8<br>11.8<br>11.8  | 4/19/85<br>260<br>8.4<br>11.4<br>11.4<br>1.5<br>0.717<br>3.1<br>180<br>1.80<br>1.80<br>1.80<br>1.80<br>1.80<br>1.80<br>1.8   |
| 5                   | 40<br>10.5<br>10.8<br>10.8<br>10.8<br>10.974<br>4.60<br>0.763<br>0.763  | $\begin{pmatrix} & & & & \\ & & & & \\ & & & & \\ & & & & $   | 9/ 455<br>250<br>250<br>2550<br>244<br>2550<br>2540<br>2550<br>2550  |
| 4                   | 220<br>220<br>25.7<br>2.946<br>2.946<br>7.14<br>0.7.8   | 9/ 4/85<br>11.8<br>12.5<br>0.9244<br>9.8<br>0.922<br>0.992<br>0.992<br>0.992<br>0.992<br>11.16<br>0.992<br>0.992<br>11.16<br>0.992<br>0.992<br>0.992<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.9520<br>0.952<br>0.9520<br>0.9520<br>0.9520<br>0.9520<br>0.9520<br>0.9520<br>0.9520<br>0.9520<br>0.95200<br>0.9520<br>0.95200<br>0.95200000000000000000000000000000000000  | 5/12<br>3.2<br>3.2<br>3.2<br>3.2<br>3.2<br>3.2<br>3.2<br>5.2<br>0.3<br>5.4<br>0.2<br>280<br>2.2<br>0.3<br>17<br>2.5<br>0.3<br>2.5<br>0.3<br>3.5<br>5.4<br>0.7<br>17<br>2.5<br>0.3<br>3.5<br>5.4<br>0.3<br>3.5<br>5.4<br>0.3<br>3.5<br>5.4<br>17<br>8<br>5.4<br>17<br>8<br>5.4<br>17<br>8<br>5.4<br>17<br>8<br>5<br>6<br>7<br>17<br>8<br>5<br>6<br>7<br>17<br>8<br>5<br>6<br>7<br>17<br>8<br>5<br>6<br>7<br>17<br>8<br>5<br>6<br>7<br>17<br>8<br>5<br>6<br>7<br>17<br>8<br>5<br>6<br>7<br>17<br>8<br>5<br>6<br>7<br>17<br>8<br>5<br>7<br>17<br>8<br>5<br>6<br>7<br>17<br>8<br>5<br>7<br>8<br>7<br>17<br>8<br>5<br>7<br>17<br>8<br>5<br>7<br>17<br>8<br>5<br>7<br>8<br>7<br>17<br>8<br>5<br>7<br>17<br>8<br>5<br>7<br>17<br>8<br>5<br>7<br>17<br>8<br>5<br>7<br>17<br>8<br>5<br>7<br>17<br>8<br>5<br>7<br>8<br>7<br>17<br>8<br>5<br>7<br>17<br>8<br>5<br>7<br>8<br>7<br>17<br>8<br>5<br>7<br>8<br>7<br>8<br>5<br>7<br>8<br>7<br>8<br>5<br>8<br>7<br>8<br>7<br>8<br>7<br>8  |
| ŝ                   | 0.836<br>0.83.1<br>0.83.1<br>0.836<br>0.836<br>0.836<br>0.836<br>0.836<br>0.836<br>0.836<br>0.836<br>0.836<br>0.836<br>0.836<br>0.836<br>0.836<br>0.836<br>0.836<br>0.55<br>0.55<br>0.55<br>0.55<br>0.55<br>0.55<br>0.55<br>0.5 | 5/185<br>5/185<br>3.20<br>3.25<br>0.335<br>0.717<br>2.80<br>0.717<br>2.80<br>0.717<br>2.80<br>0.717<br>2.80<br>0.773<br>0.773<br>0.773<br>0.773<br>0.773<br>0.773<br>0.773<br>0.773<br>0.773<br>0.773<br>0.773<br>0.773<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.775<br>0.7750<br>0.7750<br>0.7750<br>0.7750<br>0.7750000000000 | 5/13/85<br>230<br>230<br>10.7<br>11.8<br>0.909<br>7.4<br>0.907<br>7.4<br>0.916<br>8.4<br>8.4<br>8.4<br>8.4   |
| 5                   | 280<br>2.9<br>2.9<br>2.41<br>2.41<br>2.9<br>2.9<br>2.9<br>2.9<br>2.9<br>2.9<br>2.9<br>2.9<br>2.9<br>2.9   | 0.75.2<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974<br>0.975<br>0.975<br>0.975<br>0.975<br>0.956<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0.975<br>0 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3/20/85<br>3/20/85<br>250/85<br>9.5<br>0.13.9<br>270<br>0.674<br>17.6<br>0.740<br>17.2<br>0.740<br>17.2<br>0.740<br>17.2<br>0.740<br>17.2<br>0.7280<br>0.740<br>17.2<br>0.740<br>17.2<br>0.740<br>17.2<br>0.740<br>17.2<br>0.740<br>17.2<br>0.740<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0.750<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>0<br>17.2<br>10<br>17.2<br>0<br>17.2<br>0<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>17.2<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10 |
| ~                   | 180<br>3.1<br>3.1<br>0.438<br>5.6<br>10.5<br>0.534  | 4/19/85<br>4/19/85<br>260<br>3.19/85<br>3.22<br>3.22<br>3.22<br>3.22<br>3.22<br>3.22<br>3.22<br>3.2   | 1/122<br>1/122<br>1/31/85<br>0.950<br>5.3<br>0.956<br>10.5<br>10.5<br>10.5<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974   |
| RANK                | DIR (DEG)<br>SPD (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>RATIO   | TSP<br>DATE<br>DATE<br>VEL (MPH)<br>SPD (MPH)   | TSP<br>DATE<br>DATE<br>DIR (DEG)<br>SPD (MPH)<br>SPD (MPH)   |
| TOWN-SITE (SAMPLES) | METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>WORCESTER   | HARTFORD-014 (58)<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE   | MANCHESTER-001 (55)<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE  |

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1985 TEN HIGHEST 24-HOUR AVERAGE TSP DAYS WITH WIND DATA

| ~          |                     |  | M  |   |  | $\sim$   |   | 5   |
|------------|---------------------|--|--|---|--|--|---|---|
| IC MELE    | 10                  | 12/ 9/85<br>270<br>4.9<br>5.8                      | 0.848<br>330<br>2.8<br>3.7<br>0.759<br>270                         | 5.6<br>5.9<br>280<br>5.7<br>0.904   | 6/18/8<br>9.1<br>9.1                                 | 0.839<br>0.989<br>0.989<br>0.70<br>0.70<br>0.70  | 0.946<br>210<br>7.4<br>0.950<br>0.950                           | 70<br>240<br>8.5<br>0.841<br>0.841<br>5.40<br>5.40<br>5.50<br>0.911   |
| S PER CUB  | 9                   | 1/31/85<br>30<br>7.1<br>7.5                        | 0.950<br>5.10<br>0.966<br>40                                       | 10.5<br>10.8<br>60<br>4.0<br>0.75.2<br>0.763                                    | 22.8<br>6.6<br>6.6<br>6.6                            | 0.41/<br>0.710<br>0.910<br>9.60<br>1.11  | 0.870<br>7.9<br>8.1<br>0.985                                    | 71<br>3/85<br>220<br>11.1<br>12.1<br>0.921<br>440<br>440<br>8.1<br>0.606  |
| II CROGRAM | ∞ ]                 | 78<br>2/24/85<br>210<br>10.4<br>11.2               | 0.924<br>190<br>8.2<br>0.949<br>240                                | 8.6<br>8.6<br>260<br>13.6<br>0.851  | 9/ 4/85<br>250<br>11:8                               | 0.944<br>0.85.3<br>0.635<br>0.635<br>0.635<br>0.635<br>0.635<br>0.744<br>0.844<br>0.844<br>0.8240<br>0.635<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.844<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.835<br>0.8350<br>0.8350<br>0.8350<br>0.835000<br>0.83500000000000000000000000000000000000 | 0.992   | 5/13/85<br>5/13/85<br>230<br>230<br>10.7<br>11.8<br>0.909<br>7.3<br>0.907<br>0.807                                  |
| UNITS : M  | 7                   | 2/18/85<br>260<br>10.0<br>11.8                     | 0.847<br>270<br>8.8<br>10.1<br>0.871<br>270                        | 10.4<br>10.6<br>290<br>16.9<br>17.3<br>0.981                                    | 70<br>70<br>220<br>12.6<br>13.2                      | 0.922<br>8.22<br>0.893<br>14.60<br>14.86   | 0.988<br>220<br>11.8<br>12.4<br>0.957                           | 74<br>74<br>5.4<br>8.9<br>0.604<br>2.3<br>2.3<br>0.359  |
|            | 6<br>VIN)<br>0      | 3/20/85<br>250<br>9.5<br>13.9                      | 0.678<br>290<br>6.8<br>10.1<br>0.674<br>270                        | 7.6<br>10.2<br>140<br>14.0<br>15.2<br>0.916                                     | 2/21/85 1<br>300<br>7.9<br>8.6                       | 0.914<br>330<br>4.7<br>0.731<br>8.10<br>8.0<br>0.0<br>0.0  | 0.865<br>310<br>5.1<br>0.724                                    | 75<br>2/24/85<br>210.4<br>11.2<br>0.924<br>8.2<br>8.2<br>8.2<br>8.2<br>0.949  |
|            | Ŀ                   | 81<br>4/19/85<br>260<br>8.4<br>11.4                | 0.735<br>340<br>3.2<br>4.5<br>0.717<br>180                         | 3.1<br>7.2<br>0.438<br>10.5<br>0.534  | (NU)<br>3/20/85 1<br>2250<br>9.5                     | 0.678<br>16.8<br>16.8<br>16.74<br>10.674<br>7.70   | 0.740<br>14.0<br>15.2<br>0.916                                  | 0/10/85<br>240<br>13.0<br>13.7<br>0.955<br>5.0<br>5.1<br>0.553<br>0.553   |
|            | ± /                 | 84<br>3/8/85<br>220<br>11.1<br>12.1                | 0.921<br>240<br>4.9<br>8.1<br>0.606<br>240                         | 10.7<br>10.8<br>19.6<br>20.4<br>0.958   | 2/ 9/85<br>2/ 9/85<br>5.8                            | 0.848<br>2.8<br>2.8<br>2.70<br>5.6<br>5.6  | 0.945<br>5.7<br>0.90 <u>4</u><br>0.90 <u>4</u><br>0.90 <u>4</u> | 22 85<br>270 85<br>4.9<br>0.848<br>330<br>3330<br>3.18<br>3.18<br>0.759   |
|            | R<br>M              | 3/26/85<br>300<br>11.0<br>12.8                     | 0.858<br>330<br>7.3<br>0.978<br>0.978<br>320                       | 0.958<br>0.931<br>13.2<br>0.960   | 2/18/85 1<br>260<br>10.0<br>11.8                     | 0.847<br>270<br>8.8<br>10.1<br>0.871<br>270<br>270<br>270  | 0.981<br>1290<br>17.3<br>0.981                                  | 9/ 4/85 1<br>86<br>11.8<br>11.8<br>11.8<br>0.944<br>5.3<br>8.3<br>0.635   |
|            | 2<br>MN             | 5/ 1/85<br>300<br>3.2<br>9.6                       | 0.335<br>10<br>5.4<br>0.717<br>0.717<br>280                        | 0.341<br>0.341<br>0.290<br>11.9<br>0.793  | 5/ 1/85<br>3.2<br>9.6                                | 0.335<br>0.710<br>2280<br>280<br>280   | 0.341<br>290<br>11.9<br>0.793                                   | 89<br>89<br>260<br>8.4<br>11.4<br>0.735<br>3.2<br>3.2<br>0.737<br>0.737<br>0.737<br>0.737                           |
|            | - 7                 | 101<br>2/27/85<br>220<br>12.6<br>13.2              | 0.952<br>210<br>8.2<br>0.893<br>0.893<br>240                       | 14.6<br>14.8<br>0.988<br>11.8<br>12.4<br>0.957                                  | 100<br>4/19/85<br>8.4<br>11.4                        | 0.735<br>340<br>3.2<br>4.5<br>180<br>180<br>3.1  | 0.438<br>300<br>10.56<br>0.534                                  | 5/10<br>3.2<br>3.2<br>0.335<br>0.335<br>0.335<br>0.717<br>0.717   |
|            | RANK                | TSP<br>DATE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG) | VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO | TSP<br>DATE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)   | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>VEL (MPH)   | SATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO           | TSP<br>DATE<br>DATE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>RATIO |
|            | TOWN-SITE (SAMPLES) | MERIDEN-002 (59)<br>METEOROLOGICAL SITE<br>NEWARK  | METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE              | METEOROLOGICAL SITE<br>WORCESTER  | MIDDLETOWN-003 (57)<br>METEOROLOGICAL SITE<br>NEWARK | METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT  | METEOROLOGICAL SITE<br>WORGESTER                                | MILFORD-002 (60)<br>METEOROLOGICAL SITE<br>NEWARK<br>METEOROLOGICAL SITE<br>BRADLEY                                 |

TABLE 11, CONTINUED 1985 TEN HIGHEST 24-HOUR AVERAGE TSP DAYS WITH WIND DATA

G 7/ 6/85 2.00 8.3 0.953 0.957 0.957 0.957 0.957 0.957 0.957 0.956 0.966 7/24/85 150 0.41.2 0.41.2 0.41.2 0.490 0.550 0.717 0.717 0.717 0.717 0.717 0.717 0.717 0.717 0.717 0.717 UNITS : MICROGRAMS PER CUBIC METER 260 9.6 11.1 0.864 5.3 7.3 0.726 > 10 7 1/7/85 2.8 2.8 2.8 6.6 6.8 6.8 0.910 7.5 0.910 0.910 0.870 0.870 0.85 240 10.7 10.8 0.996 270 270 20.4 0.958 N. S. F. 44 δ 5/31/85 1900 1900 10.969 10.1 1900 1900 1900 1900 13.8 13.8 0.988 13.8 0.988 0.988 0.988 0.988 200 7.4 7.4 8.1 0.916 8.4 0.886 ω 10/10/85 240 240 13.7 0.955 5.0 250 0.553 0.978 0.978 0.978 0.978 0.978 0.9555 0.9555 0.9555 0.9555 0.95555 0.95555 54 230 3.3 5.3 5.3 5.3 0.620 11.0 11.5 0.955  $\sim$ 5,4% 3300 33.25 3300 33.25 3300 33.55 3300 33.55 3300 33.55 12/27/85 75 12:20 13:25 13:25 13:25 0.952 0.952 0.952 0.952 0.952 0.952 0.957 0.957 0.957 240 8.6 8.6 8.6 0.997 13.6 13.6 15.0 0.851 9 3/ 76 3/ 85 11.1 12.1 12.1 0.921 0.926 0.926 0.926 10.8 10.8 10.7 10.8 10.8 10.8 10.958 0.958 0.958 6/18/85 230 231 231 231 231 230 190 190 6.7 6.7 6.7 0.946 0.946 0.946 0.950 0.950 240 9.5 9.5 0.978 250 9.6 0.955 ŝ 7 5/31/85 19.9 19.9 19.9 19.9 190 190 190 190 190 13.8 13.9 0.967 13.9 0.967 0.988 0.988 0.988 0.988 270 5.6 5.9 5.9 5.7 5.7 0.904 7 4 2 81 4/19/85 260 8.4 11.4 0.735 340 340 3.2 0.715 0.717 180 3.1 7.2 300 300 5.6 10.5 0.534 ŝ 5.1 5.3 0.966 10.5 10.8 4.0 5.2 0.763 180 3.1 7.2 0.438 300 300 55.6 0.534 60 7 N 5/1/85 5/1/85 300 3.2 0.335 0.335 280 2.9 8.6 8.6 0.341 290 9.5 0.793 5.4 2.280 2.280 2.280 2.280 2.41 2.590 2.290 2.590 0.793 0.793 R 66 7 -DIR (DEG) VEL (MPH) SPD (MPH) DIR (DEG) VEL (MPH) SPD (M DIR (DEG) VEL (MPH) SPD (MPH) RATIO VEL (MPH) VEL (MPH) SPD (MPH) RATIO TSP DATE DATE DIR (DEG) VEL (MPH) VEL (MPH) RATIO DIR (DEG) VEL (MPH) SPD (MPH) SPD (MPH) SPD (MPH) CIR (DEG) VEL (MPH) SPD (M TSP DATE RANK METEOROLOGICAL SITE WORCESTER MÉTEOROLOGICAL SITE NEWARK METEOROLOGICAL SITE WORCESTER METEOROLOGICAL SITE NEWARK METEOROLOGICAL SITE WORCESTER METEOROLOGICAL SITE BRIDGEPORT METEOROLOGICAL SITE BRADLEY METEOROLOGICAL SITE BRIDGEPORT METEOROLOGICAL SITE BRADLEY METEOROLOGICAL SITE BRIDGEPORT TOWN-SITE (SAMPLES) NAUGATUCK-001 (60) MORRIS-001 (60)

|            |                     |                        |                                     | ha.  |  |  |                      |   | l'u  |  |   |   | 2   |
|------------|---------------------|------------------------|-------------------------------------|--|--|--|----------------------|---|--|--|---|---|---|
| IC METER   | 10                  | 53<br>53               | 10/ 10/ 00<br>240<br>13.0           | 0.979<br>230<br>9.10<br>0.1                  | 0.553<br>240<br>9.3<br>9.5                   | 0.978<br>250<br>10.1<br>0.955  | Sel<br>Sel           | 5/25/85<br>120<br>3.3<br>7.5                | 0.438<br>170<br>1.9                          | 0.407<br>3.9<br>4.7                          | 0.828<br>210<br>7.7<br>8.9<br>0.861                   | 52<br>2/24/85<br>210                        | 10.4<br>11.2<br>190<br>8.2<br>8.6<br>0.949  |
| S PER CUB  | 6                   | 59<br>59               | 250<br>11.8<br>12.5                 | 0.944<br>240<br>5.3<br>8.3                   | 0.635<br>260<br>9.7<br>9.8                   | 0.992<br>250<br>12.1<br>0.957  | 58                   | 10/10/85<br>240<br>13.0<br>13.7             | 0.955<br>230<br>5.0                          | 0.553<br>240<br>9.5<br>9.5                   | 0.978<br>250<br>9.6<br>0.955                          | NE<br>53<br>1/ 7/85                         | 0.910<br>0.910<br>0.910<br>0.910  |
| 41 CROGRAM | œ                   | 7.00<br>10<br>10<br>10 | 210<br>210<br>11.2                  | 0.924<br>190<br>8.2<br>8.6                   | 0.949<br>240<br>8.6<br>8.6                   | 0.997<br>260<br>13.6<br>0.851  | (MN)9                | 12/21/85<br>300<br>7.9<br>8.6               | 0.914<br>330<br>4.7<br>6.5                   | 0.731<br>310<br>8.0<br>9.2                   | 0.865<br>310<br>5.1<br>7.0<br>0.724                   | 54<br>54<br>240                             | 0.553<br>0.555<br>0.553<br>0.553<br>0.553   |
| UNITS : 1  | 7                   | 59<br>12 / 20 / 0E     | 260<br>10.5<br>11.1                 | 0.949<br>270<br>8.2<br>11.1                  | 0.744<br>270<br>14.2<br>14.4                 | 0.991<br>240<br>10.4<br>11.1<br>0.93Z  |                      | 3/20/85<br>250<br>13.9                      | 0.678<br>290<br>6.8<br>10.1                  | 0.674<br>270<br>7.6<br>10.2                  | 0.740<br>280<br>14.0<br>15.2<br>0.916                 | 54<br>54<br>6/18/85<br>230                  | 0.8894<br>190<br>8.1<br>0.989<br>0.989  |
|            | 9                   | 62<br>62               | 230<br>8.9<br>10.1                  | 0.887<br>210<br>4.9<br>5.9                   | 0.831<br>240<br>10.9<br>11.4                 | $0.959 \\ 240 \\ 9.1 \\ 10.9 \\ 0.830 \\ 0.930 \\ 0.930 \\ 0.930 \\ 0.950 \\ 0$ | 62                   | 12/27/85<br>220<br>12.6<br>13.2             | 0.952<br>210<br>9.2                          | 0.893<br>240<br>14.6<br>14.8                 | 0.988<br>220<br>11.8<br>12.4<br>0.957                 | 12/27/85                                    | 12.6<br>13.2<br>210<br>8.2<br>8.2<br>0.893  |
|            | 2                   | 63<br>1, 7,%           | 2.8<br>6.6                          | 0.417<br>10<br>6.8<br>7.5                    | 0.910<br>40<br>9.6<br>11.1                   | $\begin{array}{c} 0.870 \\ 70 \\ 7.9 \\ 8.1 \\ 0.985 \end{array}$  | 65                   | 2/24/85<br>210<br>10.4<br>11.2              | 0.924<br>190<br>8.2                          | 0.949<br>240<br>8.6<br>8.6                   | 0.997<br>260<br>13.6<br>16.0<br>0.851                 | NW<br>55<br>300<br>300                      | 0.914<br>0.914<br>330<br>4.7<br>4.7<br>0.731  |
|            |                     | 65<br>65               | 230<br>230<br>10.7<br>11.8          | 0.909<br>180<br>7.3<br>9.1                   | 0.807<br>200<br>7.4<br>8.1                   | 0.916<br>220<br>8.4<br>0.886   | 229                  | 5/13/85<br>230<br>10.7<br>11.8              | 0.909<br>180<br>7.3<br>9.1                   | 0.807<br>200<br>7.4<br>8.1                   | 0.916<br>220<br>8.4<br>9.5<br>0.886                   | 5/13/85                                     | 10.7<br>11.8<br>0.909<br>180<br>7.3<br>9.1<br>0.807                                 |
|            | 3                   |                        | 300<br>3.2<br>9.6                   | 0.335<br>5.4<br>7.5                          | 0.717<br>280<br>2.9<br>8.6                   | 0.341<br>290<br>9.5<br>11.9<br>0.793   | 68                   | 4/19/85<br>260<br>8.4<br>11.4               | 0.735<br>340<br>3.2<br>4.5                   | 0.717<br>180<br>3.1<br>7.2                   | 0.438<br>300<br>5.6<br>0.534                          | 66<br>44/19/85<br>260                       | 111.4<br>0.735<br>340<br>3.2<br>0.717   |
|            | N                   | (NW)<br>700,85         | 3/20/03<br>9.5<br>13.9              | 0.678<br>5.90<br>6.8<br>10.1                 | 0.674<br>270<br>7.6<br>10.2                  | 0.740<br>280<br>14.0<br>15.2<br>0.916  |                      | 5/ 1/85<br>300<br>3.2<br>9.6                | 0.335<br>10<br>7.5                           | 0.717<br>280<br>2.9<br>8.6                   | 0.341<br>290<br>9.5<br>11.9<br>0.793                  | 68<br>9/ 4/85<br>250                        | 11.8<br>12.5<br>244<br>5.3<br>6.3<br>0.635  |
|            | 1                   | 76                     | 4/ 19/00<br>260<br>8.4<br>11.4      | 0.735<br>340<br>3.2<br>4.5                   | 0.717<br>180<br>3.1<br>7.2                   | 0.438<br>300<br>5.6<br>0.534   | 62                   | 9/ 4/85<br>250<br>11.8<br>12.5              | 0.944<br>240<br>5.3<br>8.3                   | 0.635<br>9.7<br>9.8                          | 0.992<br>250<br>11.6<br>0.957                         | 5/ 1/85<br>300                              | 0.335<br>9.6<br>10<br>5.4<br>0.717  |
|            | RANK                | TSP                    | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO  | TSP                  | DATE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO | TSP<br>DATE<br>DIR (DEG)                    | VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>SPD (MPH) |
|            | TOWN-SITE (SAMPLES) | NEW BRITAIN-007 (59)   | METEOROLOGICAL SITE                 | METEOROLOGICAL SITE  <br>BRADLEY             | METEOROLOGICAL SITE<br>BRIDGEPORT            | METEOROLOGICAL SITE<br>WORCESTER   | NEW BRITAIN-008 (59) | METEOROLOGICAL SITE<br>NEWARK               | METEOROLOGICAL SITE<br>BRADLEY               | METEOROLOGICAL SITE<br>BRIDGEPORT            | METEOROLOGICAL SITE<br>WORCESTER                      | NEW BRITAIN-009 (56)<br>METEOROLOGICAL SITE | NEWARK<br>METEOROLOGICAL SITE<br>BRADLEY  |

1985 TEN HIGHEST 24-HOUR AVERAGE TSP DAYS WITH WIND DATA

TABLE 11, CONTINUED

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|      |  | 196  | 35 TEN HII                            | GHEST 24-                             | HOUR AVER.                                 | AGE TSP D/                                 | AYS WITH                            | WIND DATA                                      | UNITS : I                            | MICROGRAMS                           | S PER CUB                                      | C METER                               |   |
|------|--|--|---------------------------------------|---------------------------------------|--|--|-------------------------------------|--|--------------------------------------|--------------------------------------|--|---------------------------------------|---|
| TOWN | I-SITE (SAMPLES)                             | RANK   | ۳                                     | 2                                     | ε  | 4  | ŝ                                   | 9  | 7                                    | Ø                                    | . 0  | 10                                    |   |
|      | METEOROLOGICAL SITE<br>BRIDGEPORT            | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)                                | 280<br>2.9<br>8.6                     | 260<br>9.7<br>9.8                     | 180<br>3.1<br>7.2                          | 200<br>7.4<br>8.1                          | 310<br>8.0<br>9.2                   | 240<br>14.6<br>14.8                            | 220<br>6.7<br>7.0                    | 240<br>9.3<br>9.5                    | 40<br>9.6<br>11.1                              | 240<br>8.6<br>8.5                     |   |
|      | METEOROLOGICAL SITE<br>WORCESTER             | KALLO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO              | 0.341<br>290<br>11.9<br>0.793         | 250<br>250<br>11.6<br>0.957           | 0.438<br>300<br>10.56<br>0.534             | 0.886<br>0.886                             | 0.724                               | 0.988<br>220<br>11.8<br>12.4                   | 0.946<br>210<br>7.4<br>7.8<br>0.950  | 0.978<br>250<br>9.6<br>10.1<br>0.955 | 0.870<br>7.9<br>8.1<br>0.985                   | 0.997<br>260<br>13.6<br>16.0<br>0.851 |   |
| NEW  | HAVEN-002 (51)<br>METEODOLOCICAL SITE        | TSP<br>DATE<br>DIP (DEC)   | 5/ 1/85                               | (NW)<br>121<br>7/30/85                | 1/31/85                                    | 1/1/85                                     | 77<br>1/13/85                       | 9/ 5/85  | 75 .<br>1/19/85                      | 10/10/85                             | 2/18/85  | 2/24/85                               |   |
|      | METEOROLOGICAL SITE                          | VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)                       | 3.2<br>9.6<br>0.335                   | 0.609<br>0.609<br>0.609<br>0.609      | 7.1<br>7.5<br>0.950                        | 2.8<br>6.6<br>0.417                        | 200<br>12.7<br>13.4<br>0.947<br>280 | 0.2<br>0.884<br>0.884                          | 240<br>8.5<br>0.841<br>240           | 240<br>13.0<br>0.955<br>230          | 10.0<br>11.8<br>0.847<br>270                   | 2.10<br>10.4<br>11.2<br>0.924<br>190  |   |
|      | BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT | VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)          | 5.4<br>0.715<br>280<br>2.9            | 4.4<br>6.0<br>260<br>6.3              | 5.1<br>0.966<br>10.5                       | 6.8<br>7.5<br>0.910<br>40<br>9.6           | 4.0<br>6.2<br>0.645<br>9.9          | 1.3<br>3.6<br>0.349<br>6.0                     | 5.0<br>0.911<br>9.6                  | 5.0<br>9.1<br>240<br>9.3             | 8.8<br>10.1<br>0.871<br>270<br>10.4            | 8.2<br>8.6<br>249<br>8.6<br>8.6       |   |
|      | METEOROLOGICAL SITE<br>WORCESTER             | SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO | 8.6<br>0.341<br>2290<br>11.9<br>0.793 | 0.7792<br>280<br>5.0<br>0.674         | 10.8<br>0.974<br>60<br>4.0<br>5.2<br>0.763 | 11.1<br>0.870<br>70<br>7.9<br>8.1<br>0.985 | 0.973<br>310<br>9.8<br>0.925        | 7.0<br>0.854<br>270<br>7.9<br>8.3<br>0.945     | 11.1<br>0.864<br>5.3<br>7.3<br>0.726 | 9.5<br>250<br>9.6<br>10.1            | 10.6<br>0.981<br>290<br>16.9<br>0.981<br>0.981 | 8.6<br>260<br>13.6<br>16.0<br>0.851   |   |
| NEW  | HAVEN-013 (55)                               | TSP  | WW<br>99                              | 99                                    | 75   | 74   | ALL ALL                             | 68   | 19                                   | 767                                  | NE SE  | 292<br>655                            |   |
|      | METEOROLOGICAL SITE<br>NEWARK                | DATE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)                        | 2/ 1/85<br>300<br>3.2<br>9.6          | 4/19/85<br>260<br>8.4<br>11.4<br>11.4 | 10/10/85<br>240<br>13.0<br>13.7            | 9/ 4/85<br>250<br>11.8<br>12.5             | 2.8<br>2.8<br>6.6                   | 210<br>210<br>10.4<br>210<br>210<br>200<br>200 | 230<br>230<br>10.7<br>11.8           | 3/ 8/89<br>220<br>11.1<br>12.1       | 7.1/80<br>30<br>7.1<br>7.5                     | 1/19/85<br>240<br>8.5<br>10.1         |   |
|      | METEOROLOGICAL SITE<br>BRADLEY               | VEL (MPH)<br>SPD (MPH)<br>SPD (MPH)                                | 0.33<br>7.5<br>7.5<br>7.5             | 020<br>340<br>4-5<br>7-7              | 0.230<br>9.10<br>6.1                       | 0.744<br>5.3<br>8.3<br>8.3                 | 0.417<br>6.8<br>7.5                 | 0.924<br>8.20<br>0.62<br>0.62                  | 0. 400<br>180<br>9. 1<br>2. 3        | 0.72-1<br>240<br>8.19                | 0.00<br>                                       | 0.841<br>220<br>5.50<br>6.52<br>6     | - |
|      | METEOROLOGICAL SITE<br>BRIDGEPORT            | VEL (MPH)<br>VEL (MPH)<br>SPD (MPH)                                | 280<br>2.9<br>8.6<br>311              | 3.1                                   | 0.10<br>9.3<br>0.5<br>078                  | 0.00<br>0.7<br>0.8<br>0.0<br>0.8           | 9.6<br>11.1<br>870                  | 240<br>240<br>8.6<br>8.6                       | 200<br>200<br>8.1<br>8.1             | 0.000<br>240<br>10.7<br>10.8         |  | 9.60<br>11.1                          |   |
|      | METEOROLOGICAL SITE<br>WORCESTER             | VEL (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>RATIO                       | 0.793<br>9.5<br>11.9<br>0.793         | 0.534                                 | 250<br>9.6<br>10.1                         | 250<br>250<br>11.6<br>12.1<br>0.957        | 70<br>70<br>7.9<br>8.1<br>0.985     | 260<br>260<br>13.6<br>0.851                    | 0.320<br>8.4<br>0.886                | 0.990<br>270<br>20.4<br>0.958        | 0.974<br>60<br>5.2<br>0.763                    | 0.0004<br>5.3<br>0.726                |   |

(\_\_\_\_\_\_\_\_)

TABLE 11, CONTINUED

1985 TEN HIGHEST 24-HOUR AVERAGE TSP DAYS WITH WIND DATA

| R          | C                   | - north  | 35       |                               | )     | `.^                            |                    |                     |                        |       |                                  |               |   |       | ц<br>С           | 0                   |                        |       |                     |              | 9                   |            |                |                     |              |       |           |                  | 35                  | /                 | ~                  | ).                             |                    |
|------------|---------------------|----------|----------|-------------------------------|-------|--------------------------------|--------------------|---------------------|------------------------|-------|----------------------------------|---------------|---|-------|------------------|---------------------|------------------------|-------|---------------------|--------------|---------------------|------------|----------------|---------------------|--------------|-------|-----------|------------------|---------------------|-------------------|--------------------|--------------------------------|--------------------|
| 31C METE   | 10/                 | NE<br>S  | 3/20/8   | 000<br>13.00<br>13.00         | 0.678 | 290<br>6.8                     | 10.1               | 270                 | 10.5                   | 0.740 | 280<br>14 0                      | 15.2          | 0.210                                   | 2     | 10/10/9          | 240                 | 13.0                   | 0.955 | 230                 | 0.0          | 0.553               | 9.3        | 9.5            | 250                 | 9.6          | 0.955 | 7         | 61               | 10/10/8             | 13.0              | 13./<br>0 955      | 230                            | 9.1<br>0.553       |
| IS PER CUE | . 6                 | 7:       | 6/18/85  | 1920                          | 0.894 | 190<br>8.1                     | 0 080<br>0 080     | 220                 | 2.7<br>2               | 0.946 | 210<br>7.4                       | 7.8           | 016.0                                   | 7:    | 12/27/85         | 220                 | 12.6                   | 0.952 | 210                 | 9.2<br>0     | 0.893               | 14.6       | 14.8           | 220                 | 11.8         | 0.957 | (B)<br>II | 61               | 6/30/85             | 3 C               | 0.530              | 30                             | 4.5<br>0.415       |
| MICROGRAM  | 8                   | N.S.     | 2/18/85  | 10.01                         | 0.847 | 2/0<br>8.8                     | 10.1               | 270                 | 10.4                   | 0.981 | 290<br>16.9                      | 17.3          |   | NA MA | 12/ 0/85         | 270                 | л.<br>2<br>2           | 0.848 | 330                 | 3.7          | 0.759               | 5.6        | 5.9<br>015     | 280                 | 5.7          | 0.904 | 4         | 61               | 12/27/85            | 12.6              | 13.2<br>0.952      | 210<br>2                       | 9.2<br>0.893       |
| UNITS :    | 7                   | 2        | 10/10/85 | 13.0<br>13.7                  | 0.955 | 230<br>5.0                     | 9.1<br>0 553       | 240                 | 0<br>0<br>0            | 0.978 | 250<br>9.6                       | 10.1          | ( C C C C C C C C C C C C C C C C C C C | 2     | 77<br>5/13/85    | 230                 | 10.7<br>11 8           | 0.909 | 180                 | 9.1          | 0.807               | 7.4        | 0 016<br>0 016 | 220                 | 8.4<br>7.4   | 0.886 |           | 65<br>(65        | 1/19/85             | 100<br>100<br>100 | 0.841              | 240                            | 0.911              |
|            | 9                   | 7.       | 2/24/85  | 10.4                          | 0.924 | 190<br>8.2                     | 8.6<br>0 0/10      | 240                 | 8.<br>9.0<br>9.0       | 0.997 | 260<br>13.6                      | 16.0          | 1000                                    | 21    | 77<br>3/ 8/85    | 220                 | 1.11                   | 0.921 | 240                 | 8.1.<br>2.1. | 0.606               | 10.7       | 10.8<br>0 006  | 270                 | 19.6         | 0.958 | S.E.      | 61               | 1/ 7/85             | 0,00              | 0.0                | 10                             | 0.910              |
|            | 5                   | 7 5      | 4/25/85  | оло<br>1-1-0<br>1-1-0         | 0.604 | 200<br>2.3                     | 6.5<br>0 350       | 230                 | ຕິ<br>ຕິ               | 0.620 | 250<br>11.0                      | 11.5<br>0 055 | (((.))                                  | 4     | 82<br>11/10/85   | 260                 | 8.4<br>11.4            | 0.735 | 340                 | 4.5          | 0.717               | 3.1        | 7.2            | 300                 | 5.6<br>7.6   | 0.534 | 7         | 69               | 9/ 4/85             | 11.8              | 0.944              | 240                            | 0.635              |
|            | 11                  | С Г<br>Г | 4/19/85  | 8.4<br>11.4                   | 0.735 | 340<br>3.2                     | 4.5<br>0 717       | 180                 | - ° °                  | 0.438 | 300<br>5.6                       | 10.5          | +00.0                                   | 73    | 82<br>0/ 1/85    | 250                 | 11.8<br>12.8           | 0.944 | 240                 | <br>         | 0.635               | 9.7        | 9.8<br>000     | 250                 | 11.6         | 0.957 | >         | 71               | 5/13/85             | 10.7              | 0.909              | 180                            | 9.1<br>0.807       |
|            | e l                 | NV.      | 12/_9/85 | 74.0<br>8                     | 0.848 | 330<br>2.8                     | 3.7<br>0 759       | 270                 | 00<br>00               | 0.945 | 280<br>5.7                       | 6.3<br>0 001  | +02.0                                   | 2     | 90<br>5/31/85    | 190                 | 9.9<br>10.2            | 0.969 | 190                 | 10.1         | 0.989               | 7.2        | 7.5            | 200                 | 13.8<br>13.8 | 0.988 |           | 71               | 4/19/85             | 8.4               | 0.735              | 340                            | 4.5<br>0.717       |
|            | 2                   | 3,2      | 5/ 1/85  | 3.2<br>9.6                    | 0.335 | 5.4                            | 715                | 280                 | 0.v<br>0.v             | 0.341 | 290<br>9.5                       | 11.9          |   | SP    | 95<br>1/7/85     | 1007- 11            | 2.8<br>7.8             | 0.417 | 10                  | 7.5          | 0.910               | 9.6        | 11.1<br>0 870  | 70                  | 7.9<br>. 6   | 0.985 |           | 72               | 2/18/85             | 10.0              | 0.847              | 270<br>8 8                     | 0.871              |
|            |                     | 7 5      | 5/13/85  | 10.7                          | 0.909 | 180<br>7.3                     | 9.1<br>0 807       | 200                 | 7.4                    | 0.916 | 220<br>8.4                       | 9.5<br>0 886  |   |       | П1<br>5/ 1/85    | 300                 | 3.2<br>9.2             | 0.335 | 10                  | <br>         | 0.717               | 2.9        | 8.6<br>0 3/11  | 290                 | 0.1<br>2.0   | 0.793 | (MN)      | 108              | 5/ 1/85             |                   | 9.0                | ء<br>10                        | 7.5<br>0.717       |
|            | RANK                | TCD      | DATE     | VEL (MPH)<br>SPD (MPH)        | RATIO | VEL (MPH)                      | SPD (MPH)<br>RATIO | DIR (DEG)           | VEL (MPH)<br>SPD (MPH) | RATIO | VEL (MPH)                        | SPD (MPH)     |   |       | TSP<br>DATE      | DIR (DEG)           | VEL (MPH)<br>SPD (MPH) | RATIO | DIR (DEG)           | SPD (MPH)    | RATIO               | VEL (MPH)  | SPD (MPH)      | DIR (DEG)           | VEL (MPH)    | RATIO |           | TSP              | DATE                | VEL (MPH)         | SPD (MPH)<br>RATIO | DIR (DEG)                      | SPD (MPH)<br>RATIO |
|            | TOWN-SITE (SAMPLES) |          |          | METEURULUU UAL STTE<br>NEWARK |       | METEUROLOGICAL STIE<br>BRADLEY |                    | METEOROLOGICAL SITE | BRIDGEPORT             |       | METEOROLOGICAL STIE<br>WORCESTER |               |   |       | NORWALK-005 (57) | METEOROLOGICAL SITE | NEWARK                 |       | METEOROLOGICAL SITE | BNAULET      | METEOROLOGICAL SITE | BRIDGEPORT |                | METEOROLOGICAL SITE | WORCESTER    |       |           | NORWALK-012 (59) | METEOROLOGICAL SITE | NEWARK            |                    | METEOROLOGICAL SITE<br>READIEV |                    |

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1985 TEN HIGHEST 24-HOUR AVERAGE TSP DAYS WITH WIND DATA UNITS : MICROGR

| R           |                     |                                     | 1   | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | 3<br>2                         |                      | S  | ~                                 |                    |                                  | /                  | /~~<br>// ass | 35                |                               | (                  | 4                              |                |                                   |                    |                                  |            |
|-------------|---------------------|-------------------------------------|---|---|--------------------------------|----------------------|--|-----------------------------------|--------------------|----------------------------------|--------------------|---------------|-------------------|-------------------------------|--------------------|--------------------------------|----------------|-----------------------------------|--------------------|----------------------------------|------------|
| SIC METE    | 10                  | 240<br>9.5<br>9.5                   | 0.950<br>9.60<br>10.10                                | 63<br>63                                | 12/ 9/{<br>270<br>4.9          | 0.848                | 2.8<br>3.78<br>3.78  | 0.759<br>270<br>5.6               | 5.9                | 280                              | 0.904              | NW            | 12/ 9/8           | 270                           | 5.8<br>0.848       | 100<br>7.00<br>7.00<br>7.00    | 0.759          | 5.6                               | 5.9<br>0.945       | 280                              | 0.3        |
| S PER CUE   | 6                   | 110<br>3.5<br>4.9                   | 0.74<br>360<br>5.2<br>0.374                           | 19                                      | 9/10/85<br>350<br>2.0          | $\frac{7.5}{10.261}$ | 4.1<br>6.1   | 0.897<br>90<br>2.1                | 4.5<br>0.481       | 30<br>4.1                        | 0.985              | (m)           | 3/20/85           | 250<br>9.5                    | 13.9<br>0.678      | 260<br>0.8<br>1<br>0.8         | 0.674          | 2.10                              | 10.2<br>0.740      | 280<br>14.0                      | 15.2       |
| M I CROGRAM | ω                   | 240<br>14.6<br>14.8                 | 0.958<br>11.8<br>12.4<br>0.957                        | 68<br>68                                | 2/18/85<br>260<br>10.0         | 11.8<br>0.847        | 8.8<br>10.1  | 0.871<br>270<br>10.4              | 10.6               | 290<br>16.9                      | 0.981              | 7             | 91<br>10/10/85    | 240<br>13.0                   | 13.7<br>0.955      | 230<br>5.0                     | 0.553          | 240<br>9.3                        | 9.5<br>0.978       | 250<br>9.6                       | 10.1       |
| UNITS :     | 7                   | 260<br>9.6<br>11.1                  | 0.726<br>0.726<br>0.726                               | 72                                      | 1/25/85<br>250<br>6.9          | 9.6<br>0.719         | 5.9<br>0.4   | 0.676<br>250<br>8.1               | 8.9<br>0.907       | 280<br>7.9                       | 0.802              | 7             | 100<br>6/18/85    | 230                           | 10.2<br>0.894      | 190<br>8.1                     | 0.989          | 6.7                               | 7.0<br>0.946       | 210<br>7.4                       | 7.8        |
|             | 9                   | 40<br>9.6<br>11.1                   | 0.8/0<br>70<br>8.1<br>0.985                           | MN                                      | 12/21/85<br>300<br>7.9         | 8.6<br>0.914         | 6.5<br>6.5   | 0.731<br>310<br>8.0               | 9.2<br>0.865       | 310<br>3.10                      | 0.724              | 2             | 108<br>12/27/85   | 220<br>12.6                   | 13.2<br>0.952      | 210<br>8.20                    | 0.893          | 14.6                              | 14.8<br>0.988      | 220<br>11.8                      | 12.4       |
|             | 5                   | 260<br>9.7<br>9.8                   | 0.992<br>250<br>11.6<br>12.1<br>0.957                 | 74                                      | 5/13/85<br>230<br>10.7         | 0.909                |  | 0.807<br>200<br>7.4               | 8.1<br>0.916       | 220<br>8.4                       | 0.886              | 7             | 110<br>5/13/85    | 230                           | 11.8<br>0.909      | 7.3                            | 0.807          | 7.4                               | 8.1<br>0.916       | 220<br>8.4                       | 9.5        |
|             | 4                   | 200                                 | 0.916<br>8.4<br>9.5<br>0.886                          | ,<br>86                                 | 4/19/85<br>260<br>8.4          | 11.4                 | 4.040  | 0.717<br>180<br>3.1               | 7.2<br>0.438       | 300<br>5.6                       | 0.534              | (NN)          | 7/30/85           | 290<br>6.0                    | 9.9<br>0.609       | 290<br>4.4                     | 0.723          | 200<br>6.3                        | 7.9                | 280<br>5.0                       | 7.5        |
|             | ŝ                   | 180<br>3.1<br>7.2                   | 0.438<br>300<br>5.6<br>0.534                          | 7 68                                    | 12/27/85<br>220<br>12.6        | 0.952                | 000<br>000<br>000  | 0.893<br>240<br>14.6              | 14.8<br>0.988      | 220<br>11.8                      | 0.957              | MM            | \119<br>6/ 6/85   | 330<br>11.5                   | 11.6<br>0.987      | 340<br>8.9                     | 0.940          | 340<br>10.5                       | 10.8<br>0.972      | 330<br>9.0                       | . 9<br>. 5 |
|             | 2                   | 270<br>10.4                         | 0.981<br>290<br>16.9<br>17.3<br>0.981                 | A CAR                                   | 1/31/85<br>30<br>7.1           | 0.950                | ۍ<br>  | $0.966 \\ 40 \\ 10.5$             | 10.8               | 4.0<br>F.J                       | 0.763              |               | 142<br>4/19/85    | 260<br>8.4                    | 0.735              | 340<br>3.2                     | 0.717          | 3.1                               | $7.2 \\ 0.438$     | 300<br>5.6                       | 10.5       |
|             | -                   | 280<br>2.9<br>8.6                   | 0.341<br>290<br>9.5<br>11.9<br>0.793                  | 159                                     | 9/ 4/85<br>250<br>11.8         | 12.5<br>0.944        | 8<br>8<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9 | 0.635<br>260<br>9.7               | 9.8<br>0.992       | 250<br>11.6                      | 0.957              | (MM)          | 765<br>5/ 1/85    | 300<br>3.2                    | 9.6<br>0.335       | ری<br>15 0                     | 0.717<br>0.217 | 2.9                               | $8.6 \\ 0.341$     | 290<br>9.5                       | 11.9       |
| -           | RANK                | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | KATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO | TSP                                     | DATE<br>DIR (DEG)<br>VEL (MPH) | SPD (MPH)<br>RATIO   | VEL (MPH)<br>SPD (MPH)   | RATIÓ<br>DIR (DEG)<br>VEL (MPH)   | SPD (MPH)<br>RATIO | VEL (MPH)                        | SPU (MPH)<br>RATIO |               | TSP<br>DATE       | DIR (DEG)<br>VEL (MPH)        | SPD (MPH)<br>RATIO | VEL (MPH)                      | RATIO          | VEL (MPH)                         | SPD (MPH)<br>RATIO | DIR (DEG)<br>VEL (MPH)           | SPD (MPH)  |
|             | TOWN-SITE (SAMPLES) | METEOROLOGICAL SITE<br>BRIDGEPORT   | METEOROLOGICAL SITE<br>WORCESTER                      | NORWICH-002 (54)                        | METEOROLOGICAL SITE<br>NEWARK  |                      | MELEURULUGICAL SLIE<br>BRADLEY   | METEOROLOGICAL SITE<br>BRIDGEPORT |                    | METEOROLOGICAL SITE<br>WORCESTER |                    |               | STAMFORD-001 (56) | METEOROLOGICAL SITE<br>NEWARK |                    | METEOROLOGICAL SITE<br>BRADLEY |                | MELEUKULUGICAL SILE<br>BRIDGEPORT |                    | METEOROLOGICAL SITE<br>WORCESTER |            |

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|                                   |                        |                   |                |                         | AGE 131 U          |                    |                       | UNITS :              | M I CROGRAM           | S PER CUB      | IC METER          |        |
|-----------------------------------|------------------------|-------------------|----------------|-------------------------|--------------------|--------------------|-----------------------|----------------------|-----------------------|----------------|-------------------|--------|
| TOWN-SITE (SAMPLES)               | RANK                   | -{:               | ~              | ю                       | th<br>T            | 5                  | 9                     | 7                    | 0                     | 6              | 101               |        |
| STAMFORD-007 (58)                 | TSP                    |                   | NN<br>102      | 94<br>1, 110 / 0E       | 82<br>82<br>82     | 82<br>1.79F        | NW<br>73              | 73<br>73<br>10/10/0E |                       | 1/ 1/0°        | 63<br>7 / 20 / 8E |        |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG)<br>VEL (MPH) | 300<br>300<br>3.2 | 17.5           | 4/ 19/ 03<br>260<br>8.4 | 230<br>230<br>10.7 | 250<br>250<br>11.8 | 270<br>270<br>4.9     | 240<br>240<br>13.0   | 0/29/07<br>340<br>4.6 | 2.8<br>2.8     | 290<br>290<br>6.0 |        |
|                                   | SPD (MPH)<br>RATIO     | 9.6<br>0.335      | 17.8<br>0.980  | 11.4<br>0.735           | 0.909              | 12.5<br>0.944      | 5.8<br>0.848          | 13.7<br>0.955        | 7.6<br>0.606          | 6.6<br>0.417   | 9.9<br>0.609      |        |
| METEOROLOGICAL SITE<br>BRADLEY    | VEL (MPH)              | 10<br>10<br>10    | 320            | 340                     | 180<br>7.3         | 5.3<br>5.3         | 330<br>2.8            | 230                  | 340<br>3.6            | 0<br>10<br>10  | 500<br>150<br>150 | $\sim$ |
|                                   | SPD (MPH)<br>RATIO     | 7.7<br>0.717      | 13.1<br>0.944  | 4.5<br>0.717            | 9.1<br>0.807       | 8.3<br>0.635       | 3.1<br>0.759          | 9.1<br>0.553         | 5.6<br>0.649          | ر.7<br>0.910   | 6.0<br>0.723      | S      |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)<br>VEL (MPH) | 280<br>2.9        | 330<br>13.8    | 180<br>3.1              | 200<br>7.4         | 260<br>9.7         | 270<br>5.6            | 240<br>9.3           | 340<br>2.7            | 40<br>9.6      | 260<br>6.3        |        |
|                                   | SPD (MPH)              | 8.6<br>0.311      | 13.9           | 7.2                     | 0 916              | 9.8<br>8.0         | 5.9<br>045            | 9.5<br>0 078         | 0.50                  | 11.1           | 7.9               |        |
| METEOROLOGICAL SITE               | DIR (DEG)              | 290               | 303            | 300                     | 220                | 250                | 280                   | 250                  | 300                   | 2022           | 280               |        |
| MONOES EN                         | SPD (MPH)              | 11.9              | 14.2           | 10.5                    | , 90<br>100        | 12.1               |                       | 10.1                 | مربع                  | - 80           |                   |        |
|                                   | RATIO                  | 0.793             | 0.929          | 0.534                   | 0.886              | 146.0              | 0.904                 | 6-95                 | 0.915                 | 0.985          | 0.6/4             |        |
|                                   |                        | (NEV)             |                | NS<br>M                 | 7                  | SE                 | Control of the second | NE                   |                       | e de           | NE                |        |
| STAMFORD-021 (53)                 | TSP<br>NATF            | (11/85<br>5/ 1/85 | 84<br>4/19/85  | 78                      | 73<br>10/10/85     | -73<br>12/ 9/85    | 64<br>6/18/85         | -63<br>6/12/85       | 62<br>10/22/85        | 61<br>12/27/85 |                   |        |
| METEOROLOGICAL SITE               | DIR (DEG)              | 300               | 260            |                         | 240                | 270                | 230                   | 290                  | 60                    | 220            | 30,77             |        |
| NEWAKK                            | SPD (MPH)              |                   | 11.4           | 9.9                     | 13.7               | 50<br>70<br>70     | 10.2                  | 12.2                 | 10.4                  | 13.2           | 7.5               |        |
| METEOROLOGICAL SITE               | RATIO<br>DIR (DEG)     | 0.335 $10$        | 0.735 340      | 0.417<br>10             | 0.955<br>230       | 0.848<br>330       | 0.894<br>190          | 0.517 20             | 0.660<br>200          | 0.952<br>210   | 0.950             | C      |
| BRADLEY                           | VEL (MPH)              | 5.4               | 3.2            | 6.8<br>2                | 5.0                | 2.8                |                       | 5.0                  | - c                   | 8.0            | 5.1               | $\sim$ |
|                                   | RATIO                  | 0.717             | 0.717          | 0.910                   | 0.553              | 0.759              | 0.989                 | 046.0                | 0.844                 | 9.2<br>0.893   | 0.966             |        |
| METEOROLOGICAL SITE<br>BRIDGFPORT | DIR (DEG)<br>VFI (MPH) | 280<br>2.9        | 180<br>3.1     | 40<br>9-6               | 240<br>9.3         | 270<br>5.6         | 220<br>6.7            | 40<br>6-1            | 80<br>4.9             | 240<br>14.6    | 40<br>10.5        |        |
|                                   | SPD (MPH)              | 8.6               | 7.2            | 11.1                    | 9.5                | 6.6                | 0.7                   |                      | 5.8                   | 14.8           | 10.8              |        |
| METFOROLOGICAL SITE               | RALIO<br>DIR (DEG)     | 0.341<br>290      | 0.438<br>300   | 0.8/0<br>70             | 0.9/8<br>250       | 0.945<br>280       | 0.946<br>210          | 0./61<br>40          | 0.85/<br>260          | 0.988<br>220   | 0.9/4<br>60       |        |
| WORCESTER                         | VEL (MPH)              | 9.5               | 5.6            | 7.9                     | 9.6                | 5.7                | 7.4                   | 7.3                  | 7.2                   | 11.8           | 4.0               |        |
|                                   | SPD (MPH)<br>RATIO     | 0.793             | 10.5           | 8.1<br>0.985            | 10.1               | 6.3<br>0.904       | 7.8<br>0.950          | 9.1<br>0.806         | 7.3<br>0.986          | 12.4<br>0.957  | 5.2<br>0.763      |        |
|                                   |                        | MM                |                |                         |                    | 7                  | (M                    | 1                    | 7                     | 7              | 7                 |        |
| STRATFORD-005 (58)                | TSP                    | 114               | 60             | 89                      | 83                 | 83                 | 83                    | 81<br>81             | 81                    | 78             | 76                |        |
| METEOROLOGICAL SITE               | DALE<br>DIR (DEG)      | イ8/1/イ<br>300     | 3/ 8/85<br>220 | 4/19/85<br>260          | 9/ 4/85<br>250     | 7/25/87<br>250     | 3/20/85<br>250        | 230 230              | 2/24/85<br>210        | 4/22/85<br>320 | 72/21/85<br>220   |        |
| NEWARK                            | VEL (MPH)              | 2.5<br>0<br>7     | 1.1.1          | 8.4<br>11.4             | 11.8               | 6.9<br>6.9         | 2.0                   | 10.7                 | 10.4                  | بر<br>م        | 12.6              |        |
|                                   | RATIO                  | 0.335             | 0.921          | 0.735                   | 0.944              | 0.719              | 0.678                 | 0.909                | 0.924                 | 0.604          | 0.952             | 4      |
| METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG)<br>VEL (MPH) | 10<br>5.4         | 240<br>4.9     | 340<br>3.2              | 240<br>5.3         | 240<br>4.0         | 290<br>6.8            | 180<br>7.3           | 190<br>8.2            | 200<br>2.3     | 8<br>210<br>210   |        |
|                                   | SPD (MPH)<br>RATIO     | 7.5<br>0.717      | 8.1<br>0.606   | 4.5<br>0.717            | 8.3<br>0.635       | 5.9<br>0.676       | 10.1<br>0.674         | 9.1<br>0.807         | 8.6<br>0.949          | 6.5<br>0.359   | 9.2<br>0.893      |        |
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TABLE 11, CONTINUED 1985 TEN HIGHEST 24-HOUR AVERAGE TSP DAYS WITH WIND DATA

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| IC METER  | 10                  | 240<br>14.6<br>14.8<br>0.988<br>12.8<br>12.4<br>0.957  | 4/158<br>260/81<br>111144<br>111144<br>111144<br>11117<br>11117<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>111777<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>111777<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177<br>11177 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| 6/12/8<br>6/12/8<br>6.3<br>0.517<br>0.517<br>0.517<br>0.940   | 40<br>6.1<br>8.1<br>8.1<br>0.761<br>140<br>7.3<br>9.1<br>0.806                                 |
| s per cub | 6                   | 230<br>250<br>250<br>250<br>250<br>250<br>250<br>250<br>250<br>250<br>25   | 9/ 41/85<br>250<br>12:50<br>12:58<br>11:58<br>12:58<br>0.944<br>5:33<br>5:33<br>5:33<br>5:33<br>5:33<br>5:33<br>5:33<br>5:  | 0.9928   | 5/19/85<br>12:0<br>14:2<br>0.842<br>7.90<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.842<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0 | 300<br>9.9<br>0.972<br>10.2<br>11.5<br>0.946   |
| MICROGRAM | ω                   | 240<br>8.6<br>8.6<br>997<br>13.6<br>0.851<br>0.851<br>0.851  | 12/27/85<br>65<br>12:20<br>13:26<br>0.952<br>8:2<br>8:2<br>8:2<br>8:2<br>8:2<br>8:2   | 0.957<br>0.988<br>0.988<br>0.988<br>0.957<br>0.957   | 7/ 6/85<br>200<br>7.6<br>7.6<br>7.6<br>8.3<br>0.913<br>6.9<br>0.913<br>0.913<br>0.913   | 190<br>6.7<br>0.957<br>8.3<br>0.966  |
| UNITS :   | 7                   | 0.855<br>0.916<br>0.8220<br>0.8355<br>0.8355   | 0.864<br>15.13<br>15.13<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14<br>15.14 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0.80<br>0.80<br>0.894<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86<br>0.86  | 7/30/85<br>290<br>6.0<br>0.609<br>0.609<br>1.4<br>4.4   | 260<br>6.3<br>0.792<br>5.80<br>7.5<br>0.674  |
|           | 9                   | 270<br>270<br>10.26<br>0.740<br>14.0<br>15.2<br>0.912<br>0.912   | 3/ 67<br>3/ 67<br>12:1<br>12:1<br>12:1<br>12:1<br>12:1<br>12:1<br>12:1<br>12:   | 2200<br>2200<br>10.7<br>10.7<br>220<br>20.4<br>20.4<br>20.4  | 3/20/85<br>3/20/85<br>250<br>9.5<br>0.678<br>6.8<br>0.674   | 270<br>17.6<br>0.740<br>15.2<br>15.2<br>0.916  |
|           | Ъ                   | 0.807<br>0.907<br>0.807<br>0.807<br>0.807<br>0.807<br>0.807<br>0.807<br>0.807<br>0.807<br>0.807<br>0.807<br>0.807<br>0.807<br>0.807<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.907<br>0.9070 | 5/13/85<br>2230<br>110.7<br>111.8<br>110.8<br>110.8<br>110.8<br>1180<br>1180<br>1180  | 0.2200<br>0.811<br>0.886<br>0.886  | 6/18/85<br>230<br>230<br>230<br>230<br>230<br>230<br>19/8<br>8.1<br>8.2<br>8.2<br>0.989   | 220<br>6.7<br>0.946<br>7.1<br>7.1<br>7.1<br>0.950  |
|           | 4                   | 260<br>9.7<br>12:50<br>12:10<br>0.952<br>12:10<br>0.951  | 3/20/85<br>3/20/85<br>9.55<br>250<br>290<br>290<br>290<br>290<br>290<br>290<br>290<br>290<br>290<br>29  | 0.214<br>0.7440<br>1440<br>15.2<br>0.916   | 9/ 4/85<br>250<br>250<br>11.8<br>11.8<br>0.944<br>5.3<br>5.3<br>0.635<br>0.635  | 260<br>9.7<br>9.8<br>9.8<br>0.992<br>11.6<br>12.1<br>0.957                                     |
|           | m                   | 0.534<br>0.538<br>0.538<br>0.556<br>0.534<br>0.534   | 2/24/85<br>210<br>210<br>10.44<br>11.2<br>0.924<br>8.2<br>8.2<br>8.2  | 0.851<br>0.851<br>0.856<br>0.851<br>0.851  | 5/31/85<br>190<br>190<br>190<br>190<br>190<br>10.1<br>0.989   | 190<br>7.5<br>0.967<br>200<br>13.8<br>0.988  |
|           | 0                   | 240<br>10.7<br>10.8<br>0.996<br>270<br>270<br>20.6<br>20.4<br>20.4   | 2/18/85<br>2/18/85<br>110.0<br>11.8<br>11.8<br>270<br>8.8<br>8.8<br>8.8<br>10.1   | 0.270<br>10.4<br>10.6<br>10.6<br>2290<br>2290<br>2290<br>2290<br>277.3<br>0.981  | 56<br>260<br>260<br>8.4<br>11.4<br>0.735<br>340<br>340<br>3.40<br>3.40<br>3.40<br>3.40<br>3.40<br>3.40<br>3   | 180<br>3.1<br>7.2<br>0.438<br>300<br>300<br>10.5<br>0.534                                      |
|           | -                   | 280<br>2.9<br>2.9<br>2.9<br>2.90<br>2.90<br>0.793<br>0.793   | 0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.9500<br>0.9500<br>0.9500<br>0.9500<br>0.9500<br>0.9500<br>0.9500<br>0.9500<br>0.9500<br>0.9500<br>0.9500<br>0.9500<br>0.9500<br>0.9500<br>0.95000<br>0.9500<br>0.9500<br>0.9500<br>0.95000<br>0.95000<br>0.95000<br>0.950  | 0.763<br>0.75.2<br>0.75.2<br>0.760<br>0.75.2<br>0.760<br>0.75.2  | 5/1/85<br>3.22<br>3.26<br>3.26<br>3.35<br>0.335<br>0.717  | 280<br>2.9<br>2.9<br>2.90<br>2.5<br>0.793<br>0.793   |
|           | RANK                | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO   | TSP<br>DATE<br>DATE<br>DIR (DEC)<br>VEL (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SATIO<br>SATIO  | NATIO<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>SPD (MPH)<br>SPD (MPH)<br>RATIO   | TSP<br>DATE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>DIR (DEG)<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>SPD (MPH)  | DIR (DEG)<br>- VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO |
|           | TOWN-SITE (SAMPLES) | METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>WORCESTER  | TORRINGTON-001 (60)<br>METEOROLOGICAL SITE<br>NEWARK<br>METEOROLOGICAL SITE<br>BRADLEY  | METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>WORCESTER  | VOLUNTOWN-001 (56)<br>METEOROLOGICAL SITE<br>NEWARK<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE   | METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>WORCESTER                          |

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1985 TEN HIGHEST 24-HOUR AVERAGE TSP DAYS WITH WIND DATA UNITS : MICROGRAMS PER CUBIC METER

|                     |                      |                                     | M  |                                       |   |                      |                                | ÷                                |  |  |                               | 1.1                                 | i   |
|---------------------|----------------------|-------------------------------------|--|---------------------------------------|---|----------------------|--------------------------------|----------------------------------|--|--|-------------------------------|-------------------------------------|---|
| 1                   | 74                   | -/ //07<br>40<br>2.8<br>6.6         | 0.417<br>10<br>6.8<br>7.5                      | 0.910<br>40<br>9.6                    | 0.870<br>70<br>8.1<br>0.985                           |                      | 7.95<br>300<br>7.9<br>8.6      | 0.914<br>8.30<br>6.5             | 0.731<br>310<br>8.0<br>9.2   | 0.865<br>310<br>5.1<br>7.0<br>0.724                        | (UW)<br>52<br>3/ 2/85         | 300                                 | 0.864<br>310<br>9.0<br>0.823                            |
| 6                   | 1, 1, 6F             | 1/31/00<br>30<br>7.1<br>7.5         | 0.950<br>5.1<br>5.3                            | 0.966<br>40<br>10.5                   | 0.974<br>60<br>5.2<br>0.763                           | 72                   | 240<br>240<br>13.0             | 0.955<br>230<br>5.0<br>9.1       | 0.553<br>240<br>9.3<br>9.5   | 0.978<br>250<br>9.6<br>10.1                                | (10)<br>56<br>3/20/85         | 250<br>13.9                         | 0.6/8<br>290<br>6.8<br>10.1<br>0.674                    |
| 8                   |                      | 9/ 1/09<br>300<br>3.2<br>9.6        | 0.335<br>10<br>7.5                             | 0.717<br>280<br>280                   | 0.341<br>290<br>11.9<br>0.793                         |                      | 270<br>270<br>4.9<br>8.7       | 0.848<br>330<br>2.8<br>3.7       | 0.759<br>270<br>5.6  | 0.945<br>280<br>5.7<br>6.3<br>0.904                        | 57<br>57<br>2/27/85           | 220<br>12.6<br>13.2                 | 0.893<br>0.82<br>0.893                                  |
| 7                   | 78                   | 1/ 13/03<br>260<br>12.7<br>13.4     | 0.947<br>280<br>4.0<br>6.2                     | 0.645                                 | 0.973<br>310<br>9.8<br>0.925                          | 76                   | - 19/65<br>260<br>8.4<br>11.1  | 0.735<br>340<br>3.2<br>4.5       | 0.717<br>180<br>3.1<br>7.2   | 0.438<br>300<br>5.6<br>10.5<br>0.534                       | 58<br>58<br>2/24/85 1         | 210<br>10.4                         | 0.924<br>190<br>8.2<br>0.949                            |
| 6                   | 82<br>82             | 260<br>260<br>10.0<br>11.8          | 0.847<br>270<br>8.8<br>10.1                    | 0.871<br>270<br>10.4                  | 0.981<br>290<br>17.3<br>0.981                         | NE 1/21/05           | 1/31/85<br>30<br>7.1<br>7.5    | 0.950<br>5.1<br>5.3              | 0.966<br>40<br>10.5<br>10.8  | 0.974<br>60<br>4.0<br>5.2<br>0.763                         | 1/19/85                       | 240<br>8.5<br>10.1                  | 0.841<br>5.40<br>5.5<br>0.911                           |
| 5                   | 84<br>110 / 95       | 11.4                                | 0.735<br>340<br>3.2<br>4.5                     | 0.717<br>180<br>3.1                   | 0.438<br>300<br>5.5<br>5.5<br>0.534                   | 48                   | 5/ 2/07<br>300<br>15 1         |                                  | 0.823<br>300<br>9.6<br>10.8  | 0.894<br>300<br>14.3<br>16.2<br>0.880                      | 61<br>61<br>4/85              | 250<br>11.8<br>12.5                 | 0.944<br>5.3<br>8.3<br>0.635                            |
| - <del>1</del>      | 89<br>175/95         | 250<br>6.9<br>9.6                   | ).719<br>240<br>4.0<br>5.9                     | 0.676<br>8.1<br>8.1                   | 280<br>280<br>7.3<br>802<br>802                       | 79                   | 220<br>12.6<br>13.5            | 0.952<br>8.2<br>9.2<br>9.2       | ).893<br>240<br>14.6<br>14.8   | 0.988<br>220<br>11.8<br>12.4                               | (NE)<br>65<br>11/ 7/85        | 40<br>6.6                           | 0.910<br>7.5<br>0.910                                   |
| 3                   | 89                   | 270<br>4.9<br>5.8                   | .848<br>330<br>2.8<br>3.7                      | . 759<br>270<br>5.6                   | ).945<br>280<br>5.7<br>6.3<br>0.904                   | 80<br>80<br>7,51,76E | 210<br>210<br>10.4<br>11.2     | ).924<br>190<br>8.2<br>8.6       | ).949<br>240<br>8.6<br>8.6   | ).997<br>260<br>13.6<br>16.0<br>.851                       | 68<br>+/19/85                 | 260<br>8.4<br>11.4                  | ). 737<br>340<br>3.22<br>4.55<br>0.717                  |
| ~ \                 | 90<br>977 / 0 E 1    | 220<br>12.6<br>13.2                 | .952<br>210<br>8.2<br>9.2                      | ). 893<br>240<br>14.6                 | ).988<br>220<br>11.8<br>12.4                          | 85<br>85             | 300<br>300<br>3.2<br>0.5       | ), 335<br>5.40<br>7.5            | 2.90<br>2.9<br>8.6   | ).341<br>290<br>11.9<br>.793<br>().793                     | (NVN)<br>3/ 1/85 <sup>1</sup> | 300<br>3.2<br>9.6                   | 0.335<br>5.4<br>7.5<br>0.717                            |
| - }                 | 97<br>97<br>8705 10  | 220<br>11.1<br>12.1                 | 240<br>240<br>4.9<br>8.1                       |                                       | 270<br>270<br>20.4<br>258                             | 82                   | 240<br>240<br>8.5<br>10 1      | 5.5<br>5.5                       | 911 (0) 260 (0 | ).864 (<br>260<br>5.3<br>7.3<br>).726 (                    | 78                            | 230<br>10.7<br>11.8                 | ). 909<br>180<br>7.3<br>9.1<br>.807<br>(                |
| <b>ZANK</b>         | TSP<br>DATE          | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO (<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | VEL (MPH)                             | ZATIO<br>01R (DEC)<br>VEL (MPH)<br>SPD (MPH)<br>ZATIO | TSP                  | DALE<br>DIR (DEG)<br>VEL (MPH) | VEL (MPH)<br>SPD (MPH)           | RATIÒ<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)   | RATIO (<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>(RATIO ( | TSP<br>DATE                   | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | KALLO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO ( |
| TOWN-SITE (SAMPLES) | WALLINGFORD-001 (59) | METEOROLOGICAL SITE I<br>NEWARK \   | METEOROLOGICAL SITE                            | METEOROLOGICAL SITE I<br>BRIDGEPORT V | METEOROLOGICAL SITE I<br>WORCESTER >                  | WATERBURY-005 (56)   | METEOROLOGICAL SITE            | METEOROLOGICAL SITE I<br>BRADLEY | METEOROLOGICAL SITE I<br>BRIDGEPORT >  | METEOROLOGICAL SITE  | WATERBURY-006 (59)            | METEOROLOGICAL SITE                 | METEOROLOGICAL SITE<br>BRADLEY                          |

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|             |                     |  |   |                     |                                 | ÷   |                                     |   |       |                      |                                     | 4                               |  |   |                                 |
|-------------|---------------------|--|---|---------------------|---------------------------------|---|-------------------------------------|---|-------|----------------------|-------------------------------------|---------------------------------|--|---|---------------------------------|
| IC METER    | 10                  | 300<br>9.6<br>10.8<br>0.894                  | 300<br>14.3<br>16.2<br>0.880                          | 77<br>4/19/85       | 8.4<br>11.4<br>0.735            | 3.40<br>3.40<br>717<br>717  | 3.1                                 | 200<br>300<br>10.5<br>10.5  | 1.00  | 59<br>9/ 4/85        | 250<br>11.8<br>12.5                 | 0.944<br>240<br>5.3             | 0.635<br>9.7                                 | 9.8<br>0.992<br>250   | 11.6<br>12.1<br>0.957           |
| S PER CUB   | <u>,</u> 6          | 270<br>7.6<br>0.740                          | 280<br>14.0<br>0.916<br>0.916                         | 5/ 1/85             | 335<br>0.335<br>0.335           | 0<br>7.7<br>7.7<br>7<br>7<br>7<br>7<br>7<br>7<br>7<br>7                                       | 2.9<br>2.6<br>8.6                   | 11.9<br>703<br>703<br>703   | NWN)  | 62<br>12/ 9/85       | 270<br>5.8                          | 0.848<br>330<br>2.8             | 0.759<br>270<br>5.6                          | 0.945<br>280<br>280   | 5.7<br>6.3<br>0.904             |
| 4 I CROGRAM | ω                   | 240<br>14.6<br>0.988<br>0.988                | 220<br>11.8<br>12.4<br>0.957                          | 1/31/85             | 7.1<br>7.5<br>0.950             |   | 10.5<br>10.8                        | 1.5<br>1.5<br>1.5<br>1.5  | 003   | 63<br>3/ 8/85        | 220                                 | 0.921<br>240<br>4.9             | 8.1<br>0.606<br>240<br>10.7                  | 0.996<br>270  | 19.6<br>20.4<br>0.958           |
| UNITS : I   | 7                   | 240<br>8.6<br>8.6<br>0.997                   | 260<br>13.6<br>0.851                                  | 3/20/85             | 9.5<br>13.9<br>0.678            | 2290<br>6.8<br>10.1   | 2270<br>10.2                        | 280<br>14.0<br>15.2   | 0.2.0 | 64<br>2/24/85        | 210<br>10.4                         | 0.924<br>190<br>8.2             | 8.6<br>0.949<br>8.6                          | 8.6<br>0.997<br>260   | 13.6<br>16.0<br>0.851           |
| AIND DATA   | 9                   | 260<br>9.6<br>11.1<br>0.864                  | 260<br>5.3<br>0.726                                   | 89<br>5/13/85       | 10.7<br>11.8<br>0.909           | 0 807<br>9.1  | 2000<br>2000<br>8.1                 | 85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.54<br>85.556<br>85.556<br>85.556<br>85.556<br>85.556<br>85.556<br>85.556<br>85.556<br>85.556<br>855 | N.N.  | 67<br>3/20/85        | 250<br>9.5<br>13.9                  | 0.678<br>290<br>6.8             | 0.674<br>270<br>7.6                          | 10.2<br>0.740<br>280  | 14.0<br>15.2<br>0.916           |
| AYS WITH V  | 5                   | 260<br>9.7<br>0.992                          | 250<br>11.6<br>12.1<br>0.957                          | 99<br>3/ 2/85       | 13.3<br>15.4<br>0.864           | 0.9<br>10.9<br>823  | 0.800<br>10.8                       | 300<br>300<br>14.3<br>16.2  |       | <u>67</u><br>5/ 1/85 | 300<br>3.2<br>9.6                   | 0.335<br>15.10<br>14.10         | 0.717<br>280<br>2.9                          | 8.6<br>290<br>290   | و.9<br>11.9<br>0.793            |
| AGE TSP D/  | 4                   | 40<br>9.6<br>11.1<br>0.870                   | 70<br>8.1<br>0.985                                    | 103<br>3/ 8/85      | 11.1<br>12.1<br>0.921           | 2710<br>4.1<br>6.1  | 240<br>240<br>10.7<br>10.8          | 270<br>19.6<br>20.4   | 0/6.0 | 82<br>12/27/85       | 220<br>12.6<br>13.2                 | 0.952<br>210<br>8.2             | 0.893<br>240<br>14.6                         | 14.8<br>0.988<br>220  | 11.8<br>12.4<br>0.957           |
| HOUR AVER   | £                   | 180<br>3.1<br>7.2<br>0.438                   | 0.534<br>0.534  | 106<br>2/24/85      | 10.4<br>11.2<br>0.924           | 8.6<br>949  | 8.6<br>8.6                          | 13.6<br>16.0  |       | 1/31/85              | 30<br>7.5<br>7.5                    | 0.950<br>10<br>5.1              | 0.966<br>10.5                                | $ \begin{array}{c} 10.8 \\ 0.974 \\ 60 \\ .6$ | 4.0<br>5.2<br>0.763             |
| GHEST 24-1  | N                   | 280<br>2.9<br>8.6<br>0.341                   | 290<br>9.5<br>11.9<br>0.793                           | 2/18/85             | 200<br>10.0<br>11.8<br>0.847    | 270<br>8.8<br>10.1<br>871   | 270<br>10.4                         | 290<br>290<br>17.3<br>081   |       | 101<br>3/ 2/85       | 300<br>13.3<br>15.4                 | 0.864<br>310<br>9.0             | 0.823<br>0.823<br>9.6                        | 10.8<br>0.894<br>300  | 14.3<br>16.2<br>0.880           |
| 55 TEN HIG  | -                   | 200<br>7.4<br>8.1<br>0.916                   | 220<br>8.4<br>0.886                                   | 130<br>12/27/85     | 12.6<br>13.2<br>0.952           | 0.2<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0 | 240<br>14.6<br>14.8                 | 220<br>11.8<br>12.4   |       | 106<br>2/18/85       | 260<br>10.0<br>11.8                 | 0.847<br>270<br>8.8             | 0.871<br>270<br>10.4                         | 10.6<br>0.981<br>290  | 16.9<br>17.3<br>0.981           |
| 198         | RANK                | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>RATIO | TSP<br>DATE<br>DATE | VEL (MPH)<br>SPD (MPH)<br>RATIO | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO  | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | VEL (MPH)<br>SPD (MPH)  |       | TSP<br>DATE          | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH) | SPU (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH) | SPD (MPH)<br>RATIO<br>DIR (DEG)   | VEL (MPH)<br>SPD (MPH)<br>RATIO |
|             | TOWN-SITE (SAMPLES) | METEOROLOGICAL SITE<br>BRIDGEPORT            | METEOROLOGICAL SITE<br>WORGESTER                      | WATERBURY-007 (60)  | MELEONOLOGICAL STIE<br>NEWARK   | METEOROLOGICAL SITE<br>BRADLEY  | METEOROLOGICAL SITE<br>BRIDGEPORT   | METEOROLOGICAL SITE<br>WORCESTER  |       | WILLIMANTIC-002 (60) | METEOROLOGICAL SITE<br>NEWARK       | METEOROLOGICAL SITE<br>BRADLEY  | METEOROLOGICAL SITE<br>BRIDGEPORT            | METEOROLOGICAL SITE   | WORGESTER                       |

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TABLE 11, CONTINUED

NW = 122 = 30.5

NEW ANN - INS SE - 3 - 123 SE - 3 - 0.3

SW = 185 = 46.2

### III. SULFUR DIOXIDE

### **HEALTH EFFECTS**

Sulfur oxides are gases that come from the burning of sulfur-containing fuel, mainly coal and oilderived fuels, and also from the smelting of metals and from certain industrial processes. They have a distinctive odor. Sulfur dioxide (SO<sub>2</sub>) comprises about 95 percent of these gases, so scientists use a test for SO<sub>2</sub> alone as a measure of all sulfur oxides.

Exposure to high levels of sulfur oxides can cause an obstruction of breathing that doctors call "pulmonary flow resistance." The amount of breathing obstruction has a direct relation to the amount of sulfur compounds in the air. The effect of sulfur pollution is enhanced by the presence of other pollutants, especially particulates and oxidants. Moreover, the harm that results from two or more pollutants is more than additive. Each augments the other, and the combined effect is greater than the sum of the effects that each alone would have.

Many types of respiratory disease are associated with sulfur oxides:coughs and colds, asthma, bronchitis, and emphysema. Some researchers believe that the harm is not only due to the sulfur oxide gases but also other sulfur compounds that accompany the oxides.

### CONCLUSIONS

Sulfur dioxide concentrations in 1985 did not exceed any federal primary or secondary standards. Measured concentrations were substantially below the 365  $\mu$ g/m<sup>3</sup> primary 24-hour standard and well below both the 80  $\mu$ g/m<sup>3</sup> primary annual standard and the 1300  $\mu$ g/m<sup>3</sup> secondary 3-hour standard.

### METHOD OF MEASUREMENT

The DEP Air Monitoring Unit used the pulsed fluorescence method (Teco instruments) to continuously measure sulfur dioxide levels at all 18 sites in 1985.

### **DISCUSSION OF DATA**

Monitoring Network - Eighteen continuous SO<sub>2</sub> monitors were used to record data in fifteen towns during 1985 (see Figure 5):

| Bridgeport 012    | Milford 002     |
|-------------------|-----------------|
| Bridgeport 123    | New Britain 011 |
| Danbury 123       | New Haven 017   |
| East Hartford 005 | New Haven 123   |
| East Haven 003    | Norwalk 013     |
| Enfield 005       | Preston 002     |
| Greenwich 017     | Stamford 025    |
| Groton 007        | Stamford 123    |
| Hartford 123      | Waterbury 123   |

All of these sites telemetered the data to the central computer in Hartford on a real-time basis.

**Precision and Accuracy** - 565 precision checks were made on SO<sub>2</sub> monitors in 1985, yielding 95% probability limits ranging from -11% to +7%. Accuracy is determined by introducing a known amount of SO<sub>2</sub> into each of the monitors. Three different concentration levels are tested: low, medium, and high. The 95% probability limits for accuracy based on 19 audits were: low, -5% to + 3%; medium, -5% to +4%; and high, -6% to + 2%.

Annual Averages - SO<sub>2</sub> levels were below the primary annual standard of 80  $\mu$ g/m<sup>3</sup> at all sites in 1985 (see Table 12). The annual average SO<sub>2</sub> levels increased at  $\lambda$  of the 15 monitoring sites that had adequate data in both 1984 and 1985 to produce valid annual averages. Five sites showed decreases from 1984 to 1985. New Haven 123 experienced the highest increase of  $\chi$   $\mu$ g/m<sup>3</sup>. Hartford 123 showed the largest annual average decrease of 8  $\mu$ g/m<sup>3</sup>.

Statistical Projections - A statistical analysis of the sulfur dioxide data is presented in Table 13. This analysis provides information to compensate for any loss of data caused by instrumentation problems. The format of Table 13 is the same as that used to present the total suspended particulate annual averages (see Table 6). However, Table 13 gives the annual arithmetic mean of the valid 24-hour SO<sub>2</sub> averages to allow direct comparison to the annual SO<sub>2</sub> standards. The 95% limits and standard deviations are also arithmetic calculations. Since the distribution of the SO<sub>2</sub> data tends to be lognormal, the geometric means and standard deviations were used to predict the number of days the 24-hour standard of 365  $\mu$ g/m<sup>3</sup>would be exceeded at each site if sampling had been conducted every day.

It is important to note that these statistical tests require that the data be random for the test to be valid. This means that an equal number of samples must be collected in each season of the year and on each day of the week. For the 18 sites that operated in 1985, the distribution and quantity of SO<sub>2</sub> data were adequate — except for the Stamford 025 site. The data for these sites indicate that there were no violations of the primary SO<sub>2</sub> standard in Connecticut. For example, a statistical prediction of one day exceeding the primary 24-hour standard (365  $\mu$ g/m<sup>3</sup>) at Bridgeport 012 indicates that a slight increase in SO<sub>2</sub> emissions there might jeopardize the attainment of this standard. Two days over the standard are required for the standard to be violated.

**24-Hour Averages** - Table 14 presents the 1st and 2nd high calendar day average concentrations recorded at each monitoring site. In 1985 no sites recorded SO<sub>2</sub> levels in excess of the 24-hour primary standard of 365  $\mu$ g/m<sup>3</sup>. Second high calendar day average concentrations decreased at "14" of the 15. SO<sub>2</sub> monitoring sites that had a sufficient distribution and quantity of data in both 1984 and 1985. The decreases ranged from 12  $\mu$ g/m<sup>3</sup> at Preston 002 to 110  $\mu$ g/m<sup>3</sup> at Hartford 123.

Current EPA policy bases compliance with the primary 24-hour  $SO_2$  standard on calendar day averages. Assessment of compliance is based on the second highest calendar day average in the year. Running averages are averages computed for the 24-hour periods ending at every hour. If running averages were used, assessment of compliance would be based on the value of the second highest of the two highest non-overlapping 24-hour periods in the year. There has been some contention over which average is the more appropriate one on which to base compliance. Table 15 contains the maximum 24hour  $SO_2$  readings from both the running averages and the calendar day averages for comparison. The maximum calendar day readings are all lower than the maximum running average readings, and the differences range up to 28 µg/m<sup>3</sup> at Norwalk 013.

**3-Hour Averages** - Table 16 presents the 1st and 2nd high 3-hour concentrations recorded at each monitoring site. Measured SO<sub>2</sub> concentrations were far below, the federal secondary 3-hour standard of 1300  $\mu$ g/m<sup>3</sup> at all DEP monitoring sites in 1985. Of the 15 sites that had a sufficient distribution and guantity of data in both 1984 and 1985, all but 3 had lower 2nd high concentrations in 1985. Six of these decreases were greater than 100  $\mu$ g/m<sup>3</sup>. Of the 3 sites with higher 2nd high concentrations in 1985, the largest increase was 57  $\mu$ g/m<sup>3</sup> at New Haven 017.

**10-High Days with Wind Data** - Table 17 lists the ten highest 24-hour calendar day  $SO_2$  averages and the dates of occurrence for each  $SO_2$  site in Connecticut during 1985. The table also shows the average wind conditions that occurred on each of these dates. (The origin and use of these wind data are described in the discussion of Table 11 in the TSP section of this Air Quality Summary.)

Once again, as with TSP, many (i.e., 43.3%) of the highest SO<sub>2</sub> days occur with winds out of the southwest quadrant and most of these days have persistent winds. This relationship is caused, at least in part, by SO<sub>2</sub> transport, but any transport is limited by the chemical instability of SO<sub>2</sub>. In the atmosphere, SO<sub>2</sub> reacts with other gases to produce, among other things, sulfate particulates. Therefore, SO<sub>2</sub> is not likely to be transported very long distances. Previous studies conducted by the DEP have shown that, during periods of southwest winds, levels of SO<sub>2</sub> in Connecticut decrease with distance from the New York City metropolitan area. This relationship tends to support the transport hypothesis. On the other hand, these studies also revealed that certain meteorological parameters, most notably mixing height and wind speed, are more conducive to high SO<sub>2</sub> levels on days when there are southwesterly winds than on other days.

The data in Table 17 were used to make a tally, by date, of the frequency of occurrence of high SO<sub>2</sub> levels. Only those seventeen sites were used which had a sufficient distribution and quantity of data in 1985 to produce a valid annual average. If a given date recurred at five or more sites in this tally, the SO<sub>2</sub> levels and meteorological conditions were investigated further (there were sixteen such days). A close look at these sixteen days revealed three important points. First, fifteen of the sixteen days occurred during the winter months. This can be attributed to more fuel being burned during the cold weather. Second, eight of the sixteen days had persistent southwest winds for that calendar day. Third, two other days had persistent southwest winds for the previous 24 hours.

In summary, high levels of SO<sub>2</sub> in Connecticut seem to be caused by a number of related factors. First, Connecticut experiences its highest SO<sub>2</sub> levels during the winter months, when there is an increased amount of fuel combustion. Second, the New York City metropolitan area, a large emission source, is located to the southwest of Connecticut and, in this region, southwest winds occur relatively often in comparison to other wind directions. Also, adverse meteorological conditions are often associated with southwest winds. The net effect is that during the winter months when a persistent southwesterly wind occurs, an air mass picks up increased amounts of SO<sub>2</sub> over the New York City metropolitan area and transports this SO<sub>2</sub> into Connecticut. Here, the SO<sub>2</sub> levels remain high because the relatively low mixing heights associated with the southwest flow and low winter temperatures will not allow much vertical mixing. The levels of transported SO<sub>2</sub> eventually decline with increasing distance from New York City, as the SO<sub>2</sub> is dispersed and as it slowly reacts to produce sulfate particulates. These sulfate particulates may fall to the ground in either a dry state (dry deposition) or in a wet state after combination with water droplets (wet deposition or "acid rain").


### <u>1985 ANNUAL ARITHMETIC AVERAGES OF SULFUR DIOXIDE</u> <u>AT SITES WITH CONTINUOUS MONITORS</u> (PRIMARY STANDARD: 80 µg/m<sup>3</sup>)

| TOWN              | SITE NAME                  | <u>ANNUALAVG</u> *<br>(µg/m³) |
|-------------------|----------------------------|-------------------------------|
| Bridgeport-012    | Edison School              | 36                            |
| Bridgeport-123    | Hallett Street             | 32                            |
| Danbury-123       | Western CT State College   | 20                            |
| East Hartford-005 | Fire House - Engine Co. #5 | 22 ****                       |
| East Haven-003    | Animal Shelter             | 25                            |
| Enfield-005       | Department of Corrections  | 14                            |
| Greenwich-017     | Greenwich Point Park       | 15                            |
| Groton-007        | Fire Headquarters          | 21                            |
| Hartford-123      | State Office Building      | 23                            |
| Milford-002       | Devon Community Center     | 30                            |
| New Britain-011   | Armory                     | 23                            |
| New Haven-017     | Lombard St. Fire House     | 29 31                         |
| New Haven-123     | State Street               | 44                            |
| Norwalk-013       | Ludlow School              | 24                            |
| Preston-002       | Norwich State Hospital     | 14                            |
| Stamford-025      | <b>Recreation Center</b>   | 28**                          |
| Stamford-123      | Health Department          | 29                            |
| Waterbury-123     | Bank Street                | 23                            |

\* The annual averages are expressed in terms of the arithmetic mean because the primary ambient air quality standard for SO<sub>2</sub> is defined as the annual arithmetic mean concentration. This differs from the trend analysis presented earlier in section I.B. of this Air Quality Summary which made use of the annual geometric mean.

\*\* A valid annual average cannot be calculated because the number of observations is insufficient or is poorly distributed.

## 1983-1985 SO2 ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

LOGNORMAL DISTRIBUTION

| TOMN NAME                              | SITE              | YEAR                 | SAMPLES                       | ARI. MEAN              | 95-PCT-I<br>LOMER    | LIMITS<br>UPPER      | STD DEVIATION                 | PREDICTED<br>DAYS OVER<br>365 UG/M3 | MEASURED<br>DAYS OVER<br>365 UG/M3 |
|--|-------------------|----------------------|-------------------------------|------------------------|----------------------|----------------------|-------------------------------|-------------------------------------|------------------------------------|
| BRIDGEPORT<br>BRIDGEPORT               | 012<br>012        | 1984<br>1985         | 333<br>317                    | 32.9<br>36.0           | 32<br>35             | 34<br>37             | 33.836<br>30.464              | -                                   |                                    |
| BRIDGEPORT<br>BRIDGEPORT<br>BRIDGEPORT | 123<br>123<br>123 | 1983<br>1984<br>1985 | 359<br>358<br>358             | 33.3<br>31.8<br>31.5 % | 33<br>31<br>31<br>30 | 34<br>32<br>32       | 22.834<br>26.948<br>26.101 24 | (¢ )                                |                                    |
| DANBURY<br>Danbury<br>Danbury          | 123<br>123<br>123 | 1983<br>1964<br>1985 | 356<br>358<br>292             | 16.9<br>17.5<br>20.0   | 17<br>17             | 17<br>18<br>21       | 13.031<br>18.635<br>17.747    |                                     |                                    |
| EAST HARTFORD<br>EAST HARTFORD         | 005<br>005        | 1984<br>1985         | 306 ¥<br>306 ¥                | 27.4<br>19.8           | 26<br>19             | 28<br>21             | 24.298<br>20.695              |                                     |                                    |
| EAST HAVEN<br>EAST HAVEN               | 003<br>003        | 1984<br>1985         | 341<br>332                    | 20.1<br>24.8           | 20<br>24             | 21<br>26             | 19.700<br>23.377              |                                     |                                    |
| ENFIELD<br>Enfield<br>Enfield          | 005<br>005<br>005 | 1983<br>1984<br>1985 | 61*<br>349<br>345             | 23.1<br>13.9<br>12.7   | 18<br>14<br>12       | 28<br>14<br>13       | 20.895<br>16.871<br>13.625    |                                     |                                    |
| GREENWICH<br>GREENWICH<br>GREENWICH    | 017<br>017<br>017 | 1983<br>1984<br>1985 | 333<br>345<br>357             | 15.5<br>16.9<br>14.4   | 165<br>165<br>165    | 16<br>17<br>15       | 11.659<br>17.251<br>12.452    |                                     |                                    |
| GROTON<br>GROTON<br>GROTON             | 200<br>200<br>200 | 1983<br>1984<br>1985 | 79 <del>*</del><br>334<br>354 | 24.2<br>20.6<br>21.3   | 21<br>20<br>21       | 27<br>21<br>22       | 13.835<br>16.210<br>13.955    |                                     |                                    |
| HARTFORD<br>HARTFORD<br>HARTFORD       | 123<br>123<br>123 | 1983<br>1984<br>1985 | 360<br>361<br>361             | 32.4<br>31.4<br>22.8   | 32<br>31<br>53       | 33<br>33<br>23<br>23 | 22.793<br>31.425<br>22.298    |                                     |                                    |
|  |                   |                      |                               |                        |                      |                      |                               |                                     |                                    |

\* SAMPLING NOT RANDOM OR OF INSUFFICIENT SIZE FOR REPRESENTATIVE ANNUAL STATISTICS.

N.B. THE ANNUAL AVERAGES IN TABLE 13 VARY SLIGHTLY FROM THOSE IN TABLE 12 DUE TO THE MANNER IN WHICH THEY WERE DERIVED. THE AVERAGES IN TABLE 12 ARE BASED ON THE AVAILABLE HOURLY READINGS, WHILE THOSE IN TABLE 13 ARE BASED ON VALID 24-HOUR AVERAGES. (AT LEAST 18 HOURLY READINGS ARE REQUIRED TO PRODUCE A VALID 24-HOUR AVERAGE.)

THE ARITHMETIC MEAN AND STANDARD DEVIATION HAVE UNITS OF MICROGRAMS PER CUBIC METER.

TABLE 13, CONTINUED

## 1983-1985 SO2 ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

LOGNORMAL DISTRIBUTION

| FOMN NAME         | SITE | YEAR  | SAMPLES | ARI. MEAN | 95-PCT-<br>LOWER | -LIMITS<br>UPPER | STD DEVIATION | PREDICTED<br>DAYS OVER<br>365 UG/M3 | MEASURED<br>DAYS OVER<br>365 UG/M3 |
|-------------------|------|-------|---------|-----------|------------------|------------------|---------------|-------------------------------------|------------------------------------|
| <b>11 L F ORD</b> | 002  | 1983  | 342     | 34.8      | 34               | 36               | 27.169        |                                     |                                    |
| <b>11 L F ORD</b> | 002  | 1984  | 341     | 33.9      | 33               | 35               | 34.191        | ч                                   |                                    |
| 4I L F ORD        | 002  | 1985  | 349     | 29.3      | 29               | 30               | 27.498        |                                     |                                    |
| VEW BRITAIN       | 110  | 1984  | 227*    | 14.2      | 13               | 15               | 12.809        |                                     |                                    |
| VEW BRITAIN       | 110  | 1985  | 360     | 23.0      | 23               | 23               | 19.693        |                                     |                                    |
| JEW HAVEN         | 210  | 1 986 | 122     | 24.6      | 24               | 25               | 22.161        |                                     |                                    |
| VEW HAVEN         | 017  | 1985  | 341     | 36.2      | 35               | 37               | 31.069        |                                     |                                    |
| JEW HAVEN         | 123  | 1983  | 363     | 30.7      | 30               | 31               | 24.284        |                                     |                                    |
| VEW HAVEN         | 123  | 1984  | 346     | 34.6      | 34               | 35               | 32.585        |                                     |                                    |
| VEN HAVEN         | 123  | 1985  | 357     | 44.3      | 44               | 45               | 36.297        |                                     |                                    |
| JORWALK           | 013  | 1984  | 266*    | 17.1      | 16               | 18               | 14.621        | 1                                   |                                    |
| NORWALK           | 013  | 1985  | 364     | 23.1      | 23               | 23               | 22.858        |                                     |                                    |
| PRESTON           | 002  | 1983  | 61*     | 13.9      | 12               | 16               | 7.016         |                                     |                                    |
| PRESTON           | 002  | 1984  | 345     | 10.9      | 11               | 11               | 9.527         |                                     |                                    |
| PRESTON           | 002  | 1985  | 349     | 13.0      | 13               | 13               | 10.803        |                                     |                                    |
| STAMFORD          | 025  | 1984  | 297*    | 23.0      | 22               | 24               | 16.563        |                                     |                                    |
| STAMFORD          | 025  | 1985  | 280*    | 28.5      | 27               | 30               | 21.965        |                                     |                                    |
| STAMFORD          | 123  | 1983  | 362     | 26.7      | 26               | 27               | 18.916        |                                     |                                    |
| STAMFORD          | 123  | 1934  | 343     | 31.9      | 31               | 32               | 21.563        |                                     |                                    |
| STAMFORD          | 123  | 1985  | 353     | 23.6      | 28               | 29               | 22.817        |                                     |                                    |
| MATERBURY         | 007  | 1983  | ¥09     | 34.0      | 27               | 41               | 29.103        |                                     |                                    |
| MATERBURY         | 007  | 1984  | 350     | 28.8      | 28               | 29               | 28.810        |                                     |                                    |
| MATERBURY         | 123  | 1983  | 351     | 18.9      | 19               | 19               | 14.291        |                                     |                                    |
| MATERBURY         | 123  | 1984  | 334     | 22.7      | 22               | 23               | 20.813        |                                     |                                    |
| MATERBURY         | 123  | 1985  | 351     | 23.0      | 23               | 23               | 19.482        |                                     |                                    |
|                   |      |       |         |           |                  |                  |               |                                     |                                    |

\* SAMPLING NOT RANDOM OR OF INSUFFICIENT SIZE FOR REPRESENTATIVE ANNUAL STATISTICS.

N.B. THE ANNUAL AVERAGES IN TABLE 13 VARY SLIGHTLY FROM THOSE IN TABLE 12 DUE TO THE MANNER IN WHICH THEY WERE DERIVED. THE AVERAGES IN TABLE 12 ARE BASED ON THE AVAILABLE HOURLY READINGS, WHILE THOSE IN TABLE 13 ARE BASED ON VALID 24-HOUR AVERAGES. (AT LEAST 18 HOURLY READINGS ARE REQUIRED TO PRODUCE A VALID 24-HOUR AVERAGE.)

THE ARITHMETIC MEAN AND STANDARD DEVIATION HAVE UNITS OF MICROGRAMS PER CUBIC METER.

### **1985 MAXIMUM CALENDAR DAY AVERAGE SO2 CONCENTRATIONS**



\* Date is month/day of occurrence.

\*\* Database for the site is deficient in number or distribution of observations.

N.B. When a listed concentration occurs more than once at a site, the earliest date of occurrence is given.

Primary standard =  $365 \,\mu g/m^3$ .

### **TABLE 14, CONTINUED**

### **1985 MAXIMUM CALENDAR DAY AVERAGE SO2 CONCENTRATIONS**



\* Date is month/day of occurrence.

\* Database for the site is deficient in number or distribution of observations.

N.B. When a listed concentration occurs more than once at a site, the earliest date of occurrence is given.

Primary standard =  $365 \,\mu g/m^3$ .

### COMPARISONS OF FIRST AND SECOND HIGH CALENDAR DAY AND 24-HOUR RUNNING SO2 AVERAGES\*

|                       | FIRST HIGH         | AVERAGE         | SECOND HIG         | <u>H AVERAGE</u> |
|-----------------------|--------------------|-----------------|--------------------|------------------|
| SITE                  | RUNNING<br>24-HOUR | CALENDAR<br>DAY | RUNNING<br>24-HOUR | CALENDAR<br>DAY  |
| Bridgeport-012        | 159                | 151             | 154                | 145              |
| Bridgeport-123        | 157 /AI            | 136 124         | 141/30             | 125 114          |
| Danbury-123           | 93                 | 88              | 89                 | 76               |
| **<br>E. Hartford-005 | 99                 | 93              | 98                 | 90               |
| East Haven-003        | 149                | 146             | 135                | 119              |
| Enfield-005           | 85                 | 76              | 76                 | 68               |
| Greenwich-017         | 92                 | 89              | 67                 | 66               |
| Groton-007            | 76                 | 69              | 74                 | 68               |
| Hartford-123          | 117                | 114             | 116                | 101              |
| Milford-002           | 158                | 133             | 143                | 132              |
| New Britain-011       | 108                | 107             | 103                | 95               |
| New Haven-017         | 189                | 174             | 186                | 147              |
| New Haven-123         | 259                | 248             | 214                | 181              |
| Norwalk-013           | 150                | 122             | 128                | 121              |
| Preston-002           | 59                 | 52              | 56                 | 50               |
| Stamford-025**        | 134                | 123             | 126                | 104              |
| Stamford-123          | 128                | 124             | 119                | 113              |
| Waterbury-123         | 117                | 98              | 104                | 92               |

\* Units are μg/m<sup>3</sup>.

\*\* The number or distribution of observations at the site is inadequate for the calculation of a valid annual average.

### **1985 MAXIMUM 3-HOUR RUNNING AVERAGE SO2 CONCENTRATIONS**



\* Date is month/day/ending hour of occurrence.

\*\* Database for the site is deficient in number or distribution of observations.

N.B. When a listed concentration occurs more than once at a site, the earliest date of occurrence is given.

Secondary standard =  $1300 \,\mu g/m^3$ .

**TABLE 16, CONTINUED** 

### **1985 MAXIMUM 3-HOUR RUNNING AVERAGE SO2 CONCENTRATIONS**



Date is month/day/ending hour of occurrence.
 \*\*

\* Database for the site is deficient in number or distribution of observations.

N.B. When a listed concentration occurs more than once at a site, the earliest date of occurrence is given.

Secondary standard =  $1300 \,\mu\text{g/m}^3$ .

|         | DATA    |
|---------|---------|
|         | MIND    |
|         | WITH    |
|         | DAYS    |
|         | S02     |
| ABLE 17 | AVERAGE |
| F       | 24-HOUR |
|         | HICHEST |
|         | TEN     |
|         | 1985    |

|           |                     |                      |  | $\sim$                                       | ····   |   |                             |   | · minasing_rr  | ~  |   |                   |   | $\sim$  |
|-----------|---------------------|----------------------|--|--|--|---|-----------------------------|---|--|--|---|-------------------|---|---|
| IC METER  | 10                  | 211                  | 3/ 1/85<br>210<br>10.7                   | 0.912<br>200<br>10.8                         | 0.979<br>220<br>11.0                         | 0.954<br>260<br>17.6<br>17.8<br>0.989                 | 26                          | 2/21/85<br>160<br>3.6<br>7.5                | 0.496<br>190<br>3.3<br>4.6   | 0.711<br>130<br>2.5                          | 0.551<br>2280<br>7.9<br>0.699                         | 64                | 1/17/85<br>220<br>6.4<br>8 1                | 0.789<br>300<br>3.6<br>3.6                            |
| AMS / CUB | 6                   | 119                  | 1/19/85<br>240<br>8.5                    | 0.841<br>5.0<br>5.0                          | 0.911<br>260<br>9.6                          | 0.864<br>260<br>5.3<br>7.3<br>0.726                   | 100                         | 2/ 5/85<br>40<br>7.9                        | 0.884<br>30<br>3.6<br>3.6  | 0.712<br>60<br>11.5                          | 0.979<br>90<br>5.9<br>0.138                           | 67                | 2/21/85<br>160<br>3.6<br>7.2                | 0.496<br>190<br>3.3<br>4.6                            |
| : MICROGR | 8                   | 123                  | 2/ 2/ 2/ 2/ 2/ 2/ 2/ 2/ 2/ 2/ 2/ 2/ 2/ 2 | 0.884<br>30<br>2.6                           | 0.712<br>60<br>11.5                          | 0.979<br>90<br>5.9<br>0.138                           | 104                         | 3/ 1/85<br>210<br>10.7                      | 0.912<br>200<br>10.8<br>11.1   | 0.979<br>220<br>11.0                         | 0.954<br>260<br>17.6<br>0.989                         | 20                | 12/ 9/85<br>270<br>4.9<br>5.8               | 0.848<br>330<br>2.8<br>3.7<br>0.759                   |
| UNITS     | 7                   | 124                  | 1/28/85<br>300<br>6.8<br>9.3             | 0.723<br>320<br>3.3                          | 0.983<br>300<br>7.3                          | 0.813<br>300<br>9.5<br>10.1<br>0.945                  | 104                         | 12/ 9/85<br>270<br>4.9<br>5.8               | 0.848<br>330<br>2.8<br>3.7   | 0.759<br>270<br>5.6                          | 0.945<br>5.7<br>6.3<br>0.904                          | 20                | 7.9<br>300<br>7.9<br>8.6                    | 0.914<br>330<br>4.7<br>6.5                            |
|           | 9                   | 125                  | 7/21/2<br>260<br>9.4<br>9.9              | 0.946<br>5.5<br>6.2                          | 0.889<br>260<br>9.5<br>10.4                  | 0.920<br>260<br>8.2<br>0.971                          | 105                         | 1/31/85<br>30<br>7.1<br>7.5                 | 0.950<br>5.1<br>5.3  | 0.966<br>40<br>10.5                          | 0.974<br>60<br>4.0<br>5.2<br>0.763                    | 75                | 12/23/85<br>190<br>6.4<br>7 0               | 0.909<br>190<br>6.9<br>0.932                          |
|           | 5                   | 127                  | 24/11/2<br>240<br>11.6<br>12.5           | 0.930  | 0.796<br>240<br>9.0<br>9.6                   | 0.939<br>260<br>12.3<br>12.7<br>0.969                 | 111                         | 2/ 4/85<br>280<br>7.4<br>8.2                | 0.907<br>320<br>4.3<br>6.5   | 0.665<br>250<br>5.1                          | 0.765<br>290<br>7.1<br>7.8<br>0.921                   | 72                | 1/28/85<br>300<br>6.8<br>9_3                | 0.723<br>320<br>3.3<br>0.983                          |
|           | 4                   | 130                  | 21/31/85<br>210<br>9.5<br>10.2           | 0.930<br>9.0<br>9.2                          | 0.983<br>210<br>12.0<br>12.9                 | 0.925<br>15.5<br>0.996                                | 114                         | 1/28/85<br>300<br>6.8<br>0.3                | 0.723<br>320<br>3.3<br>3.3   | 0.983<br>300<br>6.0<br>7.3                   | 0.813<br>300<br>9.5<br>0.945                          | 72                | 68/6/2<br>04<br>7.9<br>8.9                  | 0.884<br>30<br>2.6<br>3.6<br>0.712                    |
|           | £                   | 136                  | 240<br>240<br>8.0<br>8.8                 | 0.911<br>240<br>3.9<br>4.9                   | 0.803<br>250<br>6.3<br>7.5                   | 0.844<br>270<br>6.9<br>8.1<br>0.857                   | 124                         | 1/19/85<br>240<br>8.5<br>10.1               | 0.841<br>5.0<br>5.5  | 0.911<br>260<br>9.6<br>11.1                  | 0.864<br>5.3<br>7.3<br>0.726                          | 13                | 12/29/85<br>240<br>4.2<br>6.3               | 0.661<br>210<br>5.4<br>0.829                          |
|           | 5                   | 145                  | 28/4/80<br>280<br>7.4<br>8.2             | 0.907<br>320<br>4.3<br>6.5                   | 0.665<br>250<br>5.1<br>6.6                   | 0.765<br>290<br>7.1<br>7.8<br>0.921                   | 125                         | 12140<br>240<br>7                           | 0.868<br>200<br>1.84<br>1.84<br>1.84<br>1.84<br>1.84<br>1.84<br>1.84<br>1.84 | 0(.828<br>256<br>13.4                        | 0.680   | 76                | 2/ 4/85<br>280<br>7.4<br>8.2                | 0.907<br>320<br>4.3<br>0.665                          |
|           |                     | 151                  | -/ -8/87<br>230<br>3.8<br>5.2            | 0.735<br>200<br>1.9<br>2.7                   | 0.693<br>210<br>6.8<br>7.3                   | 0.932<br>300<br>7.3<br>8.2<br>0.891                   | (136                        | 27/0<br>27/0<br>10<br>10<br>10              | 19.70<br>19.70<br>19.60  | 0.407<br>290<br>9.55<br>10.1                 | 0.9245<br>0.9240<br>0.927<br>0.927                    | 88                | 12/20/05<br>10<br>4.6<br>5.9                | 0.786<br>300<br>1.6<br>4.2<br>0.384                   |
|           | RANK                | SO2                  | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)      | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO | \$02                        | DALE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)                                 | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIÓ<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO | S02               | DALE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO |
|           | TOWN-SITE (SAMPLES) | BRIDGEPORT-012 (317) | METEOROLOGICAL SITE<br>NEWARK            | METEOROLOGICAL SITE<br>BRADLEY               | METEOROLOGICAL SITE<br>BRIDGEPORT            | METEOROLOGICAL SITE<br>WORCESTER                      | 355<br>BRIDGEPORT-123 (358) | METEOROLOGICAL SITE<br>NEWARK               | METEOROLOGICAL SITE<br>BRADLEY   | METEOROLOGICAL SITE<br>BRIDGEPORT            | METEOROLOGICAL SITE<br>WORCESTER                      | DANBURY-123 (292) | METEOROLOGICAL SITE<br>NEWARK               | METEOROLOGICAL SITE<br>BRADLEY                        |

|          | DATA    |
|----------|---------|
|          | MIND    |
|          | WITH    |
| ~        | DAYS    |
| NUE      | S02     |
| 7, CONTI | AVERAGE |
| TABLE 1  | 24-HOUR |
|          | HIGHEST |
|          | TEN     |
|          | 1985    |

|                   |  | r<br>v  | <del>ر</del> ي<br>س   |
|-------------------|--|---|---|
| 10                | 40<br>2.11<br>0.366<br>310<br>310<br>1.8<br>0.365<br>0.365                                   | 2/17/2<br>240<br>0.230<br>0.230<br>0.230<br>0.230<br>0.250<br>0.339<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.930<br>0.939<br>0.930<br>0.939<br>0.930<br>0.939<br>0.930<br>0.939<br>0.930<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.939<br>0.930<br>0.939<br>0.930<br>0.939<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.930<br>0.9300<br>0.9300<br>0.9300<br>0.9300<br>0.9300<br>0.9300<br>0.93000<br>0.93000<br>0.93000<br>0.930000000000   | $\begin{array}{c} 12 \\ 83 \\ 412 \\ 633 \\ 635 \\ 6$  |
| 6                 | 130<br>2.55<br>2.55<br>2.55<br>2.50<br>2.50<br>0.699<br>0.699                                | 1/31/85<br>7.1<br>7.1<br>7.1<br>7.1<br>7.1<br>7.1<br>7.1<br>5.1<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974<br>0.763   | 12/284<br>12/284<br>6.4<br>6.4<br>6.4<br>0.932<br>0.932<br>0.932<br>0.932<br>0.932<br>0.932<br>0.932<br>0.932<br>0.932<br>0.932<br>0.932<br>0.932<br>0.932<br>0.932<br>0.989  |
| 80                | 270<br>5.6<br>5.9<br>280<br>280<br>5.7<br>0.904  | 3/11/85<br>180<br>180<br>180<br>180<br>17.6<br>17.6<br>17.6<br>17.6<br>17.6<br>17.6<br>17.6<br>17.6   | 1/19/252<br>230<br>200<br>200<br>200<br>210<br>210<br>210<br>210<br>210<br>210<br>21  |
| 7                 | 310<br>8.0<br>9.2<br>0.865<br>5.1<br>5.1<br>0.724  | 2/ 1/85<br>20 20<br>10.7<br>10.8<br>0.996<br>5.9<br>0.952<br>0.952<br>0.952<br>0.952<br>0.952<br>0.974  | 1/31/85<br>30<br>31/85<br>7.5<br>7.5<br>10.55<br>0.956<br>0.974<br>0.974<br>0.974<br>0.974<br>0.974<br>0.763  |
| Q                 | 250<br>9.5<br>0.972<br>230<br>10.4<br>0.989  | $\begin{array}{c} 12/24/85\\ 190\\ 2.5\\ 190\\ 0.296\\ 0.296\\ 0.298\\ 0.328\\ 0.398\\ 0.398\\ 0.298\\ 0.296\\ 0.298$ | 12/20/85<br>12/20/85<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10<br>10  |
| 5                 | 300<br>6.0<br>7.3<br>300<br>300<br>9.5<br>0.945  | 12/20/85<br>12/20/85<br>12/20/85<br>100<br>100<br>100<br>100<br>100<br>100<br>100<br>10   | 101<br>114/85<br>240<br>2240<br>2240<br>2240<br>2250<br>250<br>250<br>250<br>250<br>250<br>250<br>250<br>250<br>2   |
| 11                | 60<br>11.5<br>0.979<br>0.8<br>0.8<br>0.8<br>0.138  | 2/ 87<br>310/85<br>310/85<br>310/222.9<br>222.9<br>222.9<br>15.5<br>15.3<br>15.3<br>15.3<br>15.3<br>15.3<br>15.3<br>15.3  | $\begin{array}{c} 1,28,85\\ 1,28,85\\ 5.00\\ 5.23\\ 3.23\\$   |
| 3                 | 240<br>6.5<br>7.8<br>0.831<br>8.1<br>8.3<br>0.966  | 2/5/85<br>1/5/85<br>1/5/85<br>1/60<br>1/1.5<br>1/1.5<br>1/1.5<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712   | 12/109<br>270<br>2.109<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.100<br>2.1000<br>2.1000<br>2.1000<br>2.1000<br>2.1000<br>2.10000000000  |
| N                 | 250<br>5.1<br>6.6<br>290<br>7.1<br>7.1<br>7.8  | 2/16/85<br>250<br>250<br>240<br>240<br>240<br>240<br>240<br>240<br>240<br>240<br>240<br>270<br>270<br>270<br>0.977<br>0.968   | $\begin{array}{c} 2/ \begin{array}{c} 119 \\ 400 \\ 400 \\ 719 \\ 710 \\ 710 \\ 710 \\ 711 \\ 711 \\ 711 \\ 711 \\ 711 \\ 711 \\ 711 \\ 710$  |
| -                 | 30<br>5.2<br>5.2<br>5.2<br>0.900<br>3.5<br>0.442<br>0.442                                    | 2/14/85<br>2/14/85<br>2/14/85<br>13:1<br>13:1<br>13:1<br>13:1<br>12:0<br>12:40<br>0.910<br>0.910<br>0.910<br>0.910<br>0.910<br>0.910<br>0.910<br>0.910<br>0.991   | 2/ 146<br>2/ 4/85<br>280<br>8.2<br>8.2<br>4.3<br>4.3<br>4.3<br>4.3<br>6.5<br>0.907<br>7.1<br>0.755<br>0.921   |
| RANK              | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEC)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO | S02<br>DATE<br>DATE<br>DIR (DEG)<br>VEL (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)  | SOZ<br>DIATE<br>DIATE<br>DIATE<br>NEC<br>VEL (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>VEL (MPH)<br>SPD (MPH) |
| WN-SITE (SAMPLES) | METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>WORCESTER                        | ARTFORD-005 (306)<br>METEOROLOGICAL SITE<br>NEWARK<br>METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE   | AST HAVEN-003 (332)<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE   |
|                   | WN-SITE (SAMPLES) RANK 1 2 3 4 5 6 7 8 9 10  | WN-SITE (SAMPLES)       RANK       1       2       3       4       5       6       7       8       9       10         METEOROLOGICAL SITE       DIR (DEG)       30       250       240       60       300       250       310       270       130       40         METEOROLOGICAL SITE       DIR (DEG)       30       250       240       60       300       250       310       215       25.5       2.1       0.306         METEOROLOGICAL SITE       DIR (DPH)       5.2       5.1       6.5       6.0       9.2       8.0       5.6       2.1       0.306         METEOROLOGICAL SITE       DIR (PPH)       5.8       6.6       7.3       9.5       9.2       0.915       0.40       5.6       5.6       5.6       5.6       5.6       5.6       5.6       2.1       0.366       3306       3366  | WM-SITE (SAMPLES)         RANK         1         2         3         4         5         6         7         8         9         10           METEOROLOGICAL SITE<br>BRIDGEPORT VEL (MPH)         5,2         5,1         <   |

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| TABLE |

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1985 TEN HIGHEST 24-HOUR AVERAGE SO2 DAYS WITH WIND DATA

|           |                     |                   |   | L.                              | Top.   |                                 |  |        |  |                                 | M                               | 5  |                                 |                                  |                    |                  |                           |   | t                              |                    |
|-----------|---------------------|-------------------|---|---------------------------------|--|---------------------------------|--|--------|--|---------------------------------|---------------------------------|--|---------------------------------|----------------------------------|--------------------|------------------|---------------------------|---|--------------------------------|--------------------|
| SIC METER | 10                  | 51                | 12/22/85<br>230<br>8.9                      | 0.887<br>210<br>4.9             | 0.831<br>240                                 | 11.4<br>0.959<br>240            | 9.1<br>10.9<br>0.830                             |        | 46<br>1/ 7/85<br>10                        | 0<br>0<br>0<br>0<br>0<br>0<br>0 | 0.417<br>10<br>6.8              | 0.910  | 9.6                             | 070.0<br>70<br>7.9               | 8.1<br>0.985       | 1                | 2/14/85<br>240            | 12.4  | 0.945<br>210<br>0.0            | 0.910<br>0.910     |
| AMS / CUB | 6                   | 54                | 74/8/<br>240<br>8.0<br>8.0                  | 0.911<br>240<br>3.9             | 0.803<br>250                                 | 7.5<br>0.844<br>270             | $\begin{array}{c} 6.9\\ 8.1\\ 0.857 \end{array}$ |        | 49<br>1/24/85<br>250                       | 12.0                            | 0.94/<br>220<br>4.7             | 6.0<br>0.786<br>250                              | 11.2                            | 290<br>290<br>11.9               | 12.1<br>0.982      | 5                | 11/24/85<br>290           | 10.6  | 0.109<br>300<br>5.0            | 8.3<br>0.602       |
| : MICROGR | 80                  | 54                | 12/29/85<br>240<br>4.2                      | 0.661<br>210<br>5.4             | 0.829  | 7.8<br>0.831<br>230             | 8.1<br>8.3<br>0.966                              |        | 50<br>12/23/85<br>100                      | 0.0<br>- 0<br>- 0<br>- 0<br>- 0 | 0.909<br>190<br>6.4             | 6.9<br>0.932<br>250                              | 0.00                            | 0.972<br>230<br>10.4             | 0.989              | 6                | 2/15/85<br>260            | 4.6   | 0.946<br>240<br>540            | 0.889              |
| UNITS     | 7                   | 55                | 2/14/85<br>240<br>12.4                      | 0.945<br>210<br>9.0             | 0.910<br>240                                 | 12.2<br>0.980<br>250            | 12.3<br>12.4<br>0.991                            | 4      | 53<br>12/11/85<br>30                       | 2.03                            | 0.260<br>3.2                    | $ \begin{array}{c} 3.9\\ 0.834\\ 50\end{array} $ | 00.<br>1.1<br>1.1               | 0.5<br>0.5                       | 5.0<br>0.093       | 0                | 12/21/85<br>300           | 7.9   | 0.914<br>330<br>1 7            | 6.5<br>0.731       |
|           | 9                   | 56                | 12/23/85<br>190<br>6.4                      | 0.909<br>190<br>6.4             | 0.932  | 9.5<br>0.972<br>230             | 10.4<br>10.5<br>0.989                            | e<br>L | 53<br>12/ 5/85<br>10                       | 5.5<br>5.0<br>5.0               | 0.805<br>20<br>3.1              | $3.4 \\ 0.913 \\ 40$                             | 4 SC 5                          | 4.5<br>4.5                       | 5.9<br>0.759       | ġ                | 2/16/85                   | 10.7  | 0.930<br>240<br>6 h            | 7.2<br>0.892       |
|           | 5                   | 56                | 28/12/21<br>300<br>7.9<br>8.6               | 0.914<br>330<br>4.7             | 0.731<br>310<br>8_0                          | 9.2<br>0.865<br>310             | 5.1<br>7.0<br>0.724                              | l      | 56<br>12/ 9/85<br>270                      |                                 | 0.848<br>330<br>2.8             | 3.1<br>0.759<br>270                              |                                 | 0.747<br>280<br>5.7              | $6.3 \\ 0.904$     | ξÛ               | 2/ 5/85<br>40             | 7.9<br>8.9  | 0.004<br>30<br>2 6             | 3.6<br>0.712       |
|           | 4                   | 62<br>27 = 795    | 7.9<br>04<br>7.9<br>0 8                     | 0.884<br>30<br>2.6              | 0.712<br>60                                  | 11.8<br>0.979<br>90             | 0.8<br>5.9<br>0.138                              | ľ      | 2/ 5/85                                    | 6.8                             | 0.884<br>30<br>2.6              | 3.6<br>0.712<br>60                               | 11.5                            | 676.0<br>90<br>8.0               | 5.9<br>0.138       | ξU               | 1/ 4/85<br>360            | 7.2   | 0.090<br>10                    | 1.9<br>0.558       |
|           | 3                   | 64<br>64          | 12/24/85<br>190<br>2.5<br>3.5               | 0.789<br>190<br>1.7             | 0.296<br>140<br>200                          | 5.0<br>0.398<br>190             | 5.6<br>6.8<br>0.833                              |        | 65<br>1/14/85<br>240                       | 0.00                            | 0.911<br>240<br>3.9             | 0.803<br>250                                     | 6.3<br>7.5                      | 0.044<br>270<br>6.9              | 0.857              | 77               | 1/28/85<br>300            | 6.8<br>9.3  | 0.723<br>320<br>320            | 3.3<br>0.983       |
|           | N                   | 68<br>68<br>68    | 1/18/85<br>230<br>3.8<br>5.2                | 0.735<br>200<br>1.9             | 0.693<br>210<br>6.8                          | $\frac{7.3}{0.932}$             | 7.3<br>8.2<br>0.891                              | Ň      | 66<br>1/31/85<br>30                        | 7.5                             | 0.920<br>10<br>10               | 0.966<br>40                                      | 10.5                            | 0.714<br>60<br>4.0               | 5.2<br>0.763       | 3                | 1/14/85<br>240            | 880<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9<br>9 | 0.911<br>240<br>3 0            | 4.9<br>0.803       |
|           | -                   | 76                | 12/20/85<br>10<br>4.6<br>5.0                | 0.786<br>300<br>1.6             | 4.2<br>0.384<br>30<br>5.2                    | 0.900<br>260                    | 3.5<br>7.9<br>0.442                              | 0      | 89<br>12/20/85<br>10                       |                                 | 0.786<br>300<br>1.6             | 0.384   30   30   30   30   30   30   30   3     | 5.8                             | 0.300<br>260<br>3.5              | 7.9<br>0.442       | U Y              | 2/21/85<br>160            | 3.6   | 0.490<br>190<br>3 3            | 4.6                |
|           | RANK                | S02               | DAIE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH) | SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH) | SPD (MPH)<br>RATIO<br>DIR (DEG) | VEL (MPH)<br>SPD (MPH)<br>RATIO                  |        | SOZ<br>DATE<br>DIR (DFG)                   | VEL (MPH)<br>SPD (MPH)          | KALIU<br>DIR (DEG)<br>VEL (MPH) | SPU (MPH)<br>RATIO<br>DIR (DEG)                  | VEL (MPH)<br>SPD (MPH)<br>BATIO | DIR (DEG)<br>VEL (MPH)           | SPD (MPH)<br>RATIO | 000              | DATE<br>DATE<br>DIR (DEG) | VEL (MPH)<br>SPD (MPH)  | DIR (DEG)<br>VEI (MDH)         | SPD (MPH)<br>RATIO |
|           | TOWN-SITE (SAMPLES) | ENFIELD-005 (345) | METEOROLOGICAL SITE<br>NEWARK               | METEOROLOGICAL SITE<br>BRADLEY  | METEOROLOGICAL SITE<br>BRIDGEPORT            | METEOROLOGICAL SITE             | WORCESTER  |        | GREENWICH-017 (357)<br>MFTFORDIOGICAL SITF | NEWARK                          | METEOROLOGICAL SITE<br>BRADLEY  | METEOROLOGICAL SITE                              | BRIDGEPORT                      | METEOROLOGICAL SITE<br>WORCESTER |                    | CDOTON-007 (354) | METEOROLOGICAL SITE       | NEWARK  | METEOROLOGICAL SITE<br>BRANIEV |                    |

|                               | 198   | 5 TEN HI                     | GHEST 24-                         | HOUR AVEF                          | AGE SO2 D                             | AYS WITH I                        | HIND DATA   | UNITS                               | : MICROGR                   | AMS / CUB                    | IC METER                     |
|-------------------------------|---|------------------------------|-----------------------------------|------------------------------------|---------------------------------------|-----------------------------------|---|-------------------------------------|-----------------------------|------------------------------|------------------------------|
| (SAMPLES)                     | RANK  | -                            | 0                                 | ς                                  | 4                                     | ŋ                                 | 9   | 7                                   | ω                           | 6                            | 10                           |
| JROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>BATHO              | 130<br>2.5<br>4.6            | 250<br>6.3<br>7.5                 | 300<br>6.0<br>7.3<br>813           | 20<br>2.0<br>4.7                      | 60<br>11.5<br>11.8<br>070         | 240<br>11.5<br>11.8<br>0 077  | 310<br>8.0<br>8.5<br>8.5            | 260<br>9.5<br>10.4          | 280<br>10.7<br>11.4          | 240<br>12.0<br>12.2          |
| JROLOGICAL SITE<br>WORCESTER  | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO              | 0.699<br>0.699               | 270<br>270<br>6.9<br>8.1<br>0.857 | 0.945<br>0.945                     | 250<br>250<br>4.0<br>0.463            | 0.138<br>0.138                    | 270<br>9.3<br>0.968   | 310<br>5.1<br>7.0<br>0.724          | 8.5<br>0.971                | 260<br>10.5<br>11.2<br>0.934 | 250<br>250<br>12.3<br>0.991  |
| 123 (361)                     | SO2<br>DATE   | 114<br>2/ 5/85               | 101<br>12/24/85                   | 100<br>1/31/85                     | 95<br>12/20/85                        | 93<br>1/18/85                     | 89<br>1/14/85   | 87<br>87<br>12/29/85                | 84<br>2/ 1/85               | 83<br>2/21/85                | 82<br>1/28/85                |
| JROLOGICAL SITE<br>NEWARK     | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)                       | 40<br>7.9<br>8.9             | 2.5<br>2.5<br>2.5                 | 30<br>7.5                          |                                       | 5.080<br>1.080<br>1.080           | 540<br>58<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5<br>5 |                                     | 10.7<br>10.8                | 3.6<br>3.6                   | 300<br>9.3<br>1.3<br>200     |
| JROLOGICAL SITE<br>BRADLEY    | KALLU<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)              | 0.884<br>30<br>3.6<br>3.6    | 0.789<br>190<br>5.6<br>5.6        | 0.20<br>5.1<br>5.3                 | 0.780<br>300<br>4.2                   | 200<br>200<br>2.7                 | 0.911   | 0.001<br>5.5                        | 0. 390<br>5. 9              | 0.450<br>3.3<br>4.6          |                              |
| DROLOGICAL SITE<br>BRIDGEPORT | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)              | 0.712<br>60<br>11.5          | 0.296<br>140<br>2.0<br>5.0        | 0.966<br>40<br>10.5<br>10.8        | 0.384<br>5.2<br>5.8                   | 0.693<br>210<br>7.3               | 0.803<br>250<br>7.5   | 0.829<br>240<br>6.5<br>7.8          | 0.981<br>20<br>8.8<br>9.2   | 0.711<br>2.5<br>4.6          | 0.983<br>300<br>6.0<br>7.3   |
| JROLOGICAL SITE<br>WORCESTER  | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO     | 0.979<br>90<br>5.9           | 0.398<br>190<br>5.6<br>6.8        | 0.974<br>60<br>4.0<br>5.2<br>0.763 | 0.900<br>260<br>3.5<br>7.9            | 0.932<br>300<br>7.3<br>8.2<br>891 | 0.844<br>270<br>6.9<br>8.1<br>8.7   | 0.831<br>230<br>8.1<br>8.3<br>0.966 | 0.952<br>60<br>5.2<br>0.974 | 0.551<br>280<br>5.5<br>1.9   | 0.813<br>300<br>9.5<br>0.945 |
|                               |   |                              |                                   |                                    |                                       |                                   |   |                                     |                             |                              |                              |
| 02 (349)                      | SO2<br>DATF   | 133<br>2/ 9/85               | 132<br>1/26/85                    | 125<br>1/ 8/85                     | 110<br>12/14/85                       | 109<br>1/14/85                    | 108<br>4/17/85  | 12/ 3/85                            | 105<br>1/28/85              | 102                          | 101<br>1/17/85               |
| OROLOGICAL SITE<br>NEWARK     | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)                       | 22.9<br>22.9                 | 19.8<br>19.8                      | 20.7                               | 310                                   | 240<br>8.8<br>8.8                 | 330<br>15.9   | 310<br>19.9<br>20.3                 | 300<br>9.3<br>9.3           | 320<br>16.6<br>17.8          | 2550<br>8.4<br>8.7           |
| OROLOGICAL SITE<br>BRADLEY    | KALLO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)              | 0.982<br>340<br>15.3<br>15.5 | 0.969<br>330<br>9.0<br>9.8        | 0.930<br>330<br>10.6<br>11.1       | 0.964<br>330<br>12.8<br>13.2          | 0.911<br>240<br>3.9<br>4.9        | 0.978<br>330<br>12.9<br>13.7  | 0.982<br>310<br>16.5                | 0.723<br>3.3<br>3.3<br>3.3  | 0.931<br>340<br>10.2<br>10.9 | 0.789<br>300<br>3.6<br>3.6   |
| OROLOGICAL SITE<br>BRIDGEPORT | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)              | 0.982<br>320<br>15.9         | 0.920<br>320<br>13.4              | 0.960<br>310<br>15.2               | 0.966<br>310<br>15.6                  | 0.803<br>250<br>6.3               | 0.945<br>330<br>11.3<br>11.5  | 0.966<br>320<br>11.1                | 0.983<br>300<br>7.3         | 0.932<br>310<br>11.3         | 0.090<br>2.10<br>2.10        |
| OROLOGICAL SITE<br>WORCESTER  | KALLO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>SPD (MPH) | 0.990<br>340<br>18.8<br>19.0 | 0.983<br>330<br>17.8<br>18.8      | 0.971<br>320<br>11.3<br>12.2       | 0.900<br>290<br>14.1<br>14.5<br>0 075 | 0.844<br>270<br>6.9<br>8.1<br>8.1 | 0.984<br>300<br>14.3<br>15.0<br>056   | 0.916<br>280<br>15.5<br>16.0        | 0.813<br>300<br>9.5<br>0.10 | 0.9/3<br>15.2<br>16.7        | 0.200<br>3310<br>24.9<br>265 |
|                               | DI IN   | 0. 220                       | ナナハ・つ                             | 0.760                              | 0.716                                 | 110.0                             | 0.2.0   | 0.710                               | C • 7 4 V                   | 0.010                        | 100.0                        |

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TABLE 17, CONTINUED

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|            |                     | ( )  | 0  | $\langle 0 \rangle$   |
|------------|---------------------|--|--|---|
| IC METER   | 10                  | 12/21/85<br>300<br>7.9<br>7.9<br>7.9<br>8.0<br>310<br>310<br>310<br>310<br>310<br>310<br>310<br>310<br>310<br>31   | $\begin{array}{c} \begin{array}{c} & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & & & \\ & & & & & & & & \\ & & & & & & & \\ & & & & & & & \\ & & & & & & & & \\ & & $   | 12/20/85<br>10<br>10<br>5.9<br>0.786<br>0.786<br>1.6<br>0.384   |
| AMS / CUB  | 6                   | 2/ 4/85<br>280<br>280<br>7.4<br>7.4<br>7.4<br>7.4<br>7.4<br>8.2<br>0.921<br>0.921<br>0.921<br>0.921<br>0.921<br>0.921<br>0.921<br>0.921  | 2/14/85<br>2/14/85<br>240<br>2240<br>2240<br>2240<br>2240<br>2240<br>2240<br>2240  | 2/21/85<br>2/21/85<br>3.6<br>3.6<br>0.496<br>3.3<br>4.6<br>0.711  |
| : MICROGR  | 8                   | 2/15/85<br>260<br>9.9<br>9.9<br>9.9<br>0.946<br>0.946<br>0.946<br>0.946<br>0.946<br>0.946<br>0.946<br>0.926<br>0.926<br>0.926<br>0.971<br>0.971  | 1/14/85<br>240<br>8.0<br>8.0<br>8.0<br>8.0<br>8.0<br>7.5<br>0.81<br>0.81<br>0.857<br>0.857<br>0.857<br>0.857   | 149<br>1/28/85<br>6.8<br>6.8<br>6.8<br>6.8<br>0.723<br>3.3<br>3.3<br>0.983                                      |
| UNITS      | ~                   | 12/22/85<br>230<br>8.9<br>8.9<br>8.9<br>8.9<br>8.7<br>8.9<br>7.9<br>10.1<br>11.4<br>11.4<br>11.4<br>9.1<br>9.1<br>9.1<br>0.83<br>0.83<br>0.83<br>0.83<br>0.83<br>0.83<br>0.83<br>0.83  | $\begin{smallmatrix} & & & & & & & & & & & & & & & & & & &$  | 153<br>2/15/85<br>9.4<br>9.9<br>0.946<br>5.5<br>0.889   |
| WIND DAIA  | Q                   | 12/11/85<br>30<br>1.3<br>0.250<br>0.250<br>0.834<br>0.834<br>0.811<br>0.811<br>0.655<br>0.55<br>0.55<br>0.55<br>0.093<br>0.55<br>0.093<br>0.55<br>0.093<br>0.093<br>0.093<br>0.093<br>0.093<br>0.093<br>0.093<br>0.093<br>0.003<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.002<br>0.00000000  | 0.966<br>0.966<br>0.966<br>0.823<br>0.865<br>0.885<br>0.8831<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.821<br>0.821<br>0.821<br>0.825<br>0.821<br>0.825<br>0.825<br>0.825<br>0.825<br>0.825<br>0.825<br>0.825<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0.855<br>0 | 154<br>1/14/85<br>240<br>8.8<br>8.8<br>8.8<br>0.911<br>3.9<br>240<br>3.9<br>4.9<br>0.803                        |
| AYS WITH   | ñ                   | 12/24/85<br>2.5<br>2.5<br>2.5<br>2.5<br>2.5<br>1.7<br>1.7<br>1.7<br>1.7<br>1.7<br>1.7<br>1.7<br>1.7<br>1.7<br>1.7  | 12/23/85<br>141<br>190<br>190<br>190<br>190<br>10.5<br>0.932<br>10.4<br>10.4<br>10.4<br>10.5<br>0.989<br>0.989   | 158<br>3/27/85<br>220<br>10.5<br>10.9<br>0.99<br>5.7<br>0.993   |
| AGE SUZ D  | 4                   | 1/28/85<br>6.8<br>6.8<br>6.8<br>6.8<br>3.3<br>3.3<br>3.3<br>0.723<br>3.3<br>3.0<br>0.933<br>9.5<br>0.945<br>0.945  | 12/22/85<br>230<br>230<br>230<br>2210<br>2210<br>210<br>10.9<br>0.837<br>10.9<br>0.837<br>0.830<br>0.830<br>0.830<br>0.830   | 2/ 5/85<br>2/ 5/85<br>7.9<br>7.9<br>0.884<br>0.884<br>30<br>2.6<br>3.6<br>0.712                                 |
| HUUK AVEK  | ю                   | $\begin{array}{c} 1/31/85\\ 1/31/85\\ 7.1\\ 7.1\\ 7.1\\ 7.1\\ 7.1\\ 7.1\\ 7.5\\ 0.956\\ 0.956\\ 10.5\\ 10.5\\ 10.5\\ 10.5\\ 10.5\\ 10.5\\ 10.5\\ 0.974\\ 0.974\\ 0.974\\ 0.763$  | 12/144<br>1227/85<br>12220<br>1226<br>132.6<br>132.6<br>132.6<br>132.4<br>0.952<br>14.8<br>0.952<br>14.8<br>0.957<br>0.957<br>0.957<br>0.957   | 1/19/85<br>240<br>8.5<br>10.1<br>0.841<br>5.5<br>0.911<br>0.911   |
| 164ES1 24- | 5                   | 12/20/85<br>12/20/85<br>10<br>10<br>1.6<br>1.6<br>1.6<br>0.786<br>0.786<br>0.786<br>0.786<br>0.786<br>0.786<br>0.719<br>0.442<br>0.442   | 11/28/85<br>11/28/85<br>11/28/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>147<br>128/85<br>147<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85<br>128/85   | 181<br>1/18/85<br>230<br>3.8<br>3.8<br>3.8<br>3.8<br>0.735<br>1.9<br>1.9<br>0.693                               |
|            |                     | 2/ 5/85<br>40<br>7.9<br>7.9<br>7.9<br>8.9<br>8.9<br>8.9<br>7.12<br>60<br>7.12<br>60<br>7.12<br>60<br>7.12<br>60<br>0.712<br>60<br>0.712<br>60<br>0.712<br>60<br>0.712<br>60<br>0.73<br>8.9<br>0.8<br>8.9<br>0.8<br>8.9<br>0.8<br>8.9<br>0.8<br>8.9<br>0.8<br>8.9<br>0.8<br>8.9<br>0.8<br>8.9<br>0.8<br>8.9<br>0.8<br>8.9<br>0.8<br>8.9<br>0.8<br>8.9<br>0.8<br>8.9<br>0.7<br>7.9<br>8.9<br>0.8<br>8.9<br>0.7<br>7.9<br>8.9<br>0.8<br>8.9<br>0.8<br>8.9<br>0.8<br>8.9<br>0.7<br>7.9<br>8.9<br>0.7<br>7.9<br>8.9<br>0.7<br>7.9<br>8.9<br>0.7<br>7.9<br>8.9<br>0.7<br>7.9<br>8.9<br>0.7<br>7.12<br>7.85<br>0.7<br>7.9<br>7.9<br>7.9<br>7.9<br>7.9<br>7.9<br>7.9<br>7.9<br>7.9<br>7  | 1/174<br>230<br>230<br>230<br>2500<br>2200<br>210<br>2513<br>0.633<br>0.932<br>0.932<br>0.891<br>0.891   | 2/ 4/85<br>2/ 4/85<br>280<br>7.4<br>8.2<br>0.907<br>320<br>4.3<br>4.3<br>0.665                                  |
| - 7        | RANK                | S02<br>DATE<br>DATE<br>VEL (MPH)<br>SPD (MPH)<br>SP | S02<br>DIATE<br>DIATE<br>VEL (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>VEL (MPH)<br>DIR (DEG)<br>DIR (DEG)<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)   | S02<br>DATE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>SPD (MPH) |
|            | TOWN-SITE (SAMPLES) | NEW BRITAIN-011 (360)<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE  | NEW HAVEN-017 (341)<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE  | NEW HAVEN-123 (357)<br>METEOROLOGICAL SITE<br>NEWARK<br>METEOROLOGICAL SITE<br>BRADLEY                          |

TABLE 17, CONTINUED

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1085 TEN HIGHEST 20-HOUR AVERAGE SO2 DAVS WITH

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| 10                  | 30<br>5.2<br>5.8                    | 200<br>260<br>7.9<br>142                              | 88<br>23/85       | 190<br>7.0                          | 190<br>190<br>7.4                            | 2005                              | 012<br>230<br>230                            | ر . ر<br>89        | 43<br>21/85         | 300                           | 914<br>330<br>330                            | 5:5<br>ر<br>10                                     | 3.0<br>5.2                      | 310                              | 7.0<br>724         |
|---------------------|-------------------------------------|---|-------------------|-------------------------------------|--|-----------------------------------|--|--------------------|---------------------|-------------------------------|--|--|---------------------------------|----------------------------------|--------------------|
| •-                  |                                     | 0 0   | 5 12/2            | · ••••••                            |  | 0                                 | 0  | 0.0                | 2/01 2              | ]                             | 0  | 00   | с.<br>С                         | 5                                | 0                  |
| 6                   | 130<br>2.5<br>4.6                   | 0.551<br>280<br>7.9<br>0.699                          | 12/ 9/85          | 270                                 | 0.848<br>330<br>2.8<br>3.7                   | 0.759<br>270<br>5.6               | 0.945  | 6.3<br>0.904       | 44<br>3 / 27 / 85   | 10.5                          | 0.961  | 5.8<br>0.993<br>220                                | 8.5<br>8.5<br>066               | 240                              | 9.1<br>0.798       |
| Ø                   | 300<br>6.0<br>7.3                   | 0.813<br>300<br>9.5<br>0.945                          | 94<br>12/24/85    | 2.5                                 | 0.789<br>190<br>5.6                          | 0.296<br>140<br>2.0               | 0.398<br>190<br>5.6                          | 6.8<br>0.833       | 45<br>1 / 22 / 85   | 250                           | 0.994<br>270<br>8 5                          | 10.8<br>0.789<br>270                               | 15.3<br>15.7<br>0 078           | 280                              | 22.9               |
| 7                   | 260<br>9.5<br>10.4                  | 0.920<br>260<br>8.2<br>8.5<br>0.971                   | 94<br>2/ 5/85     | 40<br>7.9<br>8.9                    | 0.884<br>30<br>3.6<br>3.6                    | 0.712<br>60<br>11.5               | 0.979<br>90<br>8.0                           | 0.138              | 46<br>2/5/85        |                               | 0.884<br>30                                  | 3.6<br>0.712<br>60                                 | 11.5<br>11.8<br>0 070           | 06                               | 5.9<br>0.138       |
| 9                   | 250<br>6.3<br>7.5                   | 0.844<br>270<br>6.9<br>8.1<br>0.857                   | 102<br>1/19/85    | 240<br>8.5<br>10.1                  | 0.841<br>5.0<br>5.5                          | 0.911<br>260<br>9.6               | 0.864  | 0.726              | 46<br>2/16/85       | 250<br>10.7                   | 0.930  | 7.2<br>0.892<br>240                                | 11.5<br>11.8<br>0 077           | 9.3                              | 9.6<br>0.968       |
| 5                   | 220<br>8.5                          | 0.966<br>240<br>7.2<br>9.1<br>0.798                   | 103<br>1/31/85    | 30                                  | 0.220<br>5.10<br>5.3                         | 0.966<br>40<br>10.5               | 0.974<br>60<br>4.0                           | 0.763              | 46<br>2/14/85       | 240<br>12.4                   | 0.945<br>210<br>9_0                          | 0.910<br>240                                       | 12.0<br>12.2<br>0 080           | 250                              | 12.4               |
| 4                   | 60<br>11.5                          | 0.9/9<br>90<br>5.9<br>0.138                           | 110<br>1/14/85    | 240<br>8.0<br>8.8                   | 0.911<br>240<br>3.9<br>4.9                   | 0.803<br>250<br>6.3               | 0.844<br>270<br>6.9                          | 0.857              | 49<br>1/14/85       | 240<br>8.0                    | 0.911<br>240                                 | 4.9<br>0.803<br>250                                | 6.3<br>7.5<br>0 800             | 270<br>6.9                       | 8.1<br>0.857       |
| 3                   | 260<br>9.6                          | 0.864<br>5.3<br>7.3<br>0.726                          | 116<br>12/20/85   | 10<br>10<br>10<br>10                | 0.780<br>300<br>1.6<br>4.2                   | 0.384<br>30<br>5.2                | 0.900  | 0.442              | 49<br>1/28/85       | 300<br>9.8<br>9.8             | 0.723  | $ \begin{array}{c} 3.3\\ 0.983\\ 300 \end{array} $ | 6.0<br>7.3<br>0 813             | 300                              | 10.1<br>0.945      |
| N                   | 210<br>6.8<br>7.3                   | 0.932<br>300<br>8.2<br>0.891                          | 121<br>2/ 4/85    | 280<br>7.4                          | 0.90/<br>320<br>4.3<br>6.5                   | 0.665                             | 0.765<br>290<br>7.1                          | 0.921              | 50<br>50<br>2723785 | 8.7                           | 0.944<br>180<br>3.9                          | 0.969<br>230                                       | 3.7<br>5.2<br>715               | 270                              | 10.4<br>0.959      |
|                     | 250<br>5.1                          | 0.92<br>290<br>7.1<br>7.8<br>0.921                    | 122<br>1/28/85    | 300<br>9.3<br>9.3                   | 0. /23<br>320<br>3.3<br>3.3                  | 0.983<br>300<br>6.0<br>7.3        | 0.813<br>300<br>9.5                          | 0.945              | 52<br>1724/85       | 250                           | 0.947<br>220<br>4.7                          | 6.0<br>0.786<br>250                                | 11.2<br>11.4<br>0 087           | 290                              | 12.1<br>0.982      |
| RANK                | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | KALLO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO | SO2<br>DATE       | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | KALLU<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH) | RATIO<br>DIR (DEG)<br>VEL (MPH)   | STD (MFH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH) | SPU (MPH)<br>RATIO | SO2<br>DATF         | VEL (MPH)                     | SFU (MFH)<br>RATIO<br>DIR (DEG)<br>VFI (MPH) | SPD (MPH)<br>RATIO<br>DIR (DEG)                    | VEL (MPH)<br>SPD (MPH)<br>RATIO | DIR (DEG)<br>VEL (MPH)           | SPD (MPH)<br>RATIO |
| TOWN-SITE (SAMPLES) | METEOROLOGICAL SITE<br>BRIDGEPORT   | METEOROLOGICAL SITE<br>WORCESTER                      | NORWALK-013 (364) | METEOROLOGICAL SITE<br>NEWARK       | METEOROLOGICAL SITE<br>BRADLEY               | METEOROLOGICAL SITE<br>BRIDGEPORT | METEOROLOGICAL SITE<br>WORCESTER             |                    | PRESTON-002 (349)   | METEOROLOGICAL SITE<br>NEWARK | METEOROLOGICAL SITE<br>BRADIFY               | METEOROLOGICAL SITE                                | BR I DGE PORT                   | METEOROLOGICAL SITE<br>WORCESTER |                    |

1985 TEN HIGHEST 24-HOUR AVERAGE SO2 DAYS WITH WIND DATA

TABLE 17, CONTINUED

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TABLE 17, CONTINUED

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1985 TEN HIGHEST 24-HOUR AVERAGE SO2 DAYS WITH WIND DATA

| ¥  | 1 2   | m  | 1  | ц.  | v  | UNITS<br>7  | : MICROGF<br>8  | RAMS / CUB   | 10<br>10  |
|--|---|--|--|---|--|---|---|--|---|
| E E E E E E E E E E E E E E E E E E E  | 23     104     10       0/85     1/28/85     1/14       16     5.8     8.       .6     6.8     8.       .9     0.723     0.91       .20     3.3     3.       .20     3.3     3.       .2     3.3     24       .2     0.983     0.84       .2     0.983     0.84       .2     0.945     0.84       .5     10.1     8.       .5     10.1     8. | 57<br>7002<br>57<br>7700<br>57<br>7700<br>57<br>7700<br>57<br>7700<br>57<br>7700<br>57<br>7700<br>57<br>7700<br>57<br>7700<br>57<br>7700<br>57<br>7700<br>57<br>7700<br>57<br>7700<br>57<br>7700<br>57<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50<br>50   | /21/85<br>160<br>160<br>170<br>170<br>170<br>190<br>190<br>190<br>190<br>190<br>190<br>190<br>190<br>190<br>19   | 94<br>1/31/85<br>7.1<br>7.1<br>7.1<br>7.1<br>7.5<br>0.976<br>10.5<br>10.5<br>10.5<br>10.5<br>10.5<br>0.974<br>60<br>4.60<br>4.60<br>0.763   | 12/23/85<br>190<br>6.4<br>7.0<br>190<br>6.9<br>190<br>9.55<br>0.972<br>0.972<br>0.972<br>0.989 | 12/ 9/85<br>270<br>270<br>2.70<br>2.88<br>2.88<br>2.88<br>0.759<br>0.759<br>0.759<br>0.945<br>0.945<br>0.904<br>0.904   | 2/ 4/85<br>280<br>280<br>7.4<br>7.4<br>0.90.2<br>6.5<br>0.66.5<br>0.66.5<br>7.1<br>0.755<br>0.721<br>0.921                  | 12/ 5/85<br>12/ 5/85<br>0.80.6<br>3.11<br>0.90.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75.5<br>0.75 | $\begin{array}{c} 1/19/85\\ 240\\ 240\\ 240\\ 10.1\\ 10.1\\ 10.240\\ 5.50\\ 0.911\\ 10.266\\ 0.915\\ 0.915\\ 0.915\\ 0.915\\ 0.915\\ 0.915\\ 0.126\\ $  |
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1/24/85<br>12:0<br>12:0<br>12:0<br>12:0<br>12:0<br>0.987<br>11:4<br>0.987<br>0.987<br>0.987<br>11:4<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.9970<br>0.9970<br>0.9970<br>0.9970<br>0.9970<br>0.9970<br>0.9970<br>0.99700<br>0.99700<br>0.99700<br>0.9970000000000 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|          | WITH WIND DATA |
|----------|----------------|
| 0        | DAYS           |
| INUE     | S02            |
| I7, CONT | AVERAGE        |
| TABLE    | 24-HOUR        |
|          | HIGHEST        |
|          | TEN            |
|          | 1985           |

|   | }  |   | -<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>- |   |  |  |   | UNITS   | : MICROG  | RAMS / C                            | UBIC METER   |
|---|--|---|---|---|--|--|---|---|---|-------------------------------------|--|
| TOWN-SITE (SAMPLES)   | RANK   | -   | N   | ю   | Ţ  | ŋ  | 9   | 7   | ø   | 6                                   | 10   |
| METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>WORCESTER | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO | 300<br>6.0<br>7.3<br>0.813<br>9.5<br>0.945<br>0.945 | 270<br>5.6<br>5.9<br>0.945<br>5.7<br>0.904  | 210<br>6.8<br>7.3<br>0.932<br>7.3<br>7.3<br>0.891 | 140<br>2.0<br>3.398<br>1.398<br>5.8<br>0.833 | 11.5<br>11.5<br>0.979<br>0.90<br>0.90<br>0.138 | 250<br>5.1<br>6.6<br>0.765<br>7.9<br>7.9<br>0.921 | 130<br>2.55<br>2.55<br>2.55<br>2.55<br>2.55<br>0.699<br>0.699 | 250<br>250<br>270<br>270<br>270<br>270<br>270<br>270<br>270<br>270<br>270<br>27 | 240<br>6.5<br>0.831<br>8.3<br>0.966 | 0.956<br>0.939<br>12.30<br>0.960<br>0.969<br>0.969 |

### **IV. OZONE**

### HEALTH EFFECTS

Ozone is a poisonous form of oxygen and the principal component of modern smog. Until recently, EPA called this type of pollution "photochemical oxidants." The name has been changed to ozone because ozone is the only oxidant actually measured and is the most plentiful.

Ozone and other oxidants -- including peroxyacetal nitrates (PAN), formaldehyde and peroxides -are not usually emitted into the air directly. They are formed by chemical reactions in the air from two other pollutants: hydrocarbons and nitrogen oxides. Energy from sunlight is needed for these chemical reactions. This accounts for the term photochemical smog and the daily variation in ozone levels, which increase during the day and decrease at night.

Ozone is a pungent gas with a faintly bluish color. It irritates the mucous membranes of the respiratory system, causing coughing, choking and impaired lung function. It aggravates chronic respiratory diseases like asthma and bronchitis and is believed capable of hastening the death, by pneumonia, of persons in already weakened health. PAN and the other oxidants that accompany ozone are powerful eye irritants.

### NATIONAL AMBIENT AIR QUALITY STANDARD

On February 8, 1979 the EPA established a national ambient air quality standard (NAAQS) for ozone of 0.12 ppm for a one-hour average. Compliance with this standard is determined by summing the number of days at each monitoring site over a consecutive three-year period when the 1-hour standard is exceeded and then computing the average number of exceedances over this interval. If the resulting average value is less than or equal to 1.0 (that is, if the fourth highest daily value in a consecutive three-year period is less than or equal to 0.12 ppm) the ozone standard is considered attained at the site. This standard replaces the old photochemical oxidant Standard of 0.08 ppm. The definition of the pollutant was changed along with the numerical value of the standard, partly because the instruments used to measure photochemical oxidants in the air really measure only ozone. Ozone is one of a group of chemicals which are formed photochemically in the air and are called photochemical oxidants. In the past, the two terms have often been used interchangeably. This 1985 Air Quality Summary uses the term "ozone" in conjunction with the NAAQS to reflect the change in both the numerical value of the NAAQS and the definition of the pollutant.

The EPA defines the ozone standard to two decimal places. Therefore, the standard is considered exceeded when a level of 0.13 ppm is reached. However, since the DEP still measures ozone levels to three decimal places, any one-hour average ozone reading which equals or is greater than 0.125 ppm is considered an exceedance of the 0.12 ppm standard in Connecticut. This interpretation of the ozone standard differs from the one used by the DEP before 1982, when a one-hour ozone concentration of 0.121 ppm was considered an exceedance of the standard.

### CONCLUSIONS

As in past years, Connecticut experienced very high concentrations of ozone in the summer months of 1985. Levels in excess of the one-hour NAAQS of 0.12 ppm were frequently recorded at each of the ten monitored sites. Two sites experienced levels greater than 0.20 ppm in 1985, as opposed to

five sites in 1984 and nine sites in 1983. Both the highest and the second highest one-hour concentrations decreased at all but the Middletown site in 1985, when compared to 1984.

The incidence of ozone levels in excess of the 1-hour 0.12 ppm standard was less in 1985 compared to 1984 (see Table 19). There was a total of 332 exceedances in 1984 and 152 in 1985 at those monitored sites that operated in both years. This represents a drop in the frequency of such exceedances from 9.2 per 1000 sampling hours in 1984 to 4.2 per 1000 sampling hours in 1985: a 54% decrease. If one eliminates the duplication that results when two or more sites experience an exceedance in the same hour, then the number of exceedances decreased from 146 to 72. On this basis, the state experienced a 50% decrease in the frequency of hourly exceedances of the standard.

The number of days on which the ozone monitors experienced ozone levels in excess of the 1-hour standard decreased from 128 in 1984 to 62 in 1985 at those monitoring sites that operated in both years (see Table 18). This represents a decrease in the frequency of such occurrences from 8.5 per 100 sampling days in 1984 to 4.1 per 100 sampling days in 1985: a 52% decrease. If the duplication that results when two or more sites experience an exceedance on the same day is eliminated, then the number of exceedances decreased from 34 to 21. On this basis, the state experienced a 38% drop in the frequency of daily exceedances of the standard.

The yearly changes in ozone concentrations can be attributed to year-to-year variations in regional weather conditions, especially wind direction, temperature and the amount of sunlight. A large portion of the peak ozone concentrations in Connecticut is caused by the transport of ozone and/or precursors (i.e., hydrocarbons and nitrogen oxides) from the New York City area and other points to the west and southwest. The percentage of southwest winds during the "ozone season" remained about the same from 1984 to 1985, as is shown by the wind roses from Newark (Figures 9 and 10). The wind roses from Bradley (Figures 7 and 8) are believed to be not as representative, since the airport is located in the Connecticut River Valley and the wind gets channeled up or down the valley. The magnitude of the high ozone levels can be partly associated with yearly variations in temperature. Ozone production is greatest at high temperatures and in strong sunlight. The summer season's daily high temperatures were lower in 1985 than in 1984. This is demonstrated by the number of days exceeding 90° F which decreased from nine in 1984 to three in 1985 at Sikorsky Airport in Bridgeport. At Bradley International Airport, the number of days exceeding 90°F decreased from twelve in 1984 to five in 1985. The percentage of possible sunshine at Bradley averaged 63% in 1984 and 59% in 1985 for the months June through September. The average for the summer months at Bradley is normally about 62%. This decrease in the percentage of possible sunshine and the resulting decrease in high temperature days are believed to be major factors in the decrease in the number of high ozone days in Connecticut in 1985.

### **METHOD OF MEASUREMENT**

The DEP Air Monitoring Unit uses chemiluminescent instruments to measure and record instantaneous concentrations of ozone continuously by means of a fluorescent technique. Properly calibrated, these instruments are shown to be remarkably reliable and stable.

### **DISCUSSION OF DATA**

Monitoring Network - In order to gather information which will further the understanding of ozone production and transport, and to provide real-time data for the daily Pollutant Standards Index, DEP operated a state-wide ozone monitoring network consisting of four types of sites in 1985 (see Figure 6):

Urban Advection from Southwest Suburban Rural Bridgeport, East Hartford, Middletown, New Haven
Danbury, Greenwich
Groton, Madison, Stratford
Stafford

Precision and Accuracy - The ozone monitors had a total of 147 precision checks during 1985. The resulting 95% probability limits were -6% to + 10%. Accuracy is determined by introducing a known amount of ozone into each of the monitors. Three different concentration levels are tested: low, medium, and high. The 95% probability limits, based on 10 audits conducted on the monitoring system, were: low, -6% to + 6%; medium, -9% to + 7%; and high, -9% to + 10%.

1-Hour Average - The 1-hour ozone standard was exceeded at all ten DEP monitoring sites in 1985. Moreover, the highest 1-hour average ozone concentrations were lower in 1985 than in 1984 at all the sites except Middletown 007. Danbury 123 had the largest decrease of 0.066 ppm.

The number of days on which the 1-hour standard was exceeded at each site during the summertime "ozone season" is presented in Table 18. The number of hours the ozone standard was exceeded is presented in Table 19 for each site. Table 20 shows the year's high and second high concentrations at each site.

10 High Days with Wind Data - Table 21 lists the ten highest 1-hour ozone averages and their dates of occurrence for each ozone site in 1985. The wind data associated with these high readings are also presented. (See the discussion of Table 11 in the TSP section for a description of the origin and use of these wind data.)

A majority (i.e., 72%) of the high ozone levels occurred on days with southwesterly winds. This is due to the special features of a southwest wind blowing over Connecticut. The first aspect of a southwest wind is that, during the summer, it usually accompanies high temperatures and bright sunshine, which are important to the production of ozone. The second is that it will transport precursor emissions from New York City and other urban areas to the southwest of Connecticut. It is the combination of these factors that often produces unhealthful ozone levels in Connecticut.



### NUMBER OF DAYS WHEN THE 1-HOUR OZONE STANDARD WAS EXCEEDED IN 1985

| SITE            | <u>APRIL</u> | MAY | JUNE | JULY | <u>AUG</u> . | <u>SEPT</u> . | TOTAL         | TOTAL FOR<br>LAST YEAR |
|-----------------|--------------|-----|------|------|--------------|---------------|---------------|------------------------|
| Bridgeport-123  | 0            | 0   | 0    | 2    | 2            | 0             | 4             | 12                     |
| Danbury-123     | 0            | 1   | 0    | 2    | 1            | 0             | 4             | 13                     |
| E. Hartford-003 | 0            | 2   | 0    | 0    | 1            | 0             | 3             | 7                      |
| Greenwich-017   | 0            | 2   | 1    | 4    | 5            | 1             | 13            | 17                     |
| Madison-002     | 0            | 0   | 1    | 4    | 2            | 0             | 7             | 18                     |
| Middletown-007  | 0            | 3   | 1    | 3    | 2            | 1             | 10            | 14                     |
| New Haven-123   | 0            | 0   | 1    | 3    | 2            | 0             | 6             | 12                     |
| Stafford-007    | 0            | 3   | 0    | 0    | 1            | 0             | 4             | 7                      |
| Stratford-007   | 0            | 1   | 2    | 5    | 3            | 2             | <u>13</u>     | <u>28</u>              |
|                 |              |     |      | тс   | DTAL SIT     | E DAYS        | <b>.62</b> 64 | L 128                  |
|                 |              |     | TO   |      | DIVIDUA      | L DAYS        | 21            | 34                     |

### NUMBER OF EXCEEDANCES OF THE 1-HOUR OZONE STANDARD IN 1985

| SITE                 | <u>APRIL</u> | MAY | JUNE | JULY   | <u>AUG</u> . | <u>SEPT</u> . | TOTAL     | TOTAL FOR<br>LAST YEAR |
|----------------------|--------------|-----|------|--------|--------------|---------------|-----------|------------------------|
| Bridgeport-123       | 0            | 0   | 0    | 3      | 7            | 0             | 10        | 33                     |
| Danbury-123          | 0            | 1   | 0    | 4      | 1            | 0             | 6         | 26                     |
| E. Hartford-003      | 0            | 3   | 0    | 0      | 1            | 0             | 4         | 9                      |
| Greenwich-017        | 0            | 3   | 1    | 6      | 14           | 1             | 25        | 49                     |
| Madison-002          | 0            | 0   | 1    | 10     | 10           | 0             | 21        | 53                     |
| Middletown-007       | 0            | 4   | 1    | 5      | 11           | 1             | 22        | 29                     |
| New Haven-123        | 0            | 0   | 2    | 5      | 7            | 0             | 14        | 29                     |
| Stafford-00 $\chi^1$ | 0            | 7   | 0    | 0      | 4            | 0             | 11        | 15                     |
| Stratford-007        | 0            | 1   | 5    | 18     | 12           | 3             | <u>39</u> | <u>89</u>              |
|                      |              |     |      | тот    | AL SITE      | HOURS         | 152       | 332                    |
|                      |              |     | тот  | ALINDI | VIDUAL       | HOURS         | 72        | 146                    |

### **1985 MAXIMUM 1-HOUR OZONE CONCENTRATIONS**



### SECONDARY STANDARD

\* Date is month/day/ending hour of occurrence.

N.B. When a listed concentration occurs more than once at a site, the earliest date is given.

| (11.0<br>230<br>11.0<br>230<br>11.4<br>2968<br>5.6<br>5.0<br>3.8<br>3.8<br>3.8<br>3.8<br>5.0<br>5.0<br>5.0<br>5.0<br>5.0<br>5.0<br>5.0<br>5.0<br>5.0<br>5.0 |
|---|
| 0 0   |
| 0   |
| N 0 M   |
| 0.92  |
| 0.14<br>8/15<br>23<br>11.   |
| 0<br>96<br>7<br>2<br>7<br>2<br>90   |
| 0.90<br>8.8<br>8.8  |
| 0 0   |
| 0.12  |

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|                                   | 198   | 5 TEN HIG                           | GHEST 1-HO                          | UR AVERAC                            | SE OZONE D   | AYS WITH                            | WIND DATA                    |                                     | UNITS :  | PARTS PER                     | MITLION                      |
|-----------------------------------|---|-------------------------------------|-------------------------------------|--------------------------------------|--|-------------------------------------|------------------------------|-------------------------------------|--|-------------------------------|------------------------------|
| TOWN/SITE (SAMPLES)               | RANK  | <b>F</b> .                          | N                                   | m                                    | 4  | <b>ک</b>                            | 9                            | 7                                   | œ  | 6                             | 10                           |
| METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)                       | 220<br>8.1<br>8.5                   | 230<br>5.9<br>7.6                   | 220<br>7.1<br>7.3                    | 130<br>5.6<br>5.6                                    | 200<br>7.4<br>8.1                   | 200<br>6.6<br>7.3            | 230<br>8.6<br>9.1                   | 220<br>6.8<br>7.3  | 230<br>11.3                   | 120<br>1-50<br>1-20          |
| METEOROLOGICAL SITE<br>WORCESTER  | RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO     | 0.950<br>250<br>6.8<br>8.3<br>0.817 | 0.772<br>220<br>8.4<br>9.5<br>0.881 | 0.965<br>250<br>9.6<br>10.6<br>0.904 | 0.824<br>220<br>5.3<br>0.857                         | 0.916<br>220<br>8.4<br>9.5<br>0.886 | 0.896<br>5.7<br>5.7<br>0.879 | 0.948<br>240<br>9.1<br>9.3<br>0.977 | 0.922<br>260<br>8.6<br>9.5<br>0.907  | 0.968<br>230<br>21.0<br>0.990 | 0.571<br>230<br>3.6<br>0.644 |
| GREENWICH-017 (3778)              | OZONE   | 0.171                               | 0.168                               | 0.148                                | 0.143  | 0.135                               | 0.133                        | 0.132                               | 0.129  | 0.129                         | 0.127                        |
| METEOROLOGICAL SITE<br>NEWARK     | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)                       | 8/17/85<br>230<br>11.0<br>4.11      | 8/14/8<br>230<br>6.1<br>0.5         | 7/30/85<br>290<br>6.0<br>0.0         | 220<br>220<br>8.3<br>10.1                            | 8/ 5/85<br>190<br>5.8               | 5/26/85<br>270<br>3.3        | 7/ 9/85<br>170<br>2.6               | 7/19/85<br>210<br>9.5  | 9/20/85<br>220<br>8.2         | 6/ 9/85<br>200<br>5.6        |
| METEOROLOGICAL SITE<br>BRADLEY    | RATIO<br>DIR (DEG)<br>VEL (MPH)                           | 0.968<br>210<br>5.9                 | 0.645<br>210<br>1.7                 | 0.609                                | 0.821<br>220<br>7.3                                  | 0.759<br>180<br>4.4                 | 0.405                        | 0.395<br>190<br>3.8                 | 0.955<br>6.20<br>1.00<br>1.00<br>1.00<br>1.00<br>1.00<br>1.00<br>1.00<br>1 | 0.981<br>200<br>3.80          | 0.841<br>190<br>4.0          |
| METEOROLOGICAL SITE<br>BRIDGEPORT | RATIO<br>DIR (DEG)<br>VEL (MPH)                           | 0.907<br>220<br>8.1                 | 0.367<br>220<br>6.8                 | 0.723<br>260<br>6.3                  | 0.909<br>230<br>15.90                                | 0.984<br>200<br>6.6                 | 0.281<br>160<br>3.1          | 0.759<br>130<br>1.6                 | 0.906<br>230<br>8.6  | 0.758<br>220<br>6.5           | 4.7<br>0.836<br>160<br>3.0   |
| METEOROLOGICAL SITE<br>WORCESTER  | SED (MFR)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SED (MPH) | 0.950<br>250<br>6.8                 | 0.922<br>260<br>8.6                 | 0.792<br>280<br>5.0                  | 0.772<br>220<br>8.4                                  | 0.896<br>230<br>5.7                 | 0.434<br>40<br>1.4           | 0.824<br>220<br>5.3                 | 9.1<br>0.948<br>9.1  | 0.964<br>8.0<br>8.0<br>8.0    | 0.548<br>220<br>7.2          |
|                                   | RATIO   | 0.817                               | 706.0                               | 0.674                                | 0.881  | 0.879                               | 0.165                        | 0.857                               | 9.3<br>0.977   | 8.2<br>0.977                  | 9.5<br>0.762                 |
| GROTON-008 (3982)                 | OZONE   | 0.184<br>8/11/05                    | 0.152                               | 0.150<br>7/20/0E                     | 0.141  | 0.137                               | 0.136                        | 0.135                               | 0.133  | 0.128                         | 0.124                        |
| METEOROLOGICAL SITE<br>NEWARK     | VEL (MPH)   | 0/ -4/0)<br>230<br>6.1              | 290<br>290<br>6.0                   | 9.1<br>9.1                           | 0/ 320<br>320<br>3.1                                 | 170<br>170<br>2.6                   | 210<br>210<br>9.5            | 240<br>240<br>8.4                   | 7/10/85<br>230<br>8.7  | 9/19/85<br>210<br>4.5         | 9/20/85<br>220<br>8.2        |
| METEOROLOGICAL SITE               | RATIO<br>DIR (DEG)  | 0.645<br>210                        | 0.609<br>290                        | 0.933<br>290                         | $ \begin{array}{c} 8.2 \\ 0.373 \\ 340 \end{array} $ | 0.395<br>190                        | 0.955<br>220                 | 8.9<br>0.939<br>210                 | 9.8<br>0.885<br>200  | 5.0<br>0.901<br>250           | 8.3<br>0.981<br>200          |
| BRADLEY                           | VEL (MPH)<br>SPD (MPH)                                    | 1.7<br>4.7                          | 4<br>9                              | 7.2                                  | 1.8  | 5.08                                | 6.9<br>7.6                   | 3.8<br>4.9                          | 7.9  | 0.00                          | 5.08<br>0.80                 |
| METEOROLOGICAL SITE<br>BRIDGEPORT | RATIO<br>DIR (DEG)<br>VEL (MPH)                           | 0.367<br>220<br>6.8                 | 0.723<br>260<br>6.3                 | 0.761<br>230<br>7.8                  | 0.457<br>210<br>5.7                                  | 0.759<br>130<br>4.6                 | 0.906<br>230<br>8.6          | 0.769<br>240<br>7.7                 | 0.821<br>210<br>5.6  | 0.419<br>220<br>4.5           | 0.758<br>220<br>6.5          |
|                                   | SPD (MPH)<br>RATIO  | 7.3<br>0.922                        | 7.9<br>0.792                        | 7.9<br>0.982                         | 6.3<br>0.907   | 5.6<br>0.824                        | $9.1 \\ 0.948$               | 7.9<br>0.978                        | 5.9<br>0.956   | 4.6<br>0 981                  | 6.8<br>0 061                 |
| METEOROLOGICAL SITE<br>WORCESTER  | DIR (DEG)<br>VEL (MPH)                                    | 260<br>8.6                          | 280                                 | 270<br>11.6                          | 270  | 5.3                                 | 240<br>9.1                   | 250<br>8.5                          | 220  | 270<br>6.9                    | 240<br>8.0                   |
|                                   | SPD (MPH)<br>RATIO  | $9.5 \\ 0.907$                      | 7.5<br>0.674                        | 11.8<br>0.983                        | 11.6<br>0.950  | 6.2<br>0.857                        | $9.3 \\ 0.977$               | 8.8<br>0.966                        | 7.8<br>0.989   | 7.5                           | 8.2<br>0.977                 |

TABLE 21, CONTINUED

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CT 1-HOUE AVEDACE ATOME

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## 1985 TEN HIGHEST 1-HOUR AVERAGE OZONE DAYS WITH WIND DATA

|  |   |   | -   |  |   |  |  |   | UNITS :  | PARTS PER   | MELLION   |  |
|--|---|---|---|--|---|--|--|---|--|---|---|--|
| TOWN/SITE (SAMPLES)  | RANK  | ٣   | 2   | ę  | 4   | Ĵ  | 9  | 7   | ω  | 6   | 10  |  |
| MADISON-002 (3883)<br>METEOROLOGICAL S<br>METEOROLOGICAL S<br>BRA<br>BRA<br>BRIDGE<br>BRIDGE<br>BRIDGE<br>BRIDGE<br>BRIDGE<br>BRIDGE | ITE DIR (DEC<br>MARK VEL (MP)<br>MARK VEL (MP)<br>RATIO<br>RATIO<br>ITE DIR (DEC<br>PORT VEL (MP)<br>RATIO<br>ITE DIR (DEC<br>PORT VEL (MP)<br>RATIO<br>ITE DIR (DEC<br>RATIO<br>ITE DIR (DEC<br>RATIO<br>RATIO<br>RATIO<br>RATIO<br>RATIO<br>RATIO<br>RATIO<br>RATIO | $\begin{array}{c} 0.204\\ 8/15/85\\ 11.0\\ 11.4\\ 1$ | 0.149<br>8/14/85<br>230<br>6.1<br>6.1<br>7.3<br>0.945<br>7.3<br>0.945<br>7.3<br>0.922<br>0.922<br>0.922<br>0.922<br>0.905<br>0.905  | 0.143<br>219/85<br>219/85<br>219/85<br>219/85<br>219/85<br>219/1<br>219/1<br>0.913<br>0.913<br>0.973                       | 0.135<br>290<br>290<br>6.0<br>6.0<br>6.0<br>4.4<br>4.4<br>7.23<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.774<br>0.774<br>0.775<br>0.775<br>0.777<br>0.7723<br>0.777<br>0.7723<br>0.777<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7723<br>0.7724<br>0.7723<br>0.7724<br>0.7724<br>0.7724<br>0.7724<br>0.7724<br>0.7724<br>0.7724<br>0.7724<br>0.7724<br>0.7774<br>0.7724<br>0.7724<br>0.7724<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.7774<br>0.77740<br>0.77740<br>0.77740<br>0.77740<br>0.77740<br>0.77740<br>0.77740<br>0.77740000000000 | 0.133<br>7/10/85<br>230<br>8.7<br>8.7<br>8.7<br>9.8<br>5.9<br>0.821<br>5.9<br>0.821<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.967<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.9666<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.966<br>0.9666<br>0.966<br>0.96 | $\begin{array}{c} 0.125\\ 6/378\\ 3.20\\ 3.20\\ 3.1\\ 3.1\\ 3.1\\ 3.1\\ 3.1\\ 3.1\\ 3.2\\ 0.373\\ 3.1\\ 1.8\\ 1.8\\ 1.8\\ 1.8\\ 0.457\\ 5.7\\ 0.457\\ 0.907\\ 1.1\\ 1.1\\ 1.1\\ 1.1\\ 1.1\\ 0.950$ | 0.125<br>7/20/85<br>250<br>9.1<br>9.1<br>9.1<br>7.2<br>0.933<br>7.2<br>0.933<br>7.5<br>7.5<br>7.5<br>7.6<br>7.6<br>7.8<br>7.8<br>7.8<br>7.8<br>7.8<br>7.8<br>7.8<br>7.8<br>7.8<br>7.8   | 0.124<br>6/22/85<br>190<br>8.5<br>0.942<br>150<br>0.989<br>150<br>0.554<br>0.554<br>0.555<br>0.857<br>0.857<br>0.857                       | $\begin{array}{c} 0.115 \\ 6/2/85 \\ 230 \\ 6.9 \\ 6.9 \\ 6.9 \\ 6.9 \\ 7.0 \\ $ | 0.114<br>7/9/85<br>2.6<br>0.395<br>0.759<br>0.759<br>0.759<br>0.759<br>0.759<br>0.759<br>0.857<br>0.857<br>0.857<br>0.857                                     |  |
| MIDDLETOWN-007 (4071)<br>METEOROLOGICAL 9<br>METEOROLOGICAL 9<br>BR/<br>BR/<br>BR/<br>BR/<br>BR/<br>BR/<br>BR/<br>BR/<br>BR/<br>BR/  | OZONE<br>ITE DIR (DEC<br>WARK VEL (MPI<br>SPD (MPI<br>RATIO<br>DLEY VEL (MPI<br>RATIO<br>ITE DIR (DEC<br>PORT VEL (MPI<br>RATIO<br>ITE DIR (DEC<br>STER VEL (MPI<br>RATIO<br>SPD (MPI<br>RATIO<br>STER VEL (MPI<br>RATIO  | 0.219<br>8/15/85<br>8/15/85<br>1) 11.0<br>11.4<br>0.968<br>1) 0.968<br>1.1<br>0.968<br>1) 0.968<br>1.1<br>0.950<br>10.950<br>10.950<br>10.813<br>0.813<br>0.813   | 0.153<br>8/14/85<br>230<br>6.1<br>0.645<br>1.7<br>1.7<br>1.7<br>1.7<br>220<br>250<br>0.922<br>260<br>8.6<br>8.6<br>8.6<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922 | 0.152<br>7/19/85<br>9.5<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.918<br>0.913<br>0.913<br>0.973 | 0.137<br>227/85<br>227/85<br>8.3<br>8.3<br>7.3<br>7.3<br>0.821<br>7.3<br>7.3<br>0.821<br>7.3<br>0.821<br>7.2<br>0.821<br>0.772<br>0.772<br>0.772<br>0.772<br>0.831<br>0.881   | 0.134<br>5/13/85<br>230<br>10.7<br>10.7<br>11.8<br>0.909<br>7.3<br>7.3<br>7.3<br>0.907<br>0.807<br>7.4<br>0.807<br>7.4<br>0.916<br>8.4<br>0.916<br>0.886<br>0.886  | 0.134<br>9/20/85<br>8.2<br>8.2<br>8.3<br>3.0<br>220<br>8.3<br>3.0<br>5.0<br>5.0<br>5.5<br>6.5<br>6.5<br>6.5<br>6.5<br>6.5<br>6.5<br>0.964<br>8.0<br>0.964<br>0.977<br>0.977  | 0.128<br>6/230<br>5.9<br>6.9<br>6.9<br>5.9<br>7.4<br>7.4<br>7.4<br>7.4<br>7.4<br>0.832<br>0.832<br>0.832<br>0.832<br>0.832<br>0.892<br>0.892<br>0.892<br>0.892<br>0.892<br>0.892<br>0.892<br>0.892<br>0.892<br>0.892<br>0.892<br>0.892<br>0.892<br>0.892<br>0.947 | $\begin{array}{c} 0.127\\ 5/11/85\\ 230\\ 230\\ 10.9\\ 11.2\\ 5.3\\ 5.3\\ 5.3\\ 220\\ 5.3\\ 7.1\\ 7.1\\ 7.1\\ 7.1\\ 7.1\\ 7.1\\ 7.1\\ 7.1$ | 0.127<br>230<br>8.7<br>8.7<br>8.7<br>8.7<br>5.6<br>7.7<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.958<br>0.958<br>0.958  | 0.127<br>7/9/85<br>2.6<br>0.395<br>0.395<br>0.395<br>0.395<br>0.395<br>0.395<br>0.395<br>0.395<br>0.395<br>0.395<br>0.359<br>0.759<br>0.852<br>0.852<br>0.852 |  |
| NEW HAVEN-123 (4088)<br>METEOROLOGICAL 3<br>NI<br>METEOROLOGICAL 3<br>BR/  | OZONE<br>DATE<br>DATE<br>DATE<br>DATE<br>DATE<br>MPI<br>MPI<br>MPI<br>MPI<br>MPI<br>MPI<br>MPI<br>MPI<br>MPI<br>MPI   | 0.181<br>8/15/85<br>11.12<br>11.4<br>11.4<br>11.4<br>11.4<br>0.968<br>5.9<br>11.4<br>0.968<br>0.968<br>0.968  | 0.149<br>7/19/85<br>210<br>9.5<br>0.955<br>220<br>220<br>6.9<br>0.906   | 0.139<br>8/14/85<br>2.30<br>6.1<br>9.5<br>0.645<br>2.10<br>2.10<br>1.7<br>0.367<br>0.367                                   | $\begin{array}{c} 0.138 \\ 6/22/85 \\ 190 \\ 8.5 \\ 9.1 \\ 0.942 \\ 5.1 \\ 5.1 \\ 0.989 \\ 0.989 \end{array}$   | 0.137<br>7/9/85<br>110<br>2.6<br>6.6<br>0.395<br>190<br>3.8<br>3.8<br>0.759  | 0.132<br>7/10/85<br>8.7<br>9.8<br>0.885<br>5.9<br>0.821<br>0.821   | 0.122<br>9/20/85<br>8.2<br>8.3<br>0.981<br>3.8<br>3.8<br>3.8<br>0.758<br>0.758  | 0.120<br>8/10/85<br>160<br>3.7<br>7.2<br>0.514<br>180<br>2.7<br>6.0<br>0.448   | 0,117<br>6/320<br>321<br>3.1<br>8.2<br>0.373<br>340<br>1.8<br>4.0<br>0.457  | 0.115<br>6/2/85<br>6/2/85<br>6.30<br>8.6<br>798<br>7.9<br>0.798<br>7.9<br>0.832<br>0.832  |  |
|  |   |   |   | (  |   |  |  |   |  | •   |   |  |

|            | MILLION   | 10                  | 230<br>7.4<br>8.2<br>8.2<br>240<br>10.2<br>10.2<br>10.2<br>0.947                             | 0.104<br>9/20/85<br>220<br>8.2<br>8.3<br>3.8<br>3.8<br>3.8<br>3.8<br>0.758<br>0.981<br>0.758<br>0.981<br>0.950<br>0.977<br>0.977   | 0.131<br>6/22/85<br>190<br>8.5<br>9.1<br>190<br>190<br>190<br>190<br>190<br>190<br>190<br>190<br>190<br>19  |
|------------|-----------|---------------------|--|--|---|
|            | PARTS PER | 6                   | 210<br>5.7<br>6.3<br>0.907<br>270<br>11.1<br>11.1<br>0.950                                   | $\begin{array}{c} 0.106\\ 7/ 9/85\\ 2.6\\ 0.395\\ 170\\ 3.8\\ 3.8\\ 3.8\\ 1.90\\ 1.30\\ 5.6\\ 0.759\\ 0.759\\ 0.759\\ 0.857\\ $  | 0.138<br>9/20/85<br>220<br>8.2<br>8.2<br>200<br>8.2<br>200<br>220<br>220<br>6.5<br>6.5<br>6.5<br>6.5<br>0.964<br>0.964<br>0.977   |
|            | UNITS :   | 8                   | 150<br>2.6<br>0.571<br>2.30<br>2.30<br>5.6<br>0.644  | 0.114<br>210/85<br>210/85<br>210/85<br>220<br>2220<br>2220<br>2220<br>2220<br>2220<br>2240<br>2240   | 0.145<br>6/3785<br>320<br>321<br>321<br>321<br>321<br>320<br>340<br>340<br>11.8<br>0.450<br>0.457<br>5.7<br>5.7<br>5.7<br>0.457<br>0.957<br>0.950   |
|            |           | 7                   | 220<br>6.5<br>6.8<br>740<br>240<br>8.0<br>8.0<br>8.0<br>8.0<br>8.0                           | 0.117<br>5/20/85<br>220<br>13.6<br>13.6<br>10.2<br>200<br>200<br>200<br>86.6<br>0.856<br>0.856<br>0.856<br>0.856<br>0.958<br>0.966<br>0.966  | 0.147<br>7/9/85<br>2.6<br>2.6<br>3.95<br>170<br>3.8<br>3.8<br>3.8<br>130<br>159<br>0.759<br>0.759<br>0.759<br>0.824<br>0.824<br>0.824<br>0.824<br>0.824   |
|            | WIND DATA | Q                   | 210<br>5.6<br>5.9<br>220<br>220<br>7.7<br>7.7<br>0.989                                       | $\begin{array}{c} 0.124 \\ 6/2/85 \\ 230 \\ 6.9 \\ 6.9 \\ 6.9 \\ 6.9 \\ 6.9 \\ 7.0 \\ $  | 0.153<br>250<br>250<br>9.1<br>250<br>9.1<br>250<br>255<br>255<br>255<br>255<br>255<br>255<br>256<br>255<br>256<br>256   |
|            | AYS WITH  | 5                   | 130<br>5.6<br>220<br>5.3<br>5.3<br>5.3<br>0.857  | 0.124<br>5/10/85<br>240<br>240<br>240<br>14.0<br>14.0<br>240<br>210<br>230<br>230<br>230<br>230<br>230<br>230<br>230<br>230<br>230<br>23   | 0.154<br>7/19/85<br>210<br>9.5<br>9.5<br>6.9<br>7.6<br>0.955<br>6.9<br>7.6<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.957<br>0.977  |
| ONT I NUED | E OZONE D | 11                  | 150<br>4.52<br>2564<br>2230<br>5.55<br>0.857   | 0.139<br>5/13/85<br>230<br>230<br>10.7<br>11.8<br>11.8<br>7.3<br>7.3<br>7.3<br>7.3<br>7.3<br>7.3<br>7.3<br>7.3<br>7.4<br>7.3<br>7.3<br>7.4<br>7.4<br>7.4<br>7.4<br>7.4<br>7.4<br>7.4<br>7.3<br>0.916<br>8.1<br>0.886<br>0.886  | 0.164<br>290<br>6.0<br>6.0<br>6.0<br>6.0<br>6.0<br>6.0<br>0.723<br>6.0<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.723<br>0.767<br>0.767<br>0.767<br>0.767<br>0.767<br>0.767<br>0.767<br>0.767<br>0.767<br>0.767<br>0.767<br>0.767<br>0.767<br>0.767<br>0.767<br>0.767<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777<br>0.777   |
| BLE 21, C  | UR AVERAG | ŝ                   | 220<br>6.3<br>0.922<br>260<br>8.6<br>9.5<br>0.907  | $\begin{array}{c} 0.142 \\ 5/11/85 \\ 230 \\ 10.9 \\ 11.2 \\ 11.2 \\ 5.1 \\ 5.1 \\ 5.1 \\ 5.1 \\ 5.1 \\ 5.1 \\ 5.1 \\ 5.1 \\ 7.$   | 0.168<br>7/10/85<br>8.7<br>8.7<br>8.7<br>9.8<br>7.2<br>0.885<br>7.2<br>0.885<br>7.2<br>0.956<br>0.956<br>0.956<br>0.956<br>0.989  |
| TA         | HEST 1-HO | 2                   | 230<br>8.6<br>9.1<br>0.948<br>240<br>9.1<br>9.1<br>0.977                                     | 0.158<br>5/27/85<br>220<br>8.3<br>8.3<br>10.1<br>220<br>220<br>230<br>230<br>230<br>230<br>220<br>8.4<br>0.772<br>220<br>8.4<br>0.772<br>0.831   | 0.168<br>8/14/85<br>230<br>6.1<br>6.1<br>6.1<br>1.7<br>1.7<br>1.7<br>1.7<br>1.7<br>1.7<br>1.7<br>0.367<br>0.367<br>0.367<br>0.367<br>0.367<br>0.367<br>0.367<br>0.367<br>0.322<br>0.922<br>0.922<br>0.922<br>0.907<br>0.907   |
|            | 5 TEN HIG | -                   | 220<br>8.1<br>8.1<br>0.955<br>250<br>6.8<br>0.813  | 0.15/85<br>8/15/85<br>220<br>11.4<br>0.968<br>5.5<br>0.955<br>0.955<br>0.955<br>0.955<br>0.855<br>0.855<br>0.855<br>0.817<br>0.817   | 0.189<br>0.189<br>0.15785<br>0.968<br>0.968<br>0.968<br>0.968<br>0.968<br>0.950<br>0.950<br>0.813<br>0.813  |
|            | 198       | RANK                | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>SATIO | OZONE<br>DATE<br>DATE<br>DIATE<br>DIATE<br>MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SPD (MPH)<br>CEG<br>DIATO<br>DIATO<br>DIATO<br>SPD (MPH)<br>RATIO<br>DIATO<br>CEG<br>NH)<br>SPD (MPH)<br>SPD (MPH)<br>CEG<br>NH)<br>SPD (MPH)<br>SPD | OZONE<br>DATE<br>DATE<br>DATE<br>DATE<br>DATE<br>NEC<br>MPH<br>SPD (MPH<br>SPD (MPH |
|            |           | TOWN/SITE (SAMPLES) | METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>WORCESTER                        | STAFFORD-001 (4110)<br>METEOROLOGICAL SITE<br>NEWARK<br>METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE  | STRATFORD-007 (3969)<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE  |

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### WIND ROSE FOR APRIL - SEPTEMBER 1984 BRADLEY INTERNATIONAL AIRPORT WINDSOR LOCKS, CONNECTICUT



### WIND ROSE FOR APRIL - SEPTEMBER 1985 BRADLEY INTERNATIONAL AIRPORT WINDSOR LOCKS, CONNECTICUT



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### WIND ROSE FOR APRIL - SEPTEMBER 1985 NEWARK INTERNATIONAL AIRPORT NEWARK, NEW JERSEY



### V. NITROGEN DIOXIDE

### **HEALTH EFFECTS**

Nitrogen dioxide (NO<sub>2</sub>) is a toxic gas with a characteristic pungent odor and a reddish-orangebrown color. It is highly oxidizing and extremely corrosive.

Nitrogen dioxide is not emitted into the atmosphere to any great extent by man-made sources. However, its presence in the atmosphere is accounted for by the photochemical oxidation of nitric oxide (NO), large amounts of which are emitted into the air by high temperature combustion processes. Industrial furnaces, power plants and motor vehicles are the primary sources of nitric oxide emissions.

Exposure to  $NO_2$  is believed to increase the risks of acute respiratory disease and susceptibility to chronic respiratory infection.  $NO_2$  also contributes to heart, lung, liver and kidney damage. At high concentrations, this pollutant can be fatal. At lower levels of 25 to 100 parts per million, it can cause acute bronchitis and pneumonia. Occasional exposure to low levels of  $NO_2$  can irritate the eyes and skin.

Other effects of nitrogen dioxide are its toxicity to vegetation and its ability to combine with water vapor to form nitric acid. Furthermore, NO<sub>2</sub> is an essential ingredient, along with hydrocarbons, in the formation of ozone.

### **CONCLUSIONS**

Nitrogen dioxide (NO<sub>2</sub>) concentrations at all monitoring sites did not violate the NAAQS for NO<sub>2</sub> in 1985. The annual arithmetic mean NO<sub>2</sub> concentration at each site was well below the federal standard of 100  $\mu$ g/m<sup>3</sup>.

### SAMPLE COLLECTION AND ANALYSIS

The DEP Air Monitoring Unit used continuous electronic analyzers employing the chemiluminescent reference method to continuously measure NO<sub>2</sub> levels. This was the fourth year this type of analyzer was used to measure NO<sub>2</sub> levels.

### **DISCUSSION OF DATA**

Monitoring Network - There were three nitrogen dioxide monitoring sites in 1985 (see Figure 11). The sites -- Bridgeport 123, East Hartford 003 and New Haven 123 -- were located in three urban areas in order to obtain data alongside ozone monitors.

**Precision and Accuracy** - Forty-two precision checks were made on the NO<sub>2</sub> monitors in 1985, yielding 95% probability limits ranging from -10% to + 10%. Accuracy is determined by introducing a known amount of NO<sub>2</sub> into each of the monitors. Five audits for accuracy were conducted on the monitoring network in 1985. Four different concentration levels were tested on each monitor: low, low/medium, medium/high and high. The 95% probability limits for the low level test ranged from -15% to + 12%; those for the low/medium level test ranged from the high level test ranged from -8% to + 2%.

Historical Data - The DEP's historical file of annual average nitrogen dioxide data from gas bubblers for 1973-1980 is available in the 1980 Air Quality Summary. Data from continuous electronic analyzers for the years 1981 and 1982 can be found in the 1983 Air Quality Summary. Data for 1983-1985 can be found in Table 22 below.

Annual Averages - The annual average NO<sub>2</sub> standard of 100  $\mu$ g/m<sup>3</sup> was not exceeded in 1985 at any site in Connecticut (see Table 22). In 1985, all three sites had sufficient data to compute valid arithmetic means. This permits comparisons with the 1983 and 1984 annual averages. The arithmetic mean NO<sub>2</sub> concentration at each site decreased between 1983 and 1985.

**Statistical Projections** - The format of Table 22 is the same as that used to present the TSP and sulfur dioxide data. However, Table 22 gives the annual arithmetic mean of the hourly  $NO_2$  concentrations in order to allow direct comparison to the annual  $NO_2$  standard. The 95% confidence limits about the arithmetic mean for each site demonstrate that it is unlikely that any site exceeded the primary annual standard of  $100 \,\mu\text{g/m}^3$  in 1985.

**10-High Days with Wind Data** - Table 23 presents for each site the ten days in 1985 when the highest hourly NO<sub>2</sub> readings occurred, along with the associated wind conditions for each day. (See the discussion of Table 11 in the TSP section for a description of the original use of the wind data.)

According to National Weather Service local climatological data recorded at Bradley Airport, 16 of the 23 days listed in the table had more then 50% of the possible sunshine. Of the seven remaining days, three followed days when the percent of possible sunshine exceeded 72%. This is interpreted to confirm the importance of photochemical oxidation in the formation of  $NO_2$ .

Six of the high  $NO_2$  days occurred at 2 or more of the sites, and four of these days had persistent winds out of the southwest quadrant. Persistent southwest winds were also characteristic of 63% of the days listed in Table 23.

Given the above observations and the fact that two of the three  $NO_2$  sites are located on the coast of Connecticut, it appears that a combination of pollutant transport and a high percent of possible sunshine (both of which occur on days with persistent southwest winds) tend to produce high  $NO_2$  levels in Connecticut.



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# 1983 - 1985 NITROGEN DIOXIDE ANNUAL AVERAGES AND STATISTICAL PROJECTIONS

| <u>Town Name</u> | Site | Year | Samples | Arithmetic<br><u>Mean</u> | 95-Perce<br><u>Lower</u> | nt-Limits<br><u>Upper</u> | Standard<br>Deviation |
|------------------|------|------|---------|---------------------------|--------------------------|---------------------------|-----------------------|
| Bridgeport       | 123  | 1983 | 8328    | 56.4                      | 56.2                     | 56.6                      | 34.7                  |
| Bridgeport       | 123  | 1984 | 8689    | 51.5                      | 51.4                     | 51.6                      | 29.7                  |
| Bridgeport       | 123  | 1985 | 8602    | 50.3                      | 50.2                     | 50.4                      | 26.8                  |
| East Hartford    | 003  | 1983 | 8576    | 43.5                      | 43.4                     | 43.6                      | 31.3                  |
| East Hartford    | 003  | 1984 | 8172    | 39.8                      | 39.6                     | 40.0                      | 26.2                  |
| East Hartford    | 003  | 1985 | 8461    | 39.6                      | 39.5                     | 39.7                      | 23.3                  |
| New Haven        | 123  | 1983 | 7971    | 62.8                      | 62.7                     | 62.9                      | 13.5                  |
| New Haven        | 123  | 1984 | 8530    | 58.2                      | 58.1                     | 58.3                      | 29.0                  |
| New Haven        | 123  | 1985 | 8566    | 57.6                      | 57.5                     | 57.7                      | 26.6                  |
|                  |      |      |         |                           |                          |                           | •                     |

N.B. The arithmetic mean and standard deviation have units of  $\mu g/m^3$ .

| MITLION   | 10                  | 0.083<br>8/10/85<br>3.7<br>3.7<br>0.514<br>0.514<br>0.514<br>0.514<br>0.571<br>0.571<br>0.571<br>0.571<br>0.544<br>0.516<br>0.516<br>0.576<br>0.576<br>0.514   | 0.065<br>9/20/85<br>8.3<br>0.981<br>3.08<br>3.00<br>5.5<br>0.981<br>0.964<br>8.0<br>8.0<br>0.977<br>0.977   | 0.084<br>3/28/85<br>11.9<br>0.942<br>250<br>250<br>11.2<br>0.784  |
|---|---------------------|--|---|---|
| UNITS : PARTS PER                                       | 6                   | 0.084<br>+4/21/85<br>+160<br>+1.4<br>+170<br>+170<br>5.6<br>0.797<br>90<br>5.8<br>0.355<br>1.9<br>0.365<br>1.9<br>0.220<br>0.220   | $ \begin{array}{c}                                     $  | 0.087<br>12/24/85<br>2.5<br>3.2<br>0.789<br>1.6<br>5.6<br>0.296   |
|   | ω                   | 0.084<br>3/27/85<br>220<br>10.5<br>10.9<br>5.8<br>220<br>220<br>220<br>220<br>220<br>220<br>220<br>220<br>220<br>22  | $\begin{array}{c} 0.066\\ 10/9/85\\ 230\\ 230\\ 10.8\\ 0.976\\ 0.962\\ 0.952\\ 0.952\\ 12.8\\ 0.986\\ 0.986\\ 0.952\\ 0.986\\$  | 0.088<br>4/19/85<br>260<br>8.4<br>11.4<br>0.735<br>340<br>340<br>340<br>4.5<br>0.717                                    |
| 1985 TEN HIGHEST 1-HOUR AVERAGE NO2 DAYS WITH WIND DATA | 2                   | 0.085<br>8/15/85<br>230<br>230<br>5.50<br>5.59<br>0.968<br>5.50<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955<br>0.811<br>0.813   | 0.066<br>3/19/85<br>2.20<br>11.2<br>0.613<br>2.20<br>11.2<br>2.20<br>11.2<br>2.20<br>2.20<br>2.250<br>2.20<br>2.20<br>0.745<br>2.20<br>0.745<br>2.20<br>0.745<br>2.20<br>0.745<br>2.20<br>0.745<br>2.20<br>0.745<br>2.20<br>0.766<br>0.766<br>0.717<br>2.20<br>0.716<br>0.666<br>0.717<br>2.20<br>0.666<br>0.717<br>2.20<br>0.666<br>0.666<br>0.667<br>0.667<br>0.667<br>0.667<br>0.667<br>0.667<br>0.667<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.673<br>0.770<br>0.673<br>0.770<br>0.673<br>0.770<br>0.673<br>0.770<br>0.673<br>0.770<br>0.770<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.750<br>0.7500<br>0.7500<br>0.7500<br>0.7500<br>0.7500<br>0.7500<br>0.7500<br>0.7500<br>0.7500<br>0.7500<br>0.750000000000   | 0.088<br>4/16/85<br>7.2<br>0.686<br>4.7<br>0.686<br>4.7<br>0.780  |
|   | 9                   | 0.085<br>240<br>13.0<br>13.7<br>0.955<br>5.30<br>2.40<br>2.53<br>0.978<br>0.978<br>0.978<br>0.978<br>0.955<br>0.978<br>0.955<br>0.955<br>0.955<br>0.955<br>0.955   | 0.23/85<br>5.9<br>0.613<br>0.613<br>0.480<br>0.480<br>0.480<br>0.480<br>0.480<br>0.480<br>0.480<br>5.24<br>0.866<br>70<br>1.3<br>0.247<br>0.247   | 0.088<br>7/13/85<br>4.2<br>0.652<br>0.652<br>0.652<br>0.652<br>0.506<br>0.506   |
|   | ŝ                   | $ \begin{array}{c}  & 0.087 \\  & 4/25/85 \\  & 5.4 \\  & 5.4 \\  & 5.604 \\  & 230 \\  & 230 \\  & 230 \\  & 230 \\  & 230 \\  & 250 \\  & 250 \\  & 11.0 \\  & 11.0 \\  & 0.955 \\$  | 0.069<br>12/24/85<br>124/85<br>2.55<br>0.789<br>1.40<br>0.7296<br>1.40<br>0.7296<br>1.40<br>0.7398<br>0.3398<br>0.3388<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.838<br>0.8388<br>0.838<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.83888<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.8388<br>0.83888<br>0.8388<br>0.8388<br>0.8388<br>0.83888<br>0.8388<br>0.8388<br>0.83888<br>0.83888<br>0.8388<br>0.8388<br>0.83888<br>0.83888<br>0.83888<br>0.83888<br>0.83888<br>0.83888<br>0.83888<br>0.83888<br>0.83888<br>0.83888<br>0.83888<br>0.83888<br>0.83888<br>0.83888<br>0.83888<br>0.838888<br>0.83888<br>0.8388888<br>0.83888<br>0.83888<br>0.8388888<br>0.83888<br>0.8388888<br>0.83888<br>0.8388888<br>0.83888<br>0.838888<br>0.838888<br>0.838888<br>0.8388888<br>0.838888<br>0.83888888<br>0.8388888888<br>0.8388888888<br>0.838888888<br>0.838888888888  | 0.092<br>9/20/85<br>8.2<br>8.3<br>0.981<br>3.00<br>3.00<br>3.00<br>3.00<br>3.00<br>3.00<br>3.00<br>3.0                  |
|   | ħ                   | 0.088<br>3.22<br>3.25<br>0.335<br>0.335<br>0.335<br>0.335<br>0.335<br>0.341<br>0.280<br>0.341<br>0.341<br>0.341<br>0.341<br>0.341<br>0.341<br>0.341<br>0.341<br>0.341<br>0.341<br>0.341<br>0.341<br>0.341<br>0.341<br>0.341<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.345<br>0.250<br>0.345<br>0.250<br>0.250<br>0.250<br>0.250<br>0.250<br>0.250<br>0.250<br>0.250<br>0.250<br>0.250<br>0.275<br>0.250<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.275<br>0.2750<br>0.2750<br>0.2750<br>0.2750<br>0.2750<br>0.2 | 0.070<br>3/11/85<br>4.2<br>1.1280<br>1.1280<br>1.128<br>0.655<br>1.10<br>1.10<br>1.10<br>1.10<br>1.10<br>1.10<br>1.10<br>1.   | 0.096<br>9/21/85<br>8.4<br>8.9<br>0.939<br>0.939<br>0.769<br>0.769  |
|   | £                   | 0.090<br>6/18/85<br>9.1<br>9.1<br>9.1<br>9.1<br>9.1<br>9.1<br>9.1<br>9.1<br>0.989<br>0.989<br>0.989<br>0.946<br>0.946<br>0.946<br>0.950<br>0.950   | $\begin{array}{c} 0.070\\ 2/5/85\\ 7.9\\ 7.9\\ 8.9\\ 3.6\\ 3.6\\ 3.6\\ 3.6\\ 11.5\\ 11.5\\ 11.5\\ 0.712\\ 3.6\\ 0.8\\ 0.712\\ 0.712\\ 0.712\\ 0.712\\ 0.712\\ 0.73\\ 0.73\\ 0.73\\ 0.138\\ 0.13$  | 0.102<br>9/19/85<br>4.5<br>0.50<br>0.2901<br>250<br>250<br>0.419  |
|   | N                   | $\begin{array}{c} 0.097\\ 9/2/85\\ 230\\ 230\\ 6.4\\ 6.4\\ 6.4\\ 7.9\\ 7.9\\ 7.1\\ 7.1\\ 7.1\\ 7.1\\ 7.1\\ 7.1\\ 7.1\\ 7.1$  | 0.074<br>3/27/85<br>220<br>10.9<br>10.9<br>10.9<br>10.9<br>220<br>0.966<br>0.993<br>0.966<br>0.966<br>0.993<br>0.966<br>0.993<br>0.966<br>0.993<br>0.966<br>0.993<br>0.966<br>0.966<br>0.793<br>0.793<br>0.793<br>0.740<br>0.993<br>0.966<br>0.740<br>0.993<br>0.966<br>0.740<br>0.993<br>0.996<br>0.993<br>0.996<br>0.993<br>0.996<br>0.993<br>0.996<br>0.993<br>0.993<br>0.996<br>0.993<br>0.996<br>0.993<br>0.996<br>0.993<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.9966<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.996<br>0.9966<br>0.996<br>0.996<br>0.996<br>0.90 | 0.104<br>5/1/85<br>300<br>3.2<br>9.6<br>0.335<br>5.4<br>7.5<br>0.717  |
|   | -                   | 0.104<br>4/16/85<br>300<br>7.2<br>10.5<br>0.686<br>4.7<br>4.7<br>7.1<br>11.1<br>0.639<br>2200<br>2270<br>270<br>270<br>270<br>270<br>270<br>270<br>270<br>1111<br>1111   | 0.080<br>0.080<br>1.10<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>1.50<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0.981<br>0  | $\begin{array}{c} 0.112\\ 3/27/85\\ 10.5\\ 10.9\\ 0.961\\ 5.8\\ 5.8\\ 0.993\\ 0.993\end{array}$                         |
|   | RANK                | NO2<br>DATE<br>DATE<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (M   | NOZ<br>DATE<br>DATE<br>VEL (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>SP  | NO2<br>DATE<br>DATE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>SPD (MPH) |
|   | TOWN-SITE (SAMPLES) | BRIDGE PORT-123 (8602)<br>METEOROLOGICAL SITE<br>NEWARK<br>METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE   | EAST HARTFORD-003 (8461)<br>METEOROLOGICAL SITE<br>NEWARK<br>METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE  | NEW HAVEN-123 (8566)<br>METEOROLOGICAL SITE<br>NEWARK<br>METEOROLOGICAL SITE<br>BRADLEY                                 |

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TABLE 23

-134-
| PER MILLION | 10                  | 230<br>8.8<br>9.5<br>0.929<br>14.6<br>174.6<br>0.959   |
|-------------|---------------------|--|
| PARTS 1     | 6                   | 140<br>2.0<br>3.398<br>190<br>5.6<br>8.3<br>0.833  |
| UNITS       | <b>60</b>           | 180<br>3.1<br>7.2<br>7.2<br>3.1<br>3.0<br>300<br>15.6<br>0.534                                   |
|             | 7                   | 270<br>7.1<br>11.1<br>0.639<br>280<br>280<br>8.0<br>8.0<br>0.726                                 |
|             | 9                   | 200<br>3.7<br>5.3<br>0.698<br>6.0<br>6.3<br>0.942  |
|             | 5                   | 220<br>6.5<br>6.5<br>6.8<br>0.964<br>8.0<br>8.0<br>8.0<br>8.2<br>0.977                           |
| AGE NUZ U   | 4                   | 240<br>7.7<br>7.9<br>7.9<br>7.9<br>7.9<br>0.978<br>8.5<br>8.5<br>0.966                           |
| HOUK AVEK   | ,Ω                  | 0.981<br>0.981<br>0.917<br>0.917<br>0.917  |
| II GHEST 1- | 2                   | 280<br>2.9<br>8.6<br>0.341<br>9.5<br>11.9<br>0.793   |
| 35 TEN H    | -                   | 220<br>8.5<br>8.5<br>8.5<br>0.966<br>7.2<br>9.1<br>0.798   |
| 198         | RANK                | DIR (DEG)<br>r Vel (MPH)<br>spd (MPH)<br>RATIO<br>DIR (DEG)<br>R Vel (MPH)<br>SPD (MPH)<br>RATIO |
|             | TOWN-SITE (SAMPLES) | METEOROLOGICAL SITE<br>BRIDGEPOR'<br>METEOROLOGICAL SITE<br>WORCESTEI                            |

TABLE 23, CONTINUED

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1985 TEN HIGHEST 1-HOUR AVERAGE NO2 DAYS WITH WIND DATA

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### VI. CARBON MONOXIDE

### HEALTH EFFECTS

Carbon monoxide (CO) is a colorless, odorless, poison gas formed when carbon-containing fuel is not burned completely. It is by far the most plentiful air pollutant. Fortunately, this deadly gas does not persist in the atmosphere. It is apparently converted by natural processes to harmless carbon dioxide in ways not yet understood, and this is done quickly enough to prevent any general buildup. However, CO can reach dangerous levels in local areas, such as city-street canyons with heavy auto traffic and little wind.

Clinical experience with accidental CO poisoning has shown clearly how it affects the body. When the gas is breathed, CO replaces oxygen in the red blood cells, reducing the amount of oxygen that can reach the body cells and maintain life. Lack of oxygen affects the brain, and the first symptoms are impaired perception and thinking. Reflexes are slowed, judgement weakened, and drowsiness ensues. An auto driver breathing high levels of CO is more likely to have an accident; an athlete's performance and skill drop suddenly. Lack of oxygen then affects the heart. Death can come from heart failure or general asphyxiation, if a person is exposed to very high levels of CO.

### **CONCLUSIONS**

The eight-hour National Ambient Air Quality Standard of 9 parts per million (ppm) was exceeded at three of the five carbon monoxide monitoring sites in Connecticut during 1985. The standard was exceeded two times at Stamford 020, six times at Hartford 017 and once at Bridgeport 004. No exceedance of the 35 ppm one-hour standard was measured at any site in 1985.

In order to put the monitoring data into proper perspective, it must be realized that carbon monoxide concentrations vary greatly from place-to-place. More than 95% of the CO emissions in Connecticut come from motor vehicles. Therefore, concentrations are greatest in areas of traffic congestion. The magnitude and frequency of high concentrations observed at any monitoring site are not necessarily indicative of widespread CO levels.

The CO standards are likely to be exceeded in any city in the state where there are areas of traffic congestion. However, as Connecticut's SIP control strategies are implemented, there should continue to be a decrease in the number of congested areas. Also, as federally - mandated controls which reduce emissions from new motor vehicles are implemented, a reduction in ambient CO levels should be achieved.

Unlike SO<sub>2</sub>, TSP and O<sub>3</sub>, elevated CO levels are not often associated with southwesterly winds, indicating that this pollutant is more of a local-scale (not regional-scale) problem.

### METHOD OF MEASUREMENT

The DEP Air Monitoring Unit uses instruments employing a non-dispersive infrared technique to continuously measure carbon monoxide levels. The instantaneous concentrations are recorded on strip charts from which hourly averages are extracted. Due to the relative inertness of CO, a long sampling line can be used without the danger of CO being depleted by chemical reactions within the lines. The most important consideration in the measurement of CO is the placement of the sampling probe inlet; that is, its proximity to traffic lanes.

### **DISCUSSION OF DATA**

**Monitoring Network** - The network in 1985 consisted of five carbon monoxide monitors: Bridgeport 004, Hartford 017, New Britain 002, New Haven 007, and Stamford 020. They are all located in urban areas. All sites are located west of the Connecticut River, with three of them in coastal towns (see Figure 12). Hartford 017 is a relatively new site and has been in existence for only two years.

**Precision and Accuracy** - The carbon monoxide monitors had a total of 141 precision checks during 1985. The resulting 95% probability limits were -9% to +9%. Accuracy is determined by introducing a known amount of CO into each of the monitors. Six audits for accuracy were conducted on the monitoring network in 1985. Three different concentration levels were tested on each monitor: low, medium and high. The 95% probability limits for the low level test ranged from -4% to + 12%; for the medium level test ranged from -4% to + 4%; and for the high level test ranged from -1% to + 2%.

- HARTFORD 047 AND STAMFERTS 020

8-Hour and 1-Hour Averages - Hartford 017 and Stamford 020 had second high CO concentrations exceeding the 8-hour standard of 9 ppm, which means that the standard was violated at these sites in 1985 (see Table 24). In 1984, both sites also recorded violations of the standard. Regarding the maximum 8-hour running average at each site, there were decreases from 1984 to 1985 at Hartford, New Britain and Stamford. Increases occurred at Bridgeport and New Haven. The second highest values were higher in 1985 than in 1984 at Hartford and New Haven and lower at Bridgeport, New Britain and Stamford.

As for 1-hour averages, no site in the state recorded a value exceeding the primary 1-hour standard of 35 ppm. Only Stamford 020 recorded a maximum 1-hour value greater than the year before. Second high 1-hour values were lower at all the sites.

The maximum and second high CO concentrations at each site are presented in Table 24. Table 25 presents monthly highs and a monthly tally of the number of times the standards were exceeded at each site. Seasonal variations in CO levels can be observed using this table.

**10-High Days with Wind Data -** Table 26 lists for each site the ten days in 1985 when the 1-hour CO averages were highest. The wind data associated with these high readings are also presented. (See the discussion of Table 11 in the TSP section for a description of the origin and use of these wind data.)

The high CO levels tended to occur during the colder months at all five CO sites. Low atmospheric mixing heights and stable atmospheric conditions are two reasons CO levels are high during the fall and winter. Also, cold starts and warmups (rich mixtures) contribute to an increase in CO. A noteworthy feature of the high CO days is that the persistence of a wind is more important than the direction to which or from which it is blowing. Since 95% of the CO emissions in Connecticut come from motor vehicles, it is likely that the high CO levels are caused when persistent winds are blowing CO emissions from the direction of nearby roads toward the monitors.

Trends - Due to the local nature of CO emissions, it is not appropriate to give an estimate of widespread CO trends. However, local CO trends can be addressed in a number of ways. Exceedances of the 8-hour standard can be tracked in order to determine if a CO problem is worsening or abating at a site. This is illustrated in Table 26a and in Figure 13. One can see that over the past five years the number of exceedances has dropped significantly at the Stamford site and has remained low and relatively unchanged at the Bridgeport, New Britain and New Haven sites. The Hartford-017 site has been in existence for only two years. Little can be said about the trend at this site. Therefore, it is included in Table 26a but not in Figure 13. The Stamford-020 site is excluded from Figure 13 because the range of the number of exceedances is too large to illustrate satisfactorily.

Another way of illustrating local CO trends is to use running averages. Running averages have the advantage of smoothing out the abrupt, transitory changes in pollutant levels that are often evident in consecutive sampling periods and from one season to the next. Figure 14 shows the 36-month running average of the hourly CO concentrations at four sites. The Hartford-017 site is not included due to the lack of sufficient data. CO levels seem to be remaining steady at all the sites except Stamford-020, where a downward trend is apparent.



## **1985 CARBON MONOXIDE STANDARDS ASSESSMENT SUMMARY**

| W High  |                |              |                 |               |              |
|---|----------------|--------------|-----------------|---------------|--------------|
| TIME OF<br>MAXIMUM<br>1-HOUR<br>AVERAGE2                    | 11/19/9        | 12/24/14     | 12/24/11        | 12/24/1       | 1/28/2       |
| 2ND HIGH<br>1-HOUR<br>AVERAGE                               | 11.7           | 16.9         | 10.7            | 9.2           | 15.5         |
| TIME OF<br>MAXIMUM<br>1-HOUR<br>AVERAGE2                    | 12/23/23       | 1/14/18      | 12/24/10        | 7/15/9        | 1/14/19      |
| MAXIMUM<br>1-HOUR<br><u>AVERAGE</u>                         | 12.2           | 20.9         | 12.0            | 13.2          | 20.0         |
| TIME OF<br>2ND HIGH<br>8-HOUR<br>RUNNING<br>AVERAGE1        | 1/14/22        | 12/24/15     | 2/1/18          | 1/14/23       | 12/24/1      |
| 2ND HIGH<br>8-HOUR<br>RUNNING<br>AVERAGE                    | 7.2            | 11.9         | 6.5             | 6.7           | 6.9          |
| TIME OF<br>MAXIMUM<br>8-HOUR<br>RUNNING<br><u>AVERAGE</u> 1 | 12/24/1        | 1/14/24      | 12/1/24         | 12/24/1       | 1/14/22      |
| MAXIMUM<br>8-HOUR<br>RUNNING<br>AVERAGE                     | 9.2            | 12.2         | 7.0             | 7.7           | 10.2         |
| TOWN-SITE   | Bridgeport-004 | Hartford-017 | New Britain-002 | New Haven-007 | Stamford-020 |

<sup>1</sup> The time of the 8-hour average is reported as follows: month/day/hour (EST), specifying the end of the 8-hour period. <sup>2</sup> The time of the 1-hour average is reported as follows: month/day/hour (EST), specifying the end of the 1-hour period.

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N.B. The CO averages are expressed in terms of parts per million (ppm).

### **1985 CARBON MONOXIDE SEASONAL FEATURES**

| TOWN-SITE       |                              | IAN  | FEB      | MAR  | APR  | MAY  | NNr | <u>IUL</u> | AUG | SEP  | OCT     | NON  | DEC    |
|-----------------|------------------------------|------|----------|------|------|------|-----|------------|-----|------|---------|------|--------|
| Bridgeport-004  | Max. 1-Hour                  | 11.1 | 7.7      | 7.0  | 5.8  | 4.9  | 2.6 | 4.1        | 5.0 | 7.7  | 9.0     | 11.7 | 12.2   |
|                 | Max. Running<br>8-Hour       | 7.2  | 5.0      | 4.4  | 3.9  | 3.9  | 2.2 | 3.1        | 3.1 | 4.4  | 4.4     | 6.3  | 9.2    |
|                 | No. of 8-Hour<br>Exceedances | 0    | 0        | 0    | 0    | 0    | 0   | 0          | 0   | 0    | 0       | 0    | 0<br>1 |
| Hartford-017    | Max. 1-Hour                  | 20.9 | 16.6     | 10.9 | 11.1 | 11.1 | 5.9 | 11.6       | 9.4 | 11.0 | 13.3    | 13.1 | 16.9   |
|                 | Max. Running<br>8-Hour       | 12.2 | 9.4      | 8.4  | 7.5  | 5.3  | 4.5 | 6.6        | 7.2 | 7.8  | 8.2     | 7.6  | 11.9   |
|                 | No. of 8-Hour<br>Exceedances | ۳    | 4        | 0    | 0    | 0    | 0   | 0          | Ö   | 0    | 0       | 0    | ব      |
| New Britain-002 | Max. 1-Hour                  | 9.5  | 9.8<br>8 | 9.9  | 5.4  | 4.8  | 5.0 | 7.8        | 7.4 | 8.4  | 7.6     | 9.6  | 12.0   |
|                 | Max. Kunning<br>8-Hour       | 6.4  | 6.5      | 4.8  | 4.2  | 3.6  | 3.6 | 5.7        | 5.1 | 4.4  | 5.3     | 7.0  | 6.5    |
|                 | No. of 8-Hour<br>Exceedances | 0    | 0        | 0    | 0    | 0    | 0   | 0          | 0   | 0    | 0       | 0    | 0      |
| New Haven-007   | Max. 1-Hour                  | 8.7  | 7.3      | 6.8  | 6.4  | 4.1  | 4.8 | 13.2       | 5.1 | 6.3  | Q.<br>Q | 9.0  | 9.2    |
|                 | Max. Kunning<br>8-Hour       | 6.7  | 3.8      | 4.0  | 3.0  | 2.7  | 2.8 | 2.7        | 3.7 | 3.3  | 4.1     | 5.0  | 7.7    |
|                 | No. of 8-Hour<br>Exceedances | 0    | 0        | 0    | 0    | 0    | 0   | 0          | 0   | 0    | 0       | 0    | 0      |
| Stamford-020    | Max. 1-Hour                  | 20.0 | 15.0     | 8.0  | 8.3  | 5.3  | 6.2 | 4.8        | 7.6 | 7.4  | 9.8     | 11.8 | 12.3   |
|                 | Max. Running<br>8-Hour       | 10.2 | 6.6      | 5.9  | 4.3  | 3.7  | 4.1 | 3.8        | 4.2 | 4.7  | 5.2     | 7.3  | 9.3    |
|                 | No. of 8-Hour<br>Exceedances | *    | 0        | 0    | 0    | 0    | 0   | 0          | 0   | 0    | 0       | 0    | 4      |

N.B. The CO concentrations are in terms of parts per million (ppm).

| WILLION    | 10                  | 9/30/85<br>210<br>8.4<br>0.972<br>5.2<br>0.972<br>0.972<br>0.972<br>0.998<br>0.974<br>0.974  | 14.1<br>14.1<br>230<br>3.30<br>3.20<br>1.9<br>1.9<br>0.693<br>0.693<br>0.693<br>0.693<br>0.693<br>0.693<br>0.891<br>0.891   | 1/7/85<br>40<br>2.8<br>6.6<br>0.417<br>10<br>6.8<br>6.8<br>6.8<br>0.910  |
|------------|---------------------|--|---|--|
| PARTS PEF  | 6                   | 2/2/85<br>3300<br>3300<br>3443<br>5.40<br>3443<br>5.40<br>3443<br>5.40<br>3443<br>5.40<br>3443<br>5.40<br>3443<br>5.6<br>320<br>320<br>5.6<br>0.966<br>0.960<br>0.960<br>0.960   | $\begin{array}{c} 14.1\\ 1/11/85\\ 350\\ 350\\ 350\\ 350\\ 350\\ 340\\ 340\\ 340\\ 340\\ 330\\ 330\\ 0.932\\ 330\\ 0.932\\ 0.93$  | 9/30/85<br>210<br>210<br>8.4<br>0.972<br>5.2<br>5.2<br>0.905   |
| UNITS :    | ø                   | $\begin{array}{c} 11 \\ 1 \\ 1 \\ 1 \\ 5 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 $  | 2, 14.4<br>2, 5/85<br>4, 60<br>3.6<br>3.6<br>3.6<br>3.6<br>3.6<br>3.6<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.712<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733<br>0.733  | 2/ 1/85<br>2/ 1/85<br>20<br>10.8<br>0.996<br>5.9<br>5.9<br>0.981   |
|            | 7                   | 10/1/85<br>210<br>5.9<br>7.2<br>7.2<br>7.2<br>7.2<br>7.2<br>7.2<br>7.2<br>7.2<br>0.956<br>7.1<br>0.956<br>7.37<br>0.973<br>0.973<br>0.973  | 14.4<br>1/17/85<br>6.4<br>6.4<br>6.4<br>6.4<br>7.89<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.366<br>0.3666<br>0.366<br>0.366<br>0.3666<br>0.366<br>0.3660 | $\begin{array}{c} & & \\$ |
| VIND DATA  | 9                   | 0.9.0<br>210/18/85<br>0.8.5<br>0.8.5<br>0.808<br>0.916<br>0.815<br>0.815<br>0.916<br>0.916<br>0.916<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950<br>0.950  | 14.4<br>300<br>6.8<br>6.8<br>6.8<br>6.8<br>3.23<br>3.23<br>3.23<br>3.23<br>3.23<br>3.23<br>3.23<br>3.   | 9.5<br>1/2/85<br>3.30<br>8.6<br>9.6<br>0.827<br>350<br>5.2<br>0.971  |
| AYS WITH V | 5                   | 11/18/85<br>5.3<br>5.3<br>0.643<br>7.3<br>0.643<br>2.50<br>0.443<br>7.3<br>0.643<br>7.3<br>0.643<br>7.3<br>0.643<br>7.3<br>0.622<br>0.622<br>0.622<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.956<br>0.622<br>0.622<br>0.622<br>0.622<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.662<br>0.6620 | 12/23/85<br>12/23/85<br>6.4<br>6.4<br>6.4<br>6.9<br>6.9<br>6.9<br>6.9<br>6.9<br>0.972<br>0.972<br>0.972<br>0.972<br>0.972<br>0.972<br>0.972<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.989<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.999<br>0.  | 2/15/85<br>2/15/85<br>9.4<br>9.9<br>9.4<br>0.946<br>5.5<br>5.5<br>0.889  |
| RAGE CO DI | 4                   | $\begin{array}{c} 12.24.85\\ 12.24.85\\ 1.90\\ 2.5\\ 0.789\\ 1.7\\ 1.7\\ 1.7\\ 1.40\\ 2.6\\ 0.398\\ 0.398\\ 0.398\\ 0.398\\ 0.833\\ 0$   | $\begin{array}{c} 16.4\\ 2/11/85\\ 50\\ 6.9\\ 1.7\\ 1.7\\ 1.7\\ 1.7\\ 1.7\\ 1.7\\ 1.7\\ 1.7$  | 9.6<br>250<br>5.3<br>8.2<br>8.2<br>0.643<br>4.5<br>4.5<br>4.5<br>0.956   |
| HOUR AVE   | £                   | 11.1.1<br>240<br>240<br>8.0<br>8.0<br>8.0<br>8.1<br>0.81<br>0.80<br>250<br>0.81<br>0.857<br>0.857<br>0.857<br>0.857<br>0.857   | 2/ 4/85<br>280<br>280<br>280<br>280<br>280<br>280<br>280<br>250<br>250<br>250<br>250<br>250<br>290<br>290<br>290<br>290<br>290<br>290<br>290<br>290<br>290<br>29  | 2/ 5/85<br>2/ 5/85<br>7.9<br>8.9<br>0.884<br>2.6<br>3.6<br>0.712   |
| HIGHEST 1- | N                   | 11/19.7<br>21/19.85<br>21/19.85<br>4.00<br>4.00<br>4.00<br>2.200<br>2.20<br>2.20<br>2.20<br>2.20<br>2.20<br>2.20<br>2.20<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.922<br>0.9   | $\begin{array}{c} 16.9\\ 124/85\\ 190\\ 2.5\\ 0.789\\ 1.7\\ 1.40\\ 2.6\\ 1.40\\ 1.40\\ 1.40\\ 1.40\\ 1.90\\ 0.838\\ 0.$   | 9.9<br>3/11/85<br>4.2<br>4.2<br>6.5<br>7.6<br>7.6<br>7.8<br>0.978  |
| 985 TEN F  | -                   | 12.2     12.2     12.2     190     0.932     0.93     0.932  | 20.9<br>1/14/85<br>240<br>8.8<br>8.8<br>8.8<br>8.8<br>0.911<br>250<br>250<br>250<br>250<br>0.814<br>8.9<br>0.851<br>0.857<br>0.857<br>0.857   | 12.0<br>12/24/85<br>2.5<br>3.2<br>0.789<br>1.7<br>5.6<br>0.296   |
| -          | RANK                | CO<br>DATE<br>DATE<br>DIR (DEG)<br>SPD (MPH)<br>SPD (MPH)  | CO<br>DATE<br>DATE<br>DATE<br>DIR (DEG)<br>SPD (MPH)<br>SPD (MPH  | CO<br>DATE<br>DATE<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO<br>RATIO  |
|            | TOWN-SITE (SAMPLES) | BRIDGEPORT-004 (8673)<br>METEOROLOGICAL SITE<br>NEWARK<br>METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>BRIDGEPORT<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE  | HARTFORD-017 (8127)<br>METEOROLOGICAL SITE<br>NEWARK<br>METEOROLOGICAL SITE<br>BRADLEY<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE   | NEW BRITAIN-002 (7883)<br>METEOROLOGICAL SITE<br>NEWARK<br>METEOROLOGICAL SITE<br>BRADLEY  |

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| PER MILLION | 10                  | 40<br>1.1.1<br>0.870<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70<br>70   | 285-10/5/85-10/5/85<br>210/5/85<br>210/5/85<br>0.225<br>0.225<br>0.225<br>0.210<br>210<br>210<br>210<br>210<br>210<br>210<br>210<br>210<br>210  | 88<br>85<br>11/ 50<br>88<br>11/ 50<br>88<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7<br>10.7 |
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| UNITS       | œ                   | 20<br>8.8<br>9.2<br>60<br>60<br>5.0<br>0.972<br>0.974<br>0.974   | 85 1/ 1/2<br>360/<br>1.00<br>0.55380<br>0.55380<br>0.55380<br>0.55380<br>0.420<br>0.4200<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.4530<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.45300<br>0.453000<br>0.45300<br>0.453000<br>0.453000<br>0.453000<br>0.45300000000000000000000000000000000000   | 85 1/24/9<br>2500<br>2247<br>2247<br>0.2847<br>0.2847<br>0.2847<br>12.190<br>0.987<br>0.987<br>11.42<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.987<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.997<br>0.99   |
| TA          | 7                   | 40<br>5.8<br>6.67<br>0.677<br>30<br>30<br>4.6<br>0.864   | 85 11 7.3<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>10.10.7<br>1 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| H WIND DA   | 9                   | 330<br>8.1<br>0.806<br>330<br>330<br>7.2<br>0.847  | 85 2/4/3<br>280/2<br>7.4<br>7.4<br>7.4<br>7.4<br>0.9255<br>0.9555<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0.9218<br>0 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| VERAGE CO   | 4                   | 250<br>3.50<br>250<br>250<br>250<br>0.9547   | 85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>85<br>1/11/1<br>1/11/1<br>85<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1<br>1/11/1 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                   |
| F 1-HOUR A  | ε                   | 0.0375<br>0.11.5<br>0.0900<br>0.13.50<br>0.13.50   |   |  |
| EN HIGHESI  | N                   | 0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.633<br>0.6330<br>0.6330<br>0.6330<br>0.6330<br>0.6330<br>0.6330<br>0.6330<br>0.6330<br>0.6330000000000 | 222<br>222<br>222<br>222<br>222<br>222<br>222<br>222  |  |
| 1985 T.     | -                   | MPH) 2-14<br>MPH) 5-14<br>MPH) 5-1<br>0.339<br>DEG) 19<br>MPH) 5-1<br>0.833<br>0.833   | 7715           DEG         7715           MPH         6.           MPH         6.           MPH         7.   | 20.<br>1/24.<br>0EG) 224.<br>21.24.<br>21.24.<br>21.24.<br>21.24.<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5<br>22.5        |
|             | RANK                | E DIR (<br>R VEL (<br>RATIO<br>RATIO<br>ER VEL (<br>RATIO<br>RATIO   | CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>C   | E DIR CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>C  |
|             | TOWN-SITE (SAMPLES) | METEOROLOGICAL SITE<br>BRIDGEPOF<br>METEOROLOGICAL SITE<br>WORCESTE  | NEW HAVEN-007 (8698)<br>METEOROLOGICAL SITE<br>NEWAF<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE<br>METEOROLOGICAL SITE   | STAMFORD-020 (8697)<br>METEOROLOGICAL SITE<br>NEWAF<br>METEOROLOGICAL SITE<br>BRADLI<br>BRADLI<br>BRIDGEPOF<br>BRIDGEPOF<br>METEOROLOGICAL SITE  |

TABLE 26, CONTINUED

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1985 TEN HIGHEST 1-HOUR AVERAGE CO DAYS WITH WIND DATA

| 4       5       6       7       8       7       8 $12/24/85$ $11/18/85$ $10/12/26$ $210/8/85$ $10/12/18/85$ $10/12/85$ <td< th=""><th>3       4       5       6       7       8       7       8         111.1       11.18       10.8       9.1       9.0       8.7       8       7       8       7       8       7       8       7       8       7       8       7       7       8       7</th><th>2       3       4       5       6       7       8       4         111.7       111.1       10.8       9.1       9.0       8.7       8.4       7         111.7       111.1       10.8       9.1       9.0       8.7       8.4       7         111.7       111.1       10.8       9.1       9.0       8.7       8.4       7         210       240       190       2.5       5.3       6.8       5.9       10.7       7.4         200       240       1.7       8.4       5.9       10.7       7.4       4.5       7.4         200       240       1.7       8.2       5.3       6.8       7.4       4.5       7.4         200       240       190       290       0.643       0.803       0.803       0.803       0.803       0.803       0.803       0.803       0.803       0.805       0.916       &lt;</th><th>1         2         3         4         5         6         7         8           12/23/85         111/19/85         11/14/85         12/24/85         11/18/85         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14</th></td<> | 3       4       5       6       7       8       7       8         111.1       11.18       10.8       9.1       9.0       8.7       8       7       8       7       8       7       8       7       8       7       8       7       7       8       7  | 2       3       4       5       6       7       8       4         111.7       111.1       10.8       9.1       9.0       8.7       8.4       7         111.7       111.1       10.8       9.1       9.0       8.7       8.4       7         111.7       111.1       10.8       9.1       9.0       8.7       8.4       7         210       240       190       2.5       5.3       6.8       5.9       10.7       7.4         200       240       1.7       8.4       5.9       10.7       7.4       4.5       7.4         200       240       1.7       8.2       5.3       6.8       7.4       4.5       7.4         200       240       190       290       0.643       0.803       0.803       0.803       0.803       0.803       0.803       0.803       0.803       0.805       0.916       <  | 1         2         3         4         5         6         7         8           12/23/85         111/19/85         11/14/85         12/24/85         11/18/85         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14/15         11/14 |
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| 4<br>12/24/85<br>12/24/85<br>190<br>190<br>11/0<br>5.6<br>0.789<br>1.7<br>1.7<br>1.7<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.789<br>0.799<br>0.799<br>0.799<br>0.799<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.790<br>0.700<br>0.700<br>0.700<br>0.700<br>0.700<br>0.700<br>0.700<br>0.700000000  | 3 4<br>11.1<br>11.1<br>1.14/85<br>240<br>8.8<br>240<br>1.14/85<br>1.14/85<br>240<br>1.17<br>1.17<br>1.17<br>1.250<br>1.17<br>1.250<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.10<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1.17<br>1 | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$   | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$   |
|   | 2/4/85<br>2/48<br>2/40<br>2/40<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8240<br>0.8270<br>0.8270<br>0.8240<br>0.8270<br>0.8240<br>0.8270<br>0.8270<br>0.8270<br>0.8240<br>0.8270<br>0.8240<br>0.8270<br>0.8240<br>0.8270<br>0.8240<br>0.8270<br>0.8270<br>0.8240<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.8270<br>0.82700<br>0.82700<br>0.82700<br>0.82700<br>0.82700<br>0.82700<br>0.82700<br>0.82700<br>0.82700<br>0.82700000000000000000000000000000000000   | $\begin{array}{cccccccccccccccccccccccccccccccccccc$  | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$   |
| RANK     1     2       CO     12.2     11.7       DATE     12.23/85     11/19/85       DATE     12/23/85     11/19/85       DIR     DEG     190     210       VEL     MPH)     6.4     4.0       VEL     MPH)     6.4     4.6       VEL     MPH)     6.4     4.6       VEL     MPH)     6.4     4.6       VEL     MPH)     6.9     9.2       VEL     MPH)     6.9     4.4       VEL     MPH)     6.9     4.4       VEL     MPH)     6.9     4.4       VEL     MPH)     6.9     4.4       VEL     MPH)     0.932     0.933       VEL     MPH)     9.2     5.1       RATIO     0.972     0.992     230       VEL     MPH     10.4     11.7       SPD     MPH     10.5     11.4       RATIO     0.922     220     220       VEL     MPH     10.4     11.7       RATIO     0.989     0.992     220       VEL     MPH     10.5     114/85       RATIO     0.989     0.992       VEL     MPH     8.0     2.5<   | RANK 1<br>CO<br>DATE<br>DATE<br>DATE<br>DATE<br>DATE<br>DATE<br>DATE<br>DATE<br>DATE<br>DATE<br>DATE<br>DATE<br>DATE<br>DATE<br>CO<br>RATIO<br>DIR (DEG)<br>DIR (DEG)<br>DIR (DEG)<br>CO<br>RATIO<br>DIR (DEG)<br>DIR (DEG)<br>CO<br>RATIO<br>DIR (DEG)<br>CO<br>CO<br>RATIO<br>DIR (DEG)<br>CO<br>CO<br>RATIO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>CO<br>C   | RANK<br>CO<br>DATE<br>DIATE<br>DIATE<br>DIATE<br>DIATE<br>DIATE<br>DIATE<br>MPH)<br>SPD (MPH)<br>SPD (MPH)<br>SP |   |

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TABLE 26, CONTINUED

1985 TEN HIGHEST 1-HOUR AVERAGE CO DAYS WITH WIND DATA

|          |                                   | 191  | 85 ien HI         |                               |                             |                            |                        |                            |                           | UNITS : I                 | PARTS PER                   | MILLION                    |
|----------|-----------------------------------|--|-------------------|-------------------------------|-----------------------------|----------------------------|------------------------|----------------------------|---------------------------|---------------------------|-----------------------------|----------------------------|
| TOWN-S   | SITE (SAMPLES)                    | RANK   | ~                 | N                             | ω.                          | 4                          | ъ                      | 9                          | 7                         | Ø                         | 6                           | 10                         |
| alan     | 4ETEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)          | 140<br>2.0<br>308 | 110<br>4.6<br>7.3<br>633      | 60<br>11.5<br>11.8<br>0 070 | 250<br>3.0<br>4.9          | 260<br>9.5<br>10.4     | 330<br>6.5<br>8.1<br>0.806 | 40<br>5.8<br>8.6<br>0.671 | 20<br>8.8<br>9.2<br>0.952 | 220<br>6.2<br>0.898         | 40<br>9.6<br>11.1<br>0.870 |
| <u> </u> | METEOROLOGICAL SITE<br>WORCESTER  | VEL (MPH)<br>VEL (MPH)<br>SPD (MPH)<br>RATIO | 0.833<br>0.833    | 0.240<br>9.0<br>10.8<br>0.834 | 0.138                       | 260<br>4.6<br>0.964        | 8.2<br>8.5<br>0.971    | 0.847                      | 30<br>4.0<br>4.6<br>0.864 | 5.0<br>5.2<br>0.974       | 230<br>9.9<br>10.2<br>0.974 | 70<br>7.9<br>8.1<br>0.985  |
| NEW HJ   | 4VEN-007 (8698)                   | CO   | 13.2<br>7/15/85 1 | 9.2<br>12/24/85               | 9.0<br>11/19/85             | 8.7<br>1/14/85             | 8.5<br>12/23/85        | 7.3<br>2/ 4/85             | 7.3<br>11/ 1/85           | 7.2<br>1/ 4/85            | 7.0<br>12/31/85             | 6.8<br>10/ 1/85            |
| -        | METEOROLOGICAL SITE<br>NEWARK     | VEL (MPH)                                    | 190<br>6.3<br>7.6 | 2.5                           | 210<br>4.0                  | 240<br>8.0<br>8.8          | 190<br>6.4<br>7.0      | 280<br>7.4                 | 50<br>10.7<br>11.8        | 360<br>7.2<br>8.1         | 210<br>9.5<br>10.2          | 7.90                       |
|          | METEOROLOGICAL SITE               | RATIO<br>DIR (DEG)                           | 0.831             | 0.789<br>190                  | 0.605                       | 0.911<br>240<br>3.9        | 0.909<br>190<br>6.4    | 0.907<br>320<br>4.3        | $0.909 \\ 20 \\ 4.5$      | 0.896<br>10<br>1.0        | 0.930<br>190<br>9.0         | 0.825<br>200<br>7.4        |
|          | BRAULET                           | SPD (MPH)<br>RATIO                           | 10.2<br>0.970     | 5.6<br>0.296                  | 4.9<br>0.938                | 4.9<br>0.803               | 0.932                  | 0.665                      | 4.7<br>0.939              | 1.9<br>0.558              | 9.2<br>0.983                | 7.6<br>0.966               |
|          | METEOROLOGICAL SITE<br>BRIDGEPORT | DIR (DEG)<br>VEL (MPH)<br>SPD (MPH)          | 200<br>7.4        | 140<br>2.0<br>5.0             | 5.2<br>5.2                  | 250<br>6.3<br>7.5          | 250<br>9.50            | 5.50<br>6.6                | 8.8<br>6 8 0              | 2.0<br>7.1                | 12.0                        | 10-10<br>10-10             |
|          | METEOROLOGICAL SITE<br>MORCESTER  | RATIO<br>DIR (DEG)<br>VFI (MPH)              | 0.951<br>220      | 0,398<br>190<br>5,6           | 0.992<br>220<br>11.7        | 0.844<br>270<br>6.9        | 0.972<br>230<br>10.4   | 0.765<br>290<br>7.1        | 0.671<br>30<br>4.0        | 0.420<br>250<br>1.9       | 0.925<br>210<br>15.5        | 0.737<br>210<br>8.0        |
|          |                                   | SPD (MPH)<br>RATIO                           | 13.4              | 6.8<br>0.833                  | 11.8<br>0.992               | $8.1 \\ 0.857$             | 10.5<br>0.989          | 7.8<br>0.921               | 4.6<br>0.864              | 4.0<br>0.463              | 15.5<br>0.996               | 8.2<br>0.973               |
| STAMF    | ORD-020 (8697)                    | co   | 20.0              | 17.1                          | 15.0                        | 12.3                       | 11.8                   | 10.6                       | 10.2<br>12/20/265         | 9.9<br>17211785           | 9.8<br>10/18/85             | 9.5                        |
|          | METEOROLOGICAL SITE               | DATE<br>DIR (DEG)                            | 1/14/85<br>240    | 1/28/85<br>300                | 2/11/85<br>50<br>1, 3       | 12/23/85<br>190<br>6 11    | 11/10/07<br>250<br>5_3 | 210                        | 15/54/07                  | 250                       | 210<br>210<br>6.8           | 10.7                       |
|          | NEWAR                             | SPD (MPH)<br>SPD (MPH)<br>RATIO              | 8.8<br>0.911      | 0.723<br>0.723                | 6.9<br>0.627                | 7.0                        | 8.2<br>0.643           | 6.6<br>0.605               | 3.2<br>0.789              | 12.7<br>0.947             | 8.5<br>0.808                | 11.8<br>0.909              |
|          | METEOROLOGICAL SITE<br>BRADLEY    | DIR (DEG)<br>VEL (MPH)                       | 3.9               | 320                           | 350                         | 61<br>6.4<br>7             | 290<br>4.5             | 200<br>4.6                 | 190<br>7.7                | 220<br>4.7<br>0           | 190<br>6.3<br>6.9           | 4.50<br>4.75               |
|          |                                   | SPD (MPH)<br>RATIO                           | 0.803             | 3.3<br>0.983                  | 3.7<br>0.461                | 0.932                      | 4.7<br>0.956<br>250    | 0.938                      | 0.296                     | 0.786                     | 0.916<br>220                | 0.939                      |
|          | METEOROLOGICAL SITE<br>BRIDGEPORI | VEL (MPH)<br>SPD (MPH)                       | 7.5<br>2          | 500<br>6.0                    | 5.9<br>6.9                  | ,<br>0<br>0<br>0<br>0<br>0 |                        | 5.0                        | 2.0                       | 11.0                      | 7.0                         | 5.8<br>8.6<br>8.6          |
|          |                                   | RATIO  | 0.844             | 0.813                         | 0.859                       | 0.972                      | 0.622                  | 0.992                      | 0.398<br>190              | 0.987<br>290              | 0.815<br>210                | 0.6/1<br>30                |
|          | METEOROLOGICAL SIIE<br>WORCESTEF  | VEL (MPH)                                    | 6.9               | 0.00                          | 0.00                        | 10.4                       | -0,-                   | 11.7                       | 2.0                       | 11.9                      | 10.1<br>10.6                | 4.0<br>4.6                 |
|          |                                   | SPD (MPH)<br>RATIO                           | 8.1<br>0.857      | 0.945                         | 0.181                       | 0.989                      | 0.964                  | 0.992                      | 0.833                     | 0.982                     | 0.950                       | 0.864                      |

### TABLE 26a

### **EXCEEDANCES OF THE 8-HOUR CO STANDARD**

| SITE            | <u>1981</u> | <u>1982</u> | <u>1983</u>    | <u>1984</u> | <u>1985</u> |
|-----------------|-------------|-------------|----------------|-------------|-------------|
| Bridgeport-004  | 0           | 0           | 1              | 0           | 20          |
| Hartford-017    | -           | -           | -              | 227         | <b>6</b> 5  |
| New Britain-002 | 1           | 22          | 2              | 0           | 0           |
| New Haven-007   | 70          | 0           | 1              | ()a         | 0           |
| Stamford-020    | 113b        | 2c          | 1 <sup>d</sup> | 32          | 21          |

<sup>a</sup> Data is missing from January through September.
 <sup>b</sup> Data is missing from October through December.
 <sup>c</sup> A local road was changed from 2-way traffic to 1-way traffic.

d 90% of the data is missing for November and December.

### FIGURE 13

### **EXCEEDANCES OF THE 8-HOUR CO STANDARD**

### SITE: BRIDGEPORT-004



YEAR

### FIGURE 13, CONTINUED

### **EXCEEDANCES OF THE 8-HOUR CO STANDARD**

### SITE: NEW BRITAIN-002



YEAR

### FIGURE 13, CONTINUED

### **EXCEEDANCES OF THE 8-HOUR CO STANDARD**

### SITE: NEW HAVEN-007



YEAR

FIGURE 14

# 36-MONTH RUNNING AVERAGES OF THE HOURLY CO CONCENTRATIONS

SITE: BRIDGEPORT-004



FIGURE 14, CONTINUED

# 36-MONTH RUNNING AVERAGES OF THE HOURLY CO CONCENTRATIONS

SITE: NEW BRITAIN-002



FIGURE 14, CONTINUED

# 36-MONTH RUNNING AVERAGES OF THE HOURLY CO CONCENTRATIONS

SITE: NEW HAVEN-007



FIGURE 14, CONTINUED

# 36-MONTH RUNNING AVERAGES OF THE HOURLY CO CONCENTRATIONS

SITE: STAMFORD-020



### VII. LEAD

### HEALTH EFFECTS

Lead (Pb) is a soft, dull gray, odorless and tasteless heavy metal. It is a ubiquitous element that is widely distributed in small amounts, particularly in soil and in all living things. Although the metallic form of lead is reactive and rarely occurs in nature, lead is prevalent in the environment in the form of various inorganic compounds, and occasional concentrated deposits of lead compounds occur in the earth's crust.

The presence of lead in the atmosphere is primarily accounted for by the emissions of lead compounds from man-made processes, such as the extraction and processing of metallic ores, the incineration of solid wastes, and the operation of motor vehicles. The combustion of lead-containing gasoline by motor vehicles is the largest source of airborne lead emissions and is responsible for approximately 73% of the national total in 1985. These emissions are in the form of fine-to-course particulate matter and are comprised of lead sulfate, ammonium lead halides, and lead halides, of which the chief component is lead bromochloride. The halide compounds appear to undergo chemical changes over a period of hours and are converted to lead carbonate, oxide and oxycarbonate.

The most important sources of lead in humans and other animals are ingestion of foods and beverages, inhalation of airborne lead, and the eating of non-food substances. From the standpoint of the general population, the intake of lead into the body is primarily through ingestion. The direct intake of lead from the ambient air is relatively small. Except in special cases, the contribution to the total body burden of lead via inhalation of airborne lead in urban areas is usually less than 30%. In non-urban areas, it is usually less than 5%.

Overexposure to lead in the United States is primarily a problem in children. Age, pica, diet, nutritional status, and multiple sources of exposure serve to increase the risk of lead poisoning in children. This is especially true in the inner cities where the prevalence of lead poisoning is greatest. Overexposure to lead compounds may result in undesirable biologic effects. These effects range from reversible clinical or metabolic symptoms that disappear after cessation of exposure to permanent damage or death from a single extreme dose or prolonged overexposure. Clinical lead poisoning is accompanied by symptoms of intestinal cramps, peripheral nerve paralysis, anemia, and severe fatigue. Very severe exposure results in permanent neurological, renal, or cardiovascular damage or death.

### CONCLUSIONS

The Connecticut primary and secondary ambient air quality standard for lead and its compounds was not exceeded at any site in Connecticut during 1985.

The monitoring sites where the lead levels were highest were generally in urban locations with moderate to heavy traffic. This is due to the fact that in Connecticut the primary source of lead to the atmosphere is the combustion of leaded gasoline in motor vehicles.

A downward trend in measured concentrations of lead has been observed since 1978. This is probably due to the increasing use of unleaded gasoline. Figure A shows that the decrease in lead emissions from gasoline combustion from 1975 to 1985 has been commensurate with a decrease in statewide ambient average lead concentrations. In fact, this relationship is so close, it has a correlation coefficient of 0.977 (see Figure B). Regarding Figures A and B, the reader should note that after 1978 and again after 1981 a change occurred in the way in which lead concentrations were determined.

Before 1979, lead concentrations were determined by analysis of quarterly composite samples from existing TSP monitors. From 1979 through 1981, lead concentrations were determined by analysis of individual daily samples from existing TSP monitors. Beginning in 1982, lead concentrations were determined by analysis of monthly composite samples from only approved lead monitors. Both the single sample and monthly composite data points are depicted in Figure A for 1982. The discontinued method gives a lower average lead concentration in 1982 than the new method. The higher average lead concentration is used in Figure B.

### SAMPLE COLLECTION AND ANALYSIS

The Air Monitoring Unit uses hi-vol and lo-vol samplers to obtain ambient concentrations of lead. These samplers are used to collect particulate matter onto fiberglass filters. The particulate matter collected on the filters is subsequently analyzed for its chemical composition. Wet chemistry techniques are used to separate the particulate matter into various components. The lead content of the TSP is determined using an atomic absorption spectrophotometer. (The use of these sampling devices and the chemical analysis techniques were fully described in the TSP section.) Unlike hi-vol TSP samples which are analyzed separately, the hi-vol lead sample is a composite of all the individual samples obtained at a site in a single month. That is, a cutting is taken from each filter during the month and these cuttings are collectively chemically analyzed for lead.

### **DISCUSSION OF DATA**

Monitoring Network - In 1985, both hi-vol and lo-vol samplers were operated in Connecticut to monitor lead levels (see Figure 15). There were 15 hi-vol sites and 7 lo-vol sites operated throughout the State (see Table 35) as part of the State and Local Air Monitoring Stations (SLAMS) network. The DEP operated the seven lo-vol monitors in areas with populations of 200,000 or more. They are Hartford 015 and 016, Stamford 022, New Haven 016 and 018, West Haven 003, and Bridgeport 010. These "micro-scale" lead sites are situated near some of the busiest city streets in order to monitor "worst-case" lead concentrations. EPA approval for these lo-vol monitors was granted in February, 1984.

Precision and Accuracy - The hi-vol lead monitors had a total of 27 precision checks in 1985. The resulting 95% probability limits were -8% to +6%. Accuracy for lead is defined as the accuracy of the analysis method. It is determined by chemical analysis of known lead samples. There were 21 audits for accuracy conducted on the monitoring network in 1985. Two different concentration levels were tested: low and high. The 95% probability limits for the low level test ranged from -10% to +5%; those for the high level test ranged from -8% to +5%.

**NAAQS** - Connecticut's ambient air quality standard for lead and its compounds, measured as elemental lead, is: 1.5 micrograms per cubic meter ( $\mu$ g/m<sup>3</sup>), maximum arithmetic mean averaged over three consecutive calendar months. This standard was enacted on November 2, 1981. Previously, Connecticut's lead standard was substantially identical: 1.5  $\mu$ g/m<sup>3</sup> for a calendar quarter-year average. The change to a 3-month running average means that a more stringent standard now applies, since there are three times as many data blocks within a calendar year which must be below the limiting concentration of 1.5  $\mu$ g/m<sup>3</sup>.

**3-Month Running Averages -** Three-month running average lead concentrations are given in Table 27 for the year 1985. These values are also presented in graphical form in Figure 16 for the period 1983-85. The New Haven-018 site lacked sufficient data and is not included in Table 27 or Figure 16.

**Trends** - As was mentioned above, airborne concentrations of lead have been trending steadily downward. This was demonstrated on a statewide level in Figure A. The trend in lead levels can also be shown on a regional or a site-specific basis. Figure C shows the trend in annual average lead

concentrations at each of seven monitoring sites that have been in existence long enough to be able to demonstrate a long term trend. Figure D shows the trends in the 3-year running average lead concentrations at the same seven sites. A downward trend in lead levels is apparent at all the sites, especially since 1978. This decrease in lead levels is commensurate with the decrease in lead emissions from gasoline combustion.

FIGURE A

(\_\_\_\_\_\_)

## STATEWIDE ANNUAL LEAD EMISSIONS FROM GASOLINE

AND

## STATEWIDE ANNUAL AVERAGE LEAD CONCENTRATIONS



and the second

FIGUREB

### **STATEWIDE ANNUAL LEAD EMISSIONS FROM GASOLINE**

VS.

## STATEWIDE ANNUAL AVERAGE LEAD CONCENTRATIONS





| 27     |
|--------|
| Ш      |
| ŝ      |
| $\leq$ |
| 8      |

1985 3-MONTH RUNNING AVERAGE LEAD CONCENTRATIONS

| 0.32 0.3<br>0.42 0.3 | 0            | õ            | 0.21         | 0.16         | 0.14         | 0.12         | 0.11         | 0.10         | 0.10         | 0.10 | 0.11 |
|----------------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|------|------|
| 0.44                 | 0.35<br>0.32 | 0.30<br>0.29 | 0.21<br>0.25 | 0.16<br>0.20 | 0.14<br>0.19 | 0.12<br>0.15 | 0.11<br>0.13 | 0.10<br>0.13 | 0.10<br>0.13 | 0.10 | 0.11 |
| 01.0                 | 0.42         | 0.34         | 0.34         | 0.29         | 0.25         | 0.22         | 0.21         | 0.19         | 0.18         | 0.18 |      |
| 0.40                 | 0.42         | 0.37         | 0.35         | 0.31         | 0.26         | 0.22         | 0.17         | 0.17         | 0.16         | 0.15 | 0.14 |
| 0.24                 | 0.23         | 0.20         | 0.17         | 0.14         | 0.11         | 0.10         | 0.09         | 0.09         | 0.09         | 0.09 | 0.09 |
| 0.31                 | 0.28         | 0.24         | 0.18         | 0.15         | 0.12         | 0.10         | 0.09         | 0.10         | 0.10         | 0.10 | 0.09 |
| 0.49                 | 0.42         | 0.32         | 0.24         | 0.21         | 0.18         | 0.15         | 0.13         | 0.13         | 0.15         | 0.14 | 0.14 |
| 0.61                 | 0.57         | 0.42         | 0.32         | 0.29         | 0.25         | 0.22         | 0.21         | 0.22         | 0.24         | 0.24 | 0.21 |
| 0.65                 | 0.61         | 0.42         | 0.39         | 0.30         | 0.31         | 0.29         | 0.28         | 0.27         | 0.27         | 0.26 | 0.25 |
| 0.46                 | 0.35         | 0.30         | 0.22         | 0.21         | 0.17         | 0.14         | 0.11         | 0.12         | 0.14         | 0.12 | 0.11 |
| 0.34                 | 0.32         | 0.26         | 0.21         | 0.19         | 0.20         | 0.15         |              | 0.13         | 0.13         | 0.13 | 0.12 |
| 0.31                 | 0.25         | 0.20         | 0.16         | 0.16         | 0.14         | 0.12         | 0.10         | 0.10         | 0.10         | 0.09 | 0.08 |
| 0.44                 | 0.46         | 0.39         | 0.37         | 0.30         |              |              |              | 0.21         |              | 8    |      |
| 0.48                 | 0.43         | 0.45         | 0.43         | 0.41         | 0.27         | 0.22         | 0.17         | 0.16         |              |      |      |
| 0.34                 | 0.28         | 0.25         | 0.19         | 0.18         | 0.15         | 0.14         | 0.13         | 0.14         | 0.14         | 0.12 | 0.10 |
| 0.25                 | 0.22         | 0.21         |              | 0.18         | 0.19         | 0.17         | 0.16         | 0.14         | 0.13         | 0.10 | 0.09 |
| 0.35                 | 0.31         | 0.29         | 0.30         | 0.25         | 0.24         | 0.21         | 0.25         |              |              |      | 0.15 |
| 0.43                 | 0.33         | 0.27         | 0.20         | 0.19         | 0.16         | 0.13         | 0.12         | 0.11         | 0.12         | 0.10 | 0.10 |
| 0.56                 | 0.44         | 0.40         | 0.31         | 0.26         | 0.21         | 0.19         | 0.17         | 0.17         | 0.16         | 0.17 | 0.17 |
| 0.72                 | 0.59         | 0.50         | 0.39         | 0.36         | 0.30         | 0.26         | 0.22         | 0.24         | 0.24         | 0.23 | 0.20 |
|                      |              |              |              |              | ****         |              | 4<br>        | 0.25         | 0.24         | 0.23 | 0.21 |



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|     |            |   |             |        |   |        |         |              |       |            |               |   | MONTH          | YEAR           |  |
|-----|------------|---|-------------|--------|---|--------|---------|--------------|-------|------------|---------------|---|----------------|----------------|--|
|     |            |   |             |        |   |        |         |              |       |            |               | * |                |                |  |
|     |            |   |             |        |   |        |         |              |       |            |               | * * * * *                               | k I ∞<br>k I ∞ | <br> <br> <br> |  |
|     |            |   |             |        |   |        |         |              |       |            |               | * * * * *                               | ##<br>-    -   | 5              |  |
|     |            |   |             |        |   |        |         |              |       |            | *<br>*        | * * * *                                 | e i 9          | !              |  |
|     |            |   |             |        |   |        |         |              |       |            | * *           | * * * * *                               |                | i              |  |
|     |            |   |             |        |   |        |         |              |       |            | * * *         | * * * * *                               |                |                |  |
|     |            |   |             |        |   |        |         |              |       |            | * * *         | * * * * *                               | k i m          |                |  |
|     |            |   |             |        |   |        |         |              |       |            | * * * *       | : * * * :<br>: * * * :                  | ≠ i ∩<br>¥     |                |  |
|     |            |   |             |        |   |        |         |              |       | 7<br>7     | * * * * *     | * * * * :                               | * i ~-<br>* i  | <u>i</u>       |  |
|     | AD         |   |             | İ      |   |        |         |              |       | * *        | * * * * *     | : * * * :<br>: * * * :                  | 101            | -              |  |
|     | ΓĒ         |   |             |        |   |        |         |              |       | 2          | * * * * *     | : * * * * :<br>: * * * * :              | *   -          |                |  |
| ED  | F0R<br>010 | , |             | ł      |   |        |         |              |       | 7          | * * * * *     | : * * * :<br>: * * * :                  | * <b> </b> 0   |                |  |
| INN | ES<br>RT   |   |             | ļ      |   |        |         |              |       |            | * * * *       | : * * * :<br>: * * * :                  | *   o          |                |  |
| ONT | RAG<br>EPO |   |             |        |   |        |         |              |       | * *        | * * * * *     | : * * * :<br>: * * * :                  | *   œ          | ł              |  |
| 0   | AVE        |   |             |        |   |        |         |              |       | 7<br>2     | * * * * *     | : * * * :<br>: * * * :                  | *   ~          | 34             |  |
| 16  | NG<br>=BR  |   |             |        |   |        |         |              |       | 2          | * * * * *     | : * * * :<br>: * * * :                  | * 0            | :              |  |
| URE | I NN I     |   |             |        |   |        |         |              |       |            | * * *         | : * * * :<br>: * * * :                  | * i ^          | Ì              |  |
| FIG | H RL       |   |             |        |   |        |         |              |       |            |               |   | i =            |                |  |
|     | ILNO       | • |             | į      |   |        |         |              |       |            |               |   | iπ             |                |  |
|     | 3 - MC     |   |             | İ      |   |        |         |              |       |            |               |   |                | 1              |  |
|     |            |   |             | Ì      |   |        |         |              |       |            |               |   |                | <u> </u>       |  |
|     |            |   |             |        |   |        |         |              |       |            |               |   | 12             |                |  |
|     |            |   |             |        |   |        |         |              |       |            |               |   | 11             |                |  |
|     |            |   |             |        |   |        |         |              |       |            |               |   | 10             |                |  |
|     |            |   |             |        |   |        |         |              |       |            |               |   | 6              |                |  |
|     |            |   |             |        |   |        |         |              |       |            |               |   | 0              | 1              |  |
|     |            |   |             |        |   |        |         |              |       | :          | * * * * * * * | * * * *                                 | *   ~          | 33             |  |
|     |            |   |             | 1      |   |        |         |              |       | :          | * * * * * *   | * * * *                                 | * 0            | , w            |  |
|     |            |   |             |        |   |        |         |              |       |            | * * *         | * * * *                                 | * <b>ເ</b> ທ   | 1              |  |
|     |            |   |             |        |   |        |         |              |       |            | * * * *       | * * * *                                 | *   =          |                |  |
|     |            |   |             |        |   |        |         |              |       |            | * * * *       | * * * *                                 | * i ~          |                |  |
|     |            |   |             |        |   |        |         |              |       | * :<br>* : | * * * * * *   | * * * *                                 | * i ∾<br>*     |                |  |
|     |            |   |             |        |   |        |         | :            | * * * | * * * :    | * * * * * *   | * * * *                                 | *   -          | <u> </u>       |  |
|     |            |   | +<br>¢<br>¢ | ·<br>? | + | -+<br> | +<br>0. | +<br>80<br>- |       |            | -+            | -+                                      | uma            |                |  |
|     |            |   | 4 4         | -      |   |        | -       | 0            |       | 0          | 5             | <u> </u>                                |                |                |  |

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| Flatter 16, Contrinued<br>3-PONTH RUNNING AVERAGES FOR LEGO<br>3-PONTH RUNNING AVERAGES FO |   |                        |     |       |           |   |   |          |                    |  |   | HTNOM   | YEAR     |  |
|--|---|------------------------|-----|-------|-----------|---|---|----------|--------------------|--|---|---|----------|--|
| +++++++++  | FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | STATION=BRIDGEPORT 123 |     |       |           |   |   |          | *<br>*<br>*<br>**  | ** ** ** ** ** ** ** ** ** ** ** ** ** | * ** ** ** ** ** ** ** ** ** ** ** ** * | 2 3 4 5 6 7 8 9 10 11 12 1 2 3 4 5 6 7 8 9 10 11 12 1 2 3 4 5 6 7 8 9 10 11 12 1 2 3 4 5 6 7 8 9 10 11 12 MONTH |          |  |
|  |   |                        | AVG | 1.6 + | +<br><br> | + | + | +<br>8.0 | ****<br>***<br>0.6 | ****<br>+<br>0.4                       | +                                       | -   | <u>.</u> |  |

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|              |     |   |             |   |       |          |       |                    |                        | 40NTH  | rear        |
|--------------|-----|---|-------------|---|-------|----------|-------|--------------------|------------------------|--------|-------------|
|              |     |   | I           |   |       |          |       |                    | * *                    | 8      | -           |
|              |     |   |             |   |       |          |       |                    | * *                    | 1-     |             |
|              |     |   |             |   |       |          |       |                    | * * *                  | 10     |             |
|              |     |   | 1           |   |       |          |       |                    | * *                    | 16     |             |
|              |     |   | 5<br>5<br>8 |   |       |          |       |                    | * * *                  | 8      |             |
|              |     |   | 1           |   |       |          |       |                    | * *                    |        | I           |
|              |     |   |             |   |       |          |       |                    | * * *                  | 9      | 85          |
|              |     |   |             |   |       |          |       |                    | * *                    | 5      |             |
|              |     |   |             |   |       |          |       |                    | ***                    | 1      |             |
|              |     |   | r<br>1<br>1 |   |       |          |       |                    | * * * * *              | 1 00   |             |
|              |     |   |             |   |       |          |       | *                  | * * * * * *            | N      |             |
|              |     |   |             |   |       |          |       | *                  | * * * * * * *          | -      |             |
| 9            |     |   | 1           |   |       |          |       | *                  | *****                  | N      | -           |
| LEA          |     |   |             |   |       |          |       | *                  | * * * * * *            |        |             |
| OR           |     |   |             |   |       |          |       |                    | * * * * * *            | 10     |             |
| S F 002      |     |   |             |   |       |          |       |                    | * * * * *              | 6      |             |
| RAGE<br>JRY  |     |   |             |   |       |          |       |                    | * * * * *              | ∞      | 1<br>1<br>1 |
| avef<br>anbi |     |   |             |   |       |          |       |                    | * * * *                | ~      | •<br>•      |
| VG /         |     |   |             |   |       |          |       |                    | * * * *                | 9      | - 81        |
| TIOI         |     |   |             |   |       |          |       |                    | ****                   | j n    |             |
| RUI          |     |   |             |   | -     |          |       |                    | * * * * * *            | 4      |             |
| HTN          |     |   |             |   |       |          |       |                    | * * * * * *            | 3      | 1           |
| OM-          |     |   |             |   |       |          |       | *                  | * * * * * *            | $\sim$ | 1           |
| ŝ            |     |   |             |   |       |          |       | * *                | * * * * *<br>* * * * * |        | <u> </u>    |
|              |     |   |             |   |       |          |       | * * *<br>* * *     | * * * * * *            | 12     | -           |
|              |     |   |             |   |       |          |       | * * *<br>* * *     | * * * * * *            | 12     |             |
|              |     |   |             |   |       |          |       | * * *              | * * * * * *            | 2      | 1           |
|              |     |   |             |   |       |          |       | * *                | * * * * * * * *        | 6      |             |
|              |     |   |             |   |       |          |       |                    | * * * *                | ø      | 1           |
|              |     |   |             |   |       |          |       |                    | * * * * *              | ~      | 33          |
|              |     |   |             |   |       |          |       |                    | * * * *                | 0      | ÷           |
|              |     |   |             |   |       |          |       |                    | * * * * *              | 5      |             |
|              |     |   |             |   |       |          |       |                    | * * * *                | 1      |             |
|              |     |   |             |   |       |          |       |                    | * * * * * *            | ŝ      | ł           |
|              |     | i |             |   |       |          |       | * *<br>* *         | * * * * * *            | i N    | Ì           |
|              |     |   |             |   |       |          |       | * * * *<br>* * * * | * * * * * *            | -      | <u>i</u>    |
|              | AVG | + | +<br>.+<br> | + | +<br> | +<br>0.8 | 0.6 + | +                  |                        | I      |             |

FIGURE 16, CONTINUED

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|         |        |     |     |        |             |     |   |          |           |                  |   | MONTH | YEAR      |  |
|---------|--------|-----|-----|--------|-------------|-----|---|----------|-----------|------------------|---|-------|-----------|--|
|         |        |     |     |        | 0<br>2<br>2 |     |   |          |           |                  | * * *                                   | 12    | 1         |  |
|         |        |     |     |        |             |     |   |          |           |                  | * * *                                   | 1=    |           |  |
|         |        |     |     |        | <br> <br>   |     |   |          |           |                  | * * *                                   | 10    |           |  |
|         |        |     |     |        |             |     |   |          |           |                  | * * *                                   | 16    | <br> <br> |  |
|         |        |     |     |        |             |     |   |          |           |                  | * * * * *                               | 1 00  | 1         |  |
|         |        |     |     |        |             |     |   |          |           |                  | * * *<br>* * *                          |       | 85        |  |
|         |        |     |     |        |             |     |   |          |           |                  | * * * * *                               |       | !         |  |
|         |        |     |     |        |             |     |   |          |           |                  | ****                                    |       | ł         |  |
|         |        |     |     |        |             |     |   |          |           |                  | *****                                   | 1.47  |           |  |
|         |        |     |     |        |             |     |   |          |           |                  | * |       | ļ         |  |
|         |        |     |     |        |             |     |   |          |           | ****             | * * * * * * * *                         |       |           |  |
|         |        |     |     |        |             |     |   |          |           | * * * *          | * * * * * * *                           |       | <u>.</u>  |  |
|         | EAD    |     |     |        |             |     |   |          |           | * * * * *        | * | 12    | ł         |  |
|         | ۲<br>۳ |     |     |        |             |     |   |          |           | * *              | * * * * * * * *<br>* * * * * * *        | 12    | ļ         |  |
| UED     | FOI    | 014 |     |        |             |     |   |          |           |                  | * * * * * * * *                         | 10    |           |  |
| TIN     | GES    | RD  |     |        |             |     |   |          |           |                  | * * * * * * *                           | 10    | 1         |  |
| CON     | ERA    | TFO |     | i<br>i |             |     |   |          |           |                  | * * * * * *                             | 1 00  | 1         |  |
| 6,      | AV     | HAR |     |        |             |     |   |          |           |                  | * * * * * * *                           |       | 84        |  |
| н-<br>Ш | I NG   | =NO |     |        |             |     |   |          |           |                  | * * * * * * * *                         | 9     | 1         |  |
| GUR     | NNN    | ATI |     |        |             |     |   |          |           |                  | * * * * * *                             | 10    | 1         |  |
| ц.      | Н      | ST  |     |        |             |     |   |          |           |                  | * * * * * *                             |       |           |  |
|         | INU    |     |     |        |             |     |   |          |           |                  | * |       |           |  |
|         | 3-1    |     |     |        |             |     |   |          |           | ب بر<br>بر<br>بر | <br>                                    |       | į         |  |
|         |        |     |     | 1      |             |     |   |          |           | * *              | * * * * * * * * *                       |       | <u>-</u>  |  |
|         |        |     |     |        |             |     |   |          |           | * * *            | * * * * * * * *                         | 12    | -         |  |
|         |        |     |     |        |             |     |   |          |           | * * *            | * * * * * * * *                         | =     |           |  |
|         |        |     |     |        |             |     |   |          |           | * *              | * * * * * * * *                         | 10    |           |  |
|         |        |     |     |        |             |     |   |          |           |                  | * * * * * * * * *                       | 10    | į         |  |
|         |        |     |     | i      |             |     |   |          |           |                  | * * * *<br>* * * *                      | iα    | İ         |  |
|         |        |     |     | i      |             |     |   |          |           |                  | * * *<br>* * *                          |       | 33        |  |
|         |        |     |     | i      |             |     |   |          |           |                  | * * * *<br>* * * *                      | 10    | ł         |  |
|         |        |     |     |        |             |     |   |          |           |                  | * * * *<br>* * * *                      | 19    |           |  |
|         |        |     |     | i      |             |     |   |          |           |                  | * * * * *<br>* * * * *                  | 4     |           |  |
|         |        |     |     | i      |             |     |   |          |           |                  | * * * * * * * *                         | 31    | -         |  |
|         |        |     |     |        |             |     |   |          |           | * * * *          | * * * * * * * *<br>* * * * * * *        |       | ł         |  |
|         |        |     |     | 1      |             |     |   |          |           | * * * * *        | * * * * * * * *<br>* * * * * * *        |       | <u>_</u>  |  |
|         |        |     | AVG | 1.6+   | +<br><br>   | ~~+ | + | +<br>8.0 | 0.6 +<br> |                  | +                                       | - 1   |           |  |

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|              |            |             |     |     |       |                             |                                   |   | MONTH<br>YEAR |
|--------------|------------|-------------|-----|-----|-------|-----------------------------|-----------------------------------|---|---------------|
|              |            | 1           |     |     |       |                             |                                   | * * * *                                 | ~ -           |
|              |            | 1<br>1<br>1 |     |     |       |                             |                                   | * * * *                                 |               |
|              |            | 1<br>1<br>1 |     |     |       |                             |                                   | * * * * * *                             |               |
|              |            |             |     |     |       |                             |                                   | * * * * *                               | 6             |
|              |            | 1<br>1<br>1 |     |     |       |                             |                                   | * * * *                                 |               |
|              |            | t<br>1<br>1 |     |     |       |                             |                                   | * * * *                                 |               |
|              |            |             |     |     |       |                             |                                   | * * * * *                               | 85            |
|              |            | <br> <br>   |     |     |       |                             | *                                 | * * * * * *                             | 2             |
|              |            |             |     |     |       |                             | · *                               | * * * * * * *                           | 4             |
|              |            |             |     |     |       |                             | *<br>* * *                        | * * * * * *                             | т             |
|              |            | 1           |     |     |       | * *                         | * * * *                           | * * * * * *                             |               |
|              |            |             |     |     |       | * * *<br>* * *<br>* * *     | * * * *<br>* * * *<br>* * * *     | * | <u> -</u>     |
| AD           |            |             |     |     |       | * * * *<br>* * * *          | * * * * *                         | * * * * * *                             | 1 3           |
| × Le         |            | ,<br>,<br>, |     |     |       | * * *                       | * * * *<br>* * * *                | * * * * * *                             | =             |
| F0F          | •          |             |     |     |       | * *                         | * * * *                           | * | 2             |
| GES<br>RD (  |            |             |     |     |       |                             | * * *<br>* * *                    | * | 0             |
| ERAI<br>TFOI |            | 1<br>1<br>1 |     |     |       |                             | * * * *                           | * * * * * *                             | ŝ             |
| AV<br>HAR    |            | 1<br>1<br>1 |     |     |       |                             | * * *                             | * * * * * *                             | 84            |
| I NG         |            | 1<br>1<br>1 |     |     |       |                             | * * *                             | * * * * * *                             |               |
| UNN          |            | <br> <br>   |     |     |       |                             | * * *<br>* * *                    | * * * * * *                             | 5             |
| ST ST        |            | <br> <br>   |     |     |       |                             | * * * * *                         | * |               |
| INUT         |            | 1<br>1<br>1 |     |     |       | * *                         | * * * * *                         | * * * * * *                             | ι ερ<br>Γ     |
| 1            |            |             |     |     |       | * *<br>* *<br>* *           | ~ ~ ~ ~ ~<br>* * * *<br>* * * * * | ~~~~~<br>* * * * * *<br>* * * * * *     |               |
|              |            |             |     |     |       | * * * *                     | * * * * *                         | * * * * * * *                           | -             |
|              |            |             |     |     |       |                             |                                   |   | 12            |
|              |            |             |     |     |       |                             |                                   |   |               |
|              |            |             |     |     |       |                             |                                   |   | 2             |
|              |            |             |     |     |       |                             |                                   |   | 6             |
|              |            |             |     |     |       |                             |                                   |   |               |
|              |            |             |     |     |       |                             |                                   |   | 83            |
|              |            |             |     |     |       |                             |                                   |   | 9             |
|              |            |             |     |     |       |                             | * * * *                           | * | 10            |
|              |            |             |     |     |       | * * *                       | ****                              | *****                                   |               |
|              |            | 6<br>       |     |     |       | * * * * *<br>* * *<br>* * * | * * * * *                         | * * * * * *                             |               |
|              |            |             |     |     |       | *****                       | * * * * *                         | ~ ~ ~ ~ <del>~</del> *<br>* * * * * *   |               |
|              | +          |             | +   |     | +     | ****<br>+                   | ¥ ¥ ¥ ¥<br>+                      | * * * * * *                             |               |
|              | AVG<br>1.6 | 1.4         | 1.2 | 1.0 | . 8.0 | 0.6                         | 0.4                               | 0.2                                     | -             |

FIGURE 16, CONTINUED

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|       |      |        |     |     |     |     |        |              |                |                       |                    |   |            | MONTH  | YEAR           |
|-------|------|--------|-----|-----|-----|-----|--------|--------------|----------------|-----------------------|--------------------|---|------------|--------|----------------|
|       |      |        |     | (   |     |     |        |              |                |                       |                    | * * *                                   | * *        |        | <del>.</del> . |
|       |      |        |     |     |     |     |        |              |                |                       |                    | * * *                                   | * *        |        |                |
|       |      |        |     | 1   |     |     |        |              |                |                       |                    | * * *                                   | * *        |        |                |
|       |      |        |     | Ì   |     |     |        |              |                |                       |                    | * * *                                   | * *        | Ē      | i              |
|       |      |        |     |     |     |     |        |              |                |                       |                    | * * *                                   | * *        |        | 1              |
|       |      |        |     |     |     |     |        |              |                |                       |                    | * * * *                                 | * *        |        | 1              |
|       |      |        |     |     |     |     |        |              |                |                       |                    | * * * * *                               | * *        |        | 85             |
|       |      |        |     |     |     |     |        |              |                |                       |                    | * * * * *                               | * *<br>* * | 9      | 1              |
|       |      |        |     |     |     |     |        |              |                |                       |                    | * * * * *                               | * *        | 5      |                |
|       |      |        |     | l   |     |     |        |              |                |                       | * *                | * * * *                                 | * *<br>* * | 1.27   | <br> <br>      |
|       |      |        |     | i   |     |     |        |              |                |                       | * *                | * * * * *                               | * *        | ŝ      | i<br>I         |
|       |      |        |     | 1   |     |     |        |              |                | * * *                 | : * * *<br>: * * * | * * * *                                 | * *<br>* * | N      | ŀ              |
|       |      |        |     |     |     |     |        |              | *              | * * *<br>* * *        | : * * *<br>: * * * | * * * *<br>* * * *                      | * *<br>* * | -      | <u> </u>       |
|       | EAD  |        |     |     |     |     |        |              | *              | * * *                 | * * * *            | * * * * *                               | * *        | 12     | 6<br>6<br>6    |
|       |      |        |     | l   |     |     |        |              |                | * *                   | : * * *<br>: * * * | * * * *                                 | * *<br>* * | 1 =    | 1<br>1<br>1    |
| JED   | FOI  | 016    |     |     |     |     |        |              |                | *                     | * * * *            | * * * * *                               | * *<br>* * | 12     | 1              |
| LIN   | GES  | д<br>С |     |     |     |     |        |              |                | *<br>*                | : * * *<br>: * * * | * * * *                                 | * *        | 6      |                |
| LNO   | ERAC | FOF    |     |     |     |     |        |              |                | * *                   | : * * *<br>: * * * | * * * * * * *                           | * *        | ίœ     | Ì              |
| 0<br> | AVE  | IART   |     |     |     |     |        |              |                | *                     | * * * *            | * * * *                                 | * *        |        | 34             |
| 16    | NG   | N=N    |     |     |     |     |        |              |                |                       | * * *              | * * * * *                               | * *        | 0      | :              |
| URE   | NN   | TIO    |     |     |     |     |        |              |                |                       | * *                | * * * *<br>* * * *                      | * *        | 5      |                |
| FIG   | RU   | STA    |     |     |     |     |        |              |                | *                     | * * * *            | * * * * *                               | * *        | 1      |                |
|       | NTH  |        |     |     |     |     |        |              | *<br>*         | * * *                 | * * * *            | * * * *                                 | * *<br>* * | 3      |                |
|       | 0W-  |        |     |     |     |     |        |              | * *            | * * *                 | * * * *            | * * * *                                 | * *        | $\sim$ |                |
|       | ŝ    |        |     |     |     |     |        | *            | * *            | * * *                 | : * * *            | * * * *                                 | * *<br>* * | -      | <u> </u>       |
|       |      |        |     |     |     |     |        |              | * *            | * * *                 | : * * *<br>: * * * | * * * * *                               | * *<br>* * | 2      |                |
|       |      |        |     |     |     |     |        |              | * *<br>* *     | * * *                 | : * * *<br>: * * * | * * * * *                               | * *        | =      | į              |
|       |      |        |     |     |     |     |        |              |                | * *                   | : * * *<br>: * * * | * * * * *                               | * *<br>* * | 2      |                |
|       |      |        |     | 1   |     |     |        |              |                |                       | * * *<br>* * *     | * | * *        | 6      |                |
|       |      |        |     | 1   |     |     |        |              |                |                       | * *                | * * * * *                               | * *        | ß      |                |
|       |      |        |     |     |     |     |        |              |                |                       | * *                | * * * * *                               | * *        |        | ŝ              |
|       |      |        |     | 1   |     |     |        |              |                | *                     | * * * *            | * * * *                                 | * *        | 9      | α<br>I         |
|       |      |        |     |     |     |     |        |              |                | #<br>k                | ***                | * * * *                                 | * *<br>* * | 5      | E<br>E<br>E    |
|       |      |        |     |     |     |     |        |              |                | * * *                 | ***                | * * * *                                 | * *        | 4      |                |
|       |      |        |     |     |     |     |        |              |                | * *                   | * * *              | * * * *                                 | * *        |        |                |
|       |      |        |     |     |     |     |        | * *          | * *            | * * *                 | * * * *            | * * * * *                               | * *        | $\sim$ |                |
|       |      |        |     |     |     |     |        | * * *        | * *            | * * *                 | ****               | ****                                    | * *<br>* * | -      | i              |
|       |      |        |     | +   |     | +   | :<br>+ | • + * *<br>+ | + <del>*</del> | ~ <del>*</del> *<br>+ | +-                 | · • • • *<br>+                          | * *        | i      | _              |
|       |      |        | AVG | 1.6 | 1.4 | 1.2 | 1.0    | 0.8          |                | 0.6                   | 0.4                | 0.2                                     |            |        |                |

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MONTH YEAR -----\* \* 9 10 11 12 \* \* \* \* \* \* \* \* \* \* \* \* \* \* ω ~ \*\* \*\* \*\* 85 9 \* \*\* \*\* ŝ \*\* \*\* \*\* \*\* 4 \* \* \*\* \*\* ŝ \*\* \*\* \*\* \*\* \*\* 2 \* \* \* \* 1111 \*\* \*\* \* ----\*\* \* \* \*\* \* \*\* \*\* \*\* \*\* ļ 9 10 11 12 3-MONTH RUNNING AVERAGES FOR LEAD \*\* \*\* \*\* \*\* \*\* \*\* \* \* \*\* \*\* \*\* \*\* \* \* \* \* FIGURE 16, CONTINUED \*\* \*\* \*\* \*\* STATION=MERIDEN 002 \* \* \* \* \* \* \* \* \* \* ω 1~ \* \* \* \* 84 9 \* \* \* \* \* \* \* \* \* 5 L \* \* \* \* \* 4 \* \* ŝ \* \* \* \*\* \* \* N \*\* \*\* \* \* \* 1 \* \* \* \* \* \* \* \* -9 10 11 12 \* \* \* \* \* \* \* \* \* \* \* \*\* \*\* \* \*\* \*\* \* \* \* \* \* \* \*\* \*\* \*\* \* \* \* \* ω \*\* \*\* \*\* \* \* \* \* \* \* ~ \*\* 83 9 \*\* \*\* \*\* \*\* \*\* ŝ \*\* \*\* \*\* \*\* \$ \*\* \*\* \*\* \*\* З \*\* \*\* \*\* \*\* \*\* N \*\* \*\* \*\* \*\* \*\* \*\* \*\* 1 \* ~ \*\* \*\* \*\* \*\* \*\* \* \* \* 0.4 0.2 0.8 0.6 1.6 1.4 1.0 AVG 1.2

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| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | 4 003 |   |  |  |  |                 | · ** *** *** · · · · · · · · · · · · · | ** ** ** ** ** ** ** ** ** | 5 6 7 8 9 10 11 12 | 85           |
|---|-------|---|--|--|--|-----------------|--|----------------------------|--------------------|--------------|
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | ¥ 003 |   |  |  |  |                 | · · · · · · · · · · · · · · · · · · ·  | ** ** ** ** ** ** ** **    | 5 6 7 8 9 10 11    | 85           |
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | 4 003 |   |  |  |  |                 | · ** *** · · · · · · · · · · · · · · · | ** ** ** ** ** **          | 5 6 7 8 9 10       | 85           |
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | V 003 |   |  |  |  |                 | · · · · · · · · · · · · · · · · · · ·  | ** ** ** ** ** **          | 5 6 7 8 9          | 85           |
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | ¥ 003 |   |  |  |  |                 | ** ***                                 | ** ** ** **                | 5 6 7 8            | 85           |
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | ¥ 003 |   |  |  |  |                 | ** **                                  | ** ** ** **                | 5 6 7              | 85           |
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | ¥ 003 |   |  |  |  |                 | *******                                | * * * * * * * *            | 5 6                | 8            |
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | ¥ 003 |   |  |  |  |                 | * :<br>* :<br>* :                      | * * *                      | 2                  | 1            |
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | N 003 |   |  |  |  |                 | *:                                     | * * *                      | i                  | 1            |
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | V 003 |   |  |  |  |                 |  | TT                         | t at               |              |
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | N 003 |   |  |  |  |                 | * * *                                  | * * *                      | m                  |              |
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | N 003 |   |  |  |  | *               | * * * *                                | * * *                      | N                  |              |
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | N 003 |   |  |  |  | ۔<br>+ +<br>+ * | * * * *                                | * * *                      | -                  | <u>i</u>     |
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD | N 003 |   |  |  |  | * *             | ***                                    | * * *                      |                    | <del>_</del> |
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR 1    | N 003 |   |  |  |  | * *             | * * * :                                | * * *                      |                    |              |
| FIGURE 16, CONTINUEE<br>3-MONTH RUNNING AVERAGES FC       | 00 1  |   |  |  |  | ג *<br>ג *      | * * * :                                | * * *                      | 10                 |              |
| FIGURE 16, CONTIN<br>3-MONTH RUNNING AVERAGES             | -     |   |  |  |  | * *             | * * *                                  | * * *                      | 6                  | 1            |
| FIGURE 16, CON<br>3-MONTH RUNNING AVER                    | LOWI  | į |  |  |  |                 | * * *                                  | * * *                      | 0                  |              |
| FIGURE 16,<br>3-MONTH RUNNING AV                          | OLET  | į |  |  |  |                 | * * *                                  | * * *                      |                    | I            |
| FIGURE 1<br>3-MONTH RUNNING                               | 1 DC  | ļ |  |  |  |                 | *                                      | * * *                      |                    | 84           |
| FIGUF<br>3-MONTH RUNN                                     | N=N0  | ļ |  |  |  |                 | *                                      | * * *                      | 5                  |              |
| FI<br>3-MONTH F   | TIC.  | ļ |  |  |  |                 | * *                                    | * * *                      |                    |              |
| 3-MONT  | STA   |   |  |  |  |                 | * *                                    | * * *                      | 100                | i<br>i       |
| 3 - 1   |       | ļ |  |  |  |                 | **                                     | * * *                      |                    |              |
|   | J     |   |  |  |  |                 | * * *                                  | * * *                      |                    | i            |
|   |       |   |  |  |  | *               | * * *                                  | * * *                      |                    |              |
|   |       |   |  |  |  | * * *           | * * *                                  | * * *                      | 12                 | -            |
|   |       |   |  |  |  | * * * * * *     | * * *                                  | * * *                      | 12                 |              |
|   |       |   |  |  |  | * :             | * * *                                  | * * *                      | 10                 |              |
|   |       |   |  |  |  |                 | * *                                    | * * *                      | 6                  | İ            |
|   |       | 1 |  |  |  |                 | * *                                    | * * *                      | 0                  | i            |
|   |       | 1 |  |  |  |                 |  | * * *                      | 1                  | 33           |
|   |       |   |  |  |  |                 |  | * * *                      | 0                  |              |
|   |       |   |  |  |  |                 |  | * * *                      | 5                  | ļ            |
|   |       | ļ |  |  |  |                 | *                                      | * * *                      | 1=                 | 1            |
|   |       | i |  |  |  |                 | * * *                                  | * * *                      | 10                 |              |
|   |       |   |  |  |  | *               | * * *                                  | * * *                      | 2                  | 1<br>1<br>1  |
|   |       |   |  |  |  | *               | * * *                                  |                            |                    |              |
|   |       |   |  |  |  | * * *           | * * *<br>* * *<br>* * *                | * * *                      |                    | i<br>        |

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|                      |  |              |  |     |       |       |      |                                      |  | MONTH  | YEAR             |  |  |
|----------------------|--|--------------|--|-----|-------|-------|------|--------------------------------------|--|--|------------------|--|--|
| FIGURE 16, CONTINUED | 3-MONTH RUNNING AVERAGES FOR LEAD<br>STATION=NEW BRITAIN 007 |              |  |     |       |       |      | **<br>** ** ** **                    | ** ** ** ** ** ** ** ** ** ** ** ** **                           | 6 7 8 9 10 11 12 1 2 3 4 5 6 7 8 9 10 11 12 1 2 3 4 5 6 7 8 9 10 11 12 MONTH | · 83 85 84 84 84 |  |  |
|                      |  |              | <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> |     |       |       |      | * * * * * *                          | · **<br>*** **<br>*** **<br>*** **<br>**<br>**<br>**<br>**<br>** | 9 10 11  |                  |  |  |
|                      |  |              | 1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1    |     |       |       |      |                                      | ** ** ** ** ** **  | t 5 6 7 8  | 83               |  |  |
|                      |  | +            |  |     |       |       | +    | *** **<br>*** **<br>*** **<br>*** ** | ** ** ** **<br>** ** **<br>** ** **<br>** ** **<br>** **         | 1 2 3 4  |                  |  |  |
|                      |  | AVG<br>1.6 - | 1.4  | 1.2 | - 0.1 | - 8.0 | .0.6 | - th - 0                             |  | •  |                  |  |  |

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|                     |     |       |   |   |            |                |   | TNOM   | YEAR     |
|---------------------|-----|-------|---|---|------------|----------------|---|--------|----------|
|                     |     |       |   |   |            |                |   | 12     | Ī        |
|                     |     |       |   |   |            |                |   | 12     |          |
|                     |     |       |   |   |            |                |   | 10     |          |
|                     |     |       |   |   |            |                | * * * *                                 | 6      |          |
|                     |     |       |   |   |            |                | 47 47 47 47                             | ω      | İ        |
|                     |     |       |   |   |            |                |   | ~      |          |
|                     | 1   |       |   |   |            |                |   | 9      | 8        |
|                     | 1   |       |   |   |            | *              | * * * * *                               | 5      |          |
|                     | 1   |       |   |   |            | *<br>* *       | * * * * *                               |        | 1        |
|                     | 1   |       |   |   |            | * * *          | * * * * * *                             | 3      |          |
|                     |     |       |   |   |            | * * *          | * * * * *                               |        | ł        |
|                     |     |       |   |   |            | * * * *        | * * * * * *                             |        | ĺ        |
|                     |     |       |   |   |            | * * * *        | * * * * *                               | i<br>i | <u> </u> |
| AD                  |     |       |   |   | *<br>*     | * * * *        | * * * * * *                             | 12     | 1        |
|                     | 1   |       |   |   |            | * * * * *      | * * * * * *                             | i E    | į        |
| FOF<br>FOF          |     |       |   |   | *<br>*     | * * * * *      | * * * * * * * *                         | i P    | i        |
|                     |     |       |   |   | *<br>*     | * * * * *      | * | i o    | i        |
| CONT<br>CRAC        |     |       |   |   | * *<br>* * | * * * * *      | * * * * * *                             | ίœ     | i        |
| Y A V               |     |       |   |   | * *        | * * * *        | * * * * * *                             | ~      | 77       |
| 16<br>= NG          |     |       |   |   |            | * * *          | * | 0      | !        |
| URE<br>NN I<br>I ON | · • |       |   |   |            | *<br>*         | * * * * * * *                           | 5      |          |
| FIG<br>RU<br>TAT    | 1   |       |   |   |            | *              | * * * * * *                             | 4      |          |
| NTH<br>S            |     |       |   |   |            | * * *          | * * * * * * *                           | m      |          |
| ОМ -                |     |       |   |   |            | * * * * *      | * * * * * *                             | $\sim$ |          |
| 'n                  |     |       |   |   |            | * * * *        | * * * * * *                             |        | <u> </u> |
|                     |     |       |   |   |            | * * * *        | * * * * *                               | 10     | -        |
|                     |     |       |   |   | * *        | * * * *        | * * * * * *                             |        |          |
|                     |     |       |   |   | * *        | * * * *        | * * * * * *                             | 10     |          |
|                     |     |       |   |   | *          | ****           | *****                                   | Ĩ      | İ        |
|                     |     |       |   |   |            | ****           | *****                                   |        | i        |
|                     |     |       |   |   |            | * * *          | *****                                   |        | i        |
|                     | 1   |       |   |   |            | * * *          | * * * * *                               |        | 83       |
|                     |     |       |   |   |            | * *<br>* *     | * * * * * *                             | 9      | ł        |
|                     |     |       |   | • |            | *              | * * * * * *                             | 5      |          |
|                     |     |       |   |   |            | * *<br>* *     | * * * * * *                             | 17     | 1        |
|                     |     |       |   |   |            | * * *<br>* * * | * * * * * *                             | ŝ      |          |
|                     |     |       |   |   |            |                |   | N      | İ        |
|                     |     |       |   |   |            |                |   |        | i        |
|                     | +   | <br>+ | + | + |            | +              | ~~ +                                    | · i    |          |

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|        |                    |     |                  |                          |     |     |     |     |   |  |  | MONTH  | YEAR                       |  |
|--------|--------------------|-----|------------------|--------------------------|-----|-----|-----|-----|---|--|--|--|----------------------------|--|
|        |                    |     |                  |                          |     |     |     |     |   |  |  | 1 12   |                            |  |
|        |                    |     |                  |                          |     |     |     |     |   |  | * * *  | 9 10 1   | 1<br>7<br>7                |  |
|        |                    |     |                  | <br> <br> <br>           |     |     |     |     |   |  | *                  | 7 8  |                            |  |
|        |                    |     |                  | 9<br>9<br>7<br>1<br>1    |     |     |     |     |   | * * *                                    | * * * *<br>* * * * *<br>* * * * *<br>* * * * *           | 5 6  | 85                         |  |
|        |                    |     |                  |                          |     |     |     |     | :                                       | * * * *<br>* * * *<br>* * * *<br>* * * * | *                  | 3 4  |                            |  |
|        |                    |     |                  | <br> <br> <br> <br> <br> |     |     |     |     | :                                       | * * * * *                                | * * * * * *<br>* * * * * *<br>* * * * * *<br>* * * * * * | 1 2  |                            |  |
|        | LEAD               |     |                  | ?<br>!<br>!<br>!         |     |     |     |     | ***                                     | ****                                     | *                  | 1 12   | -                          |  |
| INUED  | ES FOR<br>N 123    |     |                  | 1<br>1<br>1<br>1         |     |     |     |     | * *                                     | *  | * * * * *<br>* * * * *<br>* * * * *<br>* * * * *         | 9 10 1   |                            |  |
| , CONT | averagi<br>W Haven |     |                  |                          |     |     |     |     |   | * *<br>* *<br>* *<br>* *                 | * * * * * *<br>* * * * * *<br>* * * * * *<br>* * * * * * | 7 8  | +                          |  |
| URE 16 | I ON=NE            |     |                  |                          |     |     |     |     |   | * * *<br>* * *<br>* * *<br>* * *         | *                  | 5 6  |                            |  |
| FIG    | NTH RU<br>STAT     |     |                  |                          |     |     |     |     | +<br>+<br>+<br>+                        | * * * *<br>* * * *<br>* * * *            | * * * * * *<br>* * * * *<br>* * * * *                    | 3 4  | 1<br>1<br>1<br>1<br>1      |  |
|        | 3 <b>-</b> M(      |     |                  |                          |     |     |     |     | * * *<br>* * *<br>* * *                 | * * *<br>* * *<br>* * *                  | * * * * * *<br>* * * * *<br>* * * * * *                  | 1  |                            |  |
|        |                    |     |                  |                          |     |     |     | 2   | * * * *                                 | * * * *                                  | *                  | 11 12  |                            |  |
|        |                    |     |                  |                          |     |     |     |     | * * *<br>* * *<br>*                     | * * *<br>* * *<br>* * *                  | * * * * * *<br>* * * * *<br>* * * * *                    | 9 10   | 1<br>1<br>1<br>1<br>1<br>1 |  |
|        |                    |     | 1<br>1<br>1<br>1 |                          |     |     |     |     |   | * * *<br>* * *<br>* *                    | * * * * * *<br>* * * * *<br>* * * * *<br>* * * * *       | 7 8  | n<br>B                     |  |
|        |                    |     |                  |                          |     |     |     |     |   | * :<br>* :<br>* :<br>* :                 | *                  | 5 6  | }<br> <br> <br> <br>       |  |
|        |                    |     |                  |                          |     |     |     |     | * * *                                   | *  | *                  | 1<br>3<br>7<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1 |                            |  |
|        |                    |     | +                |                          |     | +   | +   | * * | * | * * * * :<br>* * * :<br>* * * :          | * * * * * *<br>* * * * *<br>* * * * *<br>* * * * *       |  |                            |  |
|        |                    | AVG | 1.6              | 1.4                      | 1.2 | 1.0 | 0.8 |     |   | 0.4                                      | 0.2  |  |                            |  |

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|   |        | :      |      |     |         |             |                |            |     |               |   |                            | MONTH          | YEAR        |
|---|--------|--------|------|-----|---------|-------------|----------------|------------|-----|---------------|---|----------------------------|----------------|-------------|
|   |        |        |      |     |         | !           |                |            |     | -             |   | * *                        | N              |             |
|   |        |        |      |     |         |             |                | •          |     |               |   | * *                        |                | 1<br>1<br>1 |
|   |        |        |      |     |         |             |                |            |     |               |   | * * *                      | 0              |             |
|   |        |        |      |     |         | 1           |                |            |     |               |   | * * *                      | 6              | i           |
|   |        |        |      |     |         |             |                |            |     |               |   | * * *                      | 0              |             |
|   |        |        |      |     |         | 1<br>1      |                |            |     |               |   | * * *                      |                | 5           |
|   |        |        |      |     |         |             |                |            |     |               |   | * * *                      | 9              | α<br>I      |
|   |        |        |      |     |         | 1<br>1<br>1 |                |            |     |               |   | * * * *                    | 12             |             |
|   |        |        |      |     |         |             |                |            |     |               |   | * * * *                    | 4              |             |
|   |        |        |      |     |         |             |                |            |     |               | 1                                       | * * * * * *                | 5              |             |
|   |        |        |      |     |         |             |                |            |     |               | * :                                     | * * * * * *                | $\sim$         |             |
|   |        |        |      |     |         | 1           |                |            |     |               | * * :                                   | * * * * * *                | -              |             |
|   |        | AD     |      |     |         | 1<br>1<br>1 |                |            |     |               | * * :                                   | * * * * * *                | 12             | 1           |
|   |        |        |      |     |         |             |                |            |     |               | * * *                                   | * * * * * *                | =              |             |
|   | JED    | FOF    | N    |     |         |             |                |            |     |               | * :                                     | * * * * * *                | 12             |             |
|   | LINU   | GES    | 10 > |     |         |             |                |            |     |               | :                                       | * * * * * *                | 6              |             |
|   | LNOC   | ERAC   | 4AL4 |     |         |             |                |            |     |               | :                                       | * * * * * *                | 8              |             |
|   | ý.     | AVE    | VORN |     |         |             |                |            |     |               | * :                                     | * * * * * *                | ~              | 34          |
| , | щ<br>Ц | I NG   | I=NO |     |         | <br> <br>   |                |            |     |               | * :                                     | * * * * * *                | 0              |             |
|   | GUR    | NNN    | ATI  |     |         | t<br>1      |                |            |     |               | :                                       | * * * * * *                | 5              |             |
|   | Ц.     | Н<br>В | ST   |     |         | [<br>]<br>[ |                |            |     |               | * :                                     | * * * * * *                | - <del>1</del> |             |
|   |        | ONT    |      |     |         | <br> <br>   |                |            |     |               | * :                                     | * * * * * *                | 3              |             |
|   |        | 3-M    |      |     |         | 1           |                |            |     |               | * * * * *                               | * * * * * *                | $\mathbb{N}$   |             |
|   |        |        |      |     |         | 1           |                |            |     |               | * * * * :                               | * * * * * *<br>* * * * * * | [              | -           |
|   |        |        |      |     |         |             |                |            |     | 3             | * | * * * * * *                | 12             | -           |
|   |        |        |      |     |         | 1           |                |            |     | * *           | * * * * * * *                           | * * * * * *                | =              |             |
|   |        |        |      |     |         |             |                |            |     |               | * * * :                                 | * * * * * *                | 10             |             |
|   |        |        |      |     |         |             |                |            |     |               | * * :                                   | * * * * * *                | 10             |             |
|   |        |        |      |     |         |             |                |            |     |               | :                                       | * * * * * *                | iα             | i<br>I      |
|   |        |        |      |     |         | 1           |                |            |     |               |   | * * * * *                  | 1              | 83          |
|   |        |        |      |     |         |             |                |            |     |               |   | * * * *                    | 9              | ł           |
|   |        |        |      |     |         | 1<br>1<br>1 |                |            |     |               |   | * * * *                    | 5              |             |
|   |        |        |      |     |         |             |                |            |     |               |   | * * * * *                  | 1              |             |
|   |        |        |      |     |         | 1<br>1<br>1 |                |            |     |               |   | * * * * * *                | 3              |             |
|   |        |        |      |     |         |             |                |            |     | الم الله الله | ***:                                    | *****                      |                |             |
|   |        |        |      |     | <b></b> |             | <b></b>        |            |     | ***           | ****                                    | * * * * * *                |                | ÷           |
|   |        |        |      | AVG | 9.1     |             | 2.<br>2.<br>1. | , <u> </u> | 8.0 | 0.6           | - 17                                    | 0.2                        | •              |             |

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MONTH YEAR \* \* \* \* 9 10 11 12 -----\* \* \*\* \* \*\* \*\* \* \* \* \* \* \* ω 1 \*\* \* \* \* ~ 85 \* \* \* \* \* v \* \* \* \* ŝ \$ \* \* \* \* \* ŝ \* \* \* \* N i \* \* \* \* \* \* -9 10 11 12 3-MONTH RUNNING AVERAGES FOR LEAD \* \* \* \* \*\* FIGURE 16, CONTINUED STATION=STAMFORD 001 \*\* \*\* \*\* \* \* \* \* \*\* ω \* \* \* \* \*\* \* \* 2 \* \* \* \*\* 84 \* \* 9 \*\* \*\* S \*\* \* \* \*\* 4 \* \* \*\* \*\* \*\* ŝ \*\* \*\* \*\* N \*\* \*\* \*\* \* \* \*\* \* \* \* \* \* \* \* ----1 10 11 12 \* \* \* \*\* \* \* \* \* \* \* \* \*\* \*\* \*\* \*\* \*\* \* \* \* \* \* \* \*\* \* \* 9 \* \*\* \*\* \* \* \* \* \* \* ω \*\* \* \* \* \* \*  $\sim$ \*\* 83 \* \* 9 \* \* \*\* ŝ \*\* 4 \*\* \*\* \*\* \*\* ŝ \*\* \*\* \*\* \* \* N \*\* \*\* \*\* \* \* \*\* \*\* 1 -\*\* \* \*\* \*\* \* \*\* \* \* \*\* \*\* 0.2 AVG 0.8 0.6 0.4 1.6 1.4 1.2 1.0

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|                    |              |             |     |                |                   |                |                                       | MONTH  | YEAR        |
|--------------------|--------------|-------------|-----|----------------|-------------------|----------------|---------------------------------------|--------|-------------|
|                    |              |             |     |                |                   |                | * * *                                 | 1 12   | -           |
|                    |              |             |     |                |                   |                |                                       | 0      |             |
|                    |              |             |     |                |                   |                |                                       | 6      |             |
|                    |              |             |     |                |                   | -              | * * * * *                             | ø      |             |
|                    |              |             |     |                |                   |                | * * * * * * * * * * * * * * * * * * * | ~      | 1           |
|                    |              |             |     |                |                   |                | *****                                 | 9      | 80          |
|                    |              |             |     |                |                   |                | * * * * * *                           | 5      |             |
|                    |              |             |     |                |                   | * :            | * * * * * *                           | 1      |             |
|                    |              |             |     |                |                   | * *            | * * * * * *                           | 3      | <br> <br>   |
|                    |              | • •         |     |                |                   | *              | * * * * * *                           | $\sim$ |             |
|                    | i            |             |     |                |                   | * *            | * * * * * *                           |        | <u> </u>    |
| ٩D                 |              |             |     |                |                   | * *            | * * * * *                             | 12     | -           |
| Ē                  |              |             |     |                |                   | * * *          | * * * * * *                           | 12     |             |
| ED<br>FOR<br>22    |              |             |     |                |                   | * *            | * * * * * *                           | 10     | 1<br>1      |
| TINU<br>ES         |              |             |     |                |                   | * * *          | * * * * * *                           | 0      |             |
| :RAG<br>IFOR       |              |             |     |                |                   | * * *          | * * * * * *                           | 8      | ł           |
| , C<br>AVE<br>STAM |              |             |     |                |                   | * * *          | * * * * * *                           | ~      | 34          |
| E 16<br>NG         |              |             |     |                |                   | * *            | * * * * * *                           | 9      | 1           |
| SURE<br>JNNI       |              |             |     |                |                   | *              | * * * * * *                           | 5      |             |
| FIC<br>STA         |              |             |     |                |                   | *              | * * * * * *                           | i      | ļ           |
| ILL                |              |             |     |                |                   | * *            | * * * * * *                           | i m    |             |
| 3 - M(             |              |             |     |                |                   | * *            | * * * * * *                           |        |             |
|                    |              |             |     |                |                   | * *            | * * * * * *                           | -      | <u>-</u>    |
|                    |              |             |     |                |                   | * *            | * * * * * *                           | 12     | 1           |
|                    |              |             |     |                |                   | * * *          | * * * * * *                           | Ξ      | i<br>i<br>i |
|                    |              |             |     |                |                   | * * * *        | * * * * * *                           | 10     | 5           |
|                    |              |             |     |                |                   | * * *<br>* * * | * * * * * *                           | 10     |             |
|                    |              |             |     |                |                   | * * * *        | * * * * * *                           | ∞      | İ           |
|                    |              |             |     |                |                   | * * *          | * * * * * *                           | -      | 83          |
|                    |              | 1           |     |                |                   | * *<br>* *     | * * * * * *                           | 10     |             |
|                    |              |             |     |                |                   | *              | * * * * * *                           | 12     | 1<br>1<br>1 |
|                    |              | 1           |     |                |                   | *              | * * * * * *                           | 17     |             |
|                    |              |             |     |                | -                 | * *            | * * * * * *                           | 3      |             |
|                    |              |             | ÷   |                |                   | * * * *        | · · · · · · · ·                       | N      |             |
|                    |              | 1<br>1<br>1 |     | <br><b>k</b> _ | * * * * * * * * * | * * * * *      | * * * * * *                           |        | <u>-</u>    |
|                    | AVG<br>1.6 + | +<br>       | 1.2 | <br>8.0        | 0.6               | 0.4            | 0.2                                   | ×      |             |

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|        |      |       |     |             |   |     |     |     |                    |   | MONTH  | YEAR        |
|--------|------|-------|-----|-------------|---|-----|-----|-----|--------------------|---|--------|-------------|
|        |      |       |     | l           |   |     |     |     |                    | * *   | 12     | :           |
|        |      |       |     |             |   |     |     |     |                    | * *   | 1      | 1           |
|        |      |       |     |             |   |     |     |     |                    | * * *   | 10     | 1           |
|        |      |       |     |             |   |     |     |     |                    | * *   | 6      | 1           |
|        |      |       |     | 1<br>K<br>5 |   |     |     |     |                    | * *   | 0      | 1<br>1<br>1 |
|        |      |       |     |             |   |     |     |     |                    | * * *   | ~      | 5           |
|        |      |       |     | 8           |   |     |     |     |                    | * * *<br>* * *  | 0      | eo<br>!     |
|        |      |       |     |             |   |     |     |     |                    | * * * * *   | 5      |             |
|        |      |       |     |             |   |     |     |     |                    | * * * *<br>* * * *  | 1      |             |
|        |      |       |     |             |   |     |     |     |                    | * * * * * *   | m      |             |
|        |      |       |     | i           |   |     |     |     | * *                | * * * * * *   | $\sim$ |             |
|        |      |       |     |             |   |     |     |     | * * * *<br>* * * * | * * * * * *   | -      | 1           |
|        | AD   |       |     |             |   |     |     |     | * * *              | * * * * * *   | 2      | -           |
|        | Ц    |       |     |             |   |     |     |     | * *                | * * * * * *   | =      |             |
| E      | FOR  | 001   |     | F<br>1<br>1 |   |     |     |     |                    | * * * * * *   | 2      |             |
| NN I   | ES   | RD    |     |             |   |     |     |     |                    | * * * * * *   | 6      |             |
| I NO   | RAG  | IGFO  |     | 1           |   |     |     |     |                    | * * * * * *   | 8      | 1           |
| ວ<br>ລ | AVE  | LIN   |     |             |   |     |     |     |                    | * * * * * *   |        | 4           |
| - 10   | NG   | MAL   |     |             |   |     |     |     |                    | * * * *   | 9      | α<br>I      |
| UKE    | NN   | =NO   |     |             |   |     |     |     |                    | * * * * *   | 5      |             |
| -      | H R( | LAT I |     |             |   |     |     |     |                    | * * * *   | ŧ      | 1<br>1<br>2 |
|        | NTI  | S     |     |             |   |     |     |     |                    | * * * * * *   | ŝ      |             |
|        | 3-M( |       |     |             |   |     |     |     | *                  | * * * * * *   | N      |             |
|        |      |       |     |             |   |     |     |     | * * *<br>* * *     | * * * * * *   | -      | <u> </u>    |
|        |      |       |     |             |   |     |     |     | * * * *            | * * * * *   | 2      |             |
|        |      |       |     |             |   |     |     |     | * * *              | * * * * * *   | Ξ      |             |
|        |      |       |     |             |   |     |     |     | *                  | * * * * * *   | 0      |             |
|        |      |       |     |             |   |     |     |     | •                  | * * * * * *   | 6      |             |
|        |      |       |     |             |   |     |     |     |                    | * * * *   | ø      |             |
|        |      |       |     |             |   |     |     |     |                    | * * * * *   | -      | ŝ           |
|        |      |       |     |             |   |     |     |     |                    | * * *  <br>* * *  | 9      | α<br>I      |
|        |      |       |     | 1           |   |     |     |     |                    | * * *   | 5      |             |
|        |      |       |     |             |   |     |     |     |                    | <br>  | 4      |             |
|        |      |       |     | 1           |   |     |     |     | *<br>*             | <br>* * * * * *  <br>* * * * *  | ŝ      | )<br> <br>  |
|        |      |       |     |             |   |     |     |     | * * *<br>* * *     | <br>* * * * *  <br>* * * * *  | 2      | -           |
|        |      |       |     | 1           |   |     |     | * * | * * * * *          | <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> <br> |        | <u> </u>    |
|        |      |       | +   |             | + | +   | +   | +   | +<br>+             | -+  |        |             |
|        |      |       | 1.( | <br>        |   | 1.( | 0.5 | 0.6 | 0.1                | 0.5   |        |             |

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|      |        |      |    |        |           |        |       |        |   |                    |                 | MONTH | YEAR         |  |
|------|--------|------|----|--------|-----------|--------|-------|--------|---|--------------------|-----------------|-------|--------------|--|
|      |        |      |    |        |           |        |       |        |   |                    | * * *           | 12    | <del>-</del> |  |
|      |        | -    |    | i      |           |        |       |        |   |                    | * * *           | 11    | ł            |  |
|      |        |      |    |        |           |        |       |        |   |                    | * * *           | 10    |              |  |
|      |        |      |    |        |           |        |       |        |   |                    | * * *           | 6     |              |  |
|      |        |      |    |        |           |        |       |        |   |                    | * * *           | 0     |              |  |
|      |        |      |    |        |           |        |       |        |   |                    | * * * * * * * * |       | 5            |  |
|      |        |      |    | 1      |           |        |       |        |   |                    | * * * * *       | 19    | 00<br>1      |  |
|      |        |      |    |        |           |        |       |        |   |                    | * * * * * *     | 5     |              |  |
|      |        |      |    | 1      | 1<br>     |        |       |        |   | *                  | * * * * * *     | - +   |              |  |
|      |        |      |    | 1      |           |        |       |        |   | * * *              | * * * * *       | 1 00  |              |  |
|      |        |      |    |        |           |        |       |        | 1                                       | * * * *            | * * * * *       |       |              |  |
|      |        |      |    |        |           |        |       |        | * * :                                   | * * * *            | * * * * * *     | -     | <u> </u>     |  |
|      | D      |      |    |        | <br> <br> |        |       |        | * * :                                   | * * * *            | * * * * *       | 1     | -            |  |
|      | LEA    |      |    |        | <br>      |        |       |        | * * *                                   | * * * *            | * * * * * *     | -     |              |  |
| Ω    | OR     | 7    |    |        |           |        |       |        | * 3                                     | * * * *            | * * * * * *     | 10    |              |  |
| NUE  | SF     | 00   |    |        |           |        |       |        |   | * * *              | * * * * *       | 16    | 1            |  |
| NTI  | AGE    | URΥ  |    |        |           |        |       |        |   | * * *              | * * * * * *     | 1 00  | 1            |  |
| 00   | VER    | ERB  |    |        |           |        |       |        |   | * * *              | * * * * * *     |       | 1            |  |
| 16,  | v<br>ک | WAT  |    |        | -         |        |       |        |   | * * *              | * * * * * *     | 9     | 84           |  |
| RE   | Ň      | i=NO |    |        |           |        |       |        |   | * *                | * * * * * *     | 10    | 1            |  |
| I GU | RUN    | ATE  |    | 1      |           |        |       |        |   | *                  | * * * * * *     | ++    | 1            |  |
|      | ΗI     | ST   |    | 1      |           |        |       |        |   | * *                | * * * * * *     | 3     | 1            |  |
|      | MOM    |      |    |        |           |        |       |        | ;                                       | * * *              | * * * * * *     |       |              |  |
|      | 3-     |      |    |        |           |        |       |        | * * :                                   | ****               | * * * * *       |       |              |  |
|      |        |      |    |        |           |        |       |        | * * *                                   | * * * *            | * * * * *       |       | _            |  |
|      |        |      |    | 1      |           |        |       |        | * * * * * *                             | * * * *            | * * * * * *     | 12    |              |  |
|      |        |      |    |        |           |        |       |        | * * * * * *                             | * * * *            | * * * * * *     | 1     |              |  |
|      |        |      |    | 1      |           |        |       |        | * *                                     | * * * *            | * * * * *       | 10    |              |  |
|      |        |      |    | 1      |           |        |       |        | 3                                       | * * * *            | * * * * * *     | 10    |              |  |
|      |        |      |    | 1      |           |        |       |        |   | * *<br>* *         | * * * * * *     | 0     | ł            |  |
|      |        |      |    | 1      |           |        |       |        |   | * *                | * * * * *       | 7     | 83           |  |
|      |        |      |    |        |           |        |       |        |   | * *                | * * * * * *     | 19    | -            |  |
|      |        |      |    |        |           |        |       |        |   |                    | * * * * * *     | 10    |              |  |
|      |        |      |    |        |           |        |       |        |   | * *<br>* *         | * * * * * *     | 1     |              |  |
|      |        |      |    | 1      |           |        |       |        | * * *                                   | * * * *<br>* * * * | * * * * * *     | i m   | Ì            |  |
|      |        |      |    |        |           |        |       | *      | * * * * * * *                           | * * * *            | * * * * * *     | i N   | 1            |  |
|      |        |      |    | 1      |           |        |       | * *    | * | * * * *            | * * * * * *     | 1     | i<br>        |  |
|      |        |      | с  | +<br>9 | +<br>\$   | +<br>N | -+    | +<br>∞ | +<br>0                                  | +<br>t             | ~+              | • 1   |              |  |
|      |        |      | A٧ | ÷.     | ÷.        | -      | <br>- | 0.     | .0                                      | 0.                 | 0.              |       |              |  |

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|  |  |   | MONTH                                  |
|--|--|---|--|
| FIGURE 16, CONTINUED<br>3-MONTH RUNNING AVERAGES FOR LEAD<br>STATION=WATERBURY 123 |  |   | *** *** *** *** *** *** *** *** *** ** |
|  |  | +*************************************  | ************************************** |
|  | -<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1<br>1 | * *<br>* *<br>* *<br>* *<br>* *<br>* * *<br>* *<br>* *<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>*<br>* | ************************************** |
| AVG<br>  |  | 0.0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0<br>0  | -+                                     |

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## **ANNUAL AVERAGE LEAD CONCENTRATIONS**

## SITE: BRIDGEPORT-123





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## **ANNUAL AVERAGE LEAD CONCENTRATIONS**

SITE: BRISTOL-001





## ANNUAL AVERAGE LEAD CONCENTRATIONS

SITE: MERIDEN-002



YEAR



## **ANNUAL AVERAGE LEAD CONCENTRATIONS**

## SITE: MIDDLETOWN-003



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FIGURE C, CONTINUED

## **ANNUAL AVERAGE LEAD CONCENTRATIONS**

## SITE: NEW HAVEN-123



FIGURE C, CONTINUED

 $\begin{pmatrix} & & \\ & & \end{pmatrix}$ 

## ANNUAL AVERAGE LEAD CONCENTRATIONS

## SITE:WALLINGFORD-001



FIGURE C, CONTINUED

## **ANNUAL AVERAGE LEAD CONCENTRATIONS**

## SITE: WATERBURY-123



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FIGURE D

# **3-YEAR RUNNING AVERAGE LEAD CONCENTRATIONS**

## SITE: BRIDGEPORT-123





# **3-YEAR RUNNING AVERAGE LEAD CONCENTRATIONS**

SITE: BRISTOL-001



FIGURE D, CONTINUED

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# **3-YEAR RUNNING AVERAGE LEAD CONCENTRATIONS**

SITE: MERIDEN-002





# **3-YEAR RUNNING AVERAGE LEAD CONCENTRATIONS**

## SITE: MIDDLETOWN-003



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FIGURE D, CONTINUED

# **3-YEAR RUNNING AVERAGE LEAD CONCENTRATIONS**

SITE: NEW HAVEN-123



## FIGURE D, CONTINUED

# **3-YEAR RUNNING AVERAGE LEAD CONCENTRATIONS**

## SITE: WALLINGFORD-001





# **3-YEAR RUNNING AVERAGE LEAD CONCENTRATIONS**

## SITE: WATERBURY-123



### VIII. ACID PRECIPITATION

### **MONITORING PROGRAM**

Recently, there has been a growing public concern about the occurrence and effects of atmospheric deposition, most notably acid precipitation or "acid rain." It has become apparent that, in order to address this concern, basic data need to be collected on the chemical properties of precipitation. Recognizing this, the State of Connecticut, through the Department of Environmental Protection, has agreed to cooperate with the Water Resources Division of the United States Geological Survey (USGS) to establish the Connecticut Atmospheric Deposition Monitoring Program.

### PROGRAM OBJECTIVES

The program is designed to collect and analyze precipitation on an event basis and has the following objectives:

- (1) to determine selected chemical and physical properties of precipitation in Connecticut;
- (2) to determine the spatial and temporal distribution of precipitation chemistry in the State;
- (3) to determine the relationships between precipitation chemistry and meteorological conditions, such as storm track and air mass movement;
- (4) to provide baseline information that can be used to determine trends and estimate loads; and
- (5) to use techniques and methodologies consistent with those of the national monitoring networks in order to provide comparative information.

### DATA COLLECTION SITES

Data collection sites have been established according to siting criteria used in the National Atmospheric Deposition Program (NADP). Use of these criteria ensures the validity of comparisons made between data which are collected through Connecticut's program and data from other atmospheric deposition programs. Other objectives considered during the siting process were the collection of samples representative of different geographic areas of the State, and the sampling of precipitation representative of long-range transport and not merely local sources. Using these criteria, precipitation sampling sites were established in the towns of Plainfield, Marlborough and Litchfield (Morris Dam). The locations of these sites are shown in Figure 17.

### EQUIPMENT

Each site is equipped with a Geo Filter automatic wet-dry sensing precipitation collector. This collector is the same type as those used by the NADP and the National Trends Network (NTN). The collector operates when precipitation wets an electronic sensor, completing an electrical circuit. This activates a motor that opens a lid over the sample container when the precipitation event begins and closes the lid when the precipitation ceases. The purpose of the lid is to retard the loss of samples through evaporation and to prevent contamination by dry fallout.

Each site is also equipped with an automatic rain gage which provides a record of the quantity of rain at 15-minute intervals.

In addition to the above equipment, a prototype precipitation quality monitor is being tested at the Plainfield site. Developed by the USGS Hydrologic Instrumentation Facility, the monitor consists of a wet-dry sensing precipitation collector fitted with a funnel in place of a collection container. Precipitation flows from the funnel through tubing to a series of sensors. The sensors continuously measure pH, temperature and specific conductance throughout a precipitation event and record the data at pre-selected intervals. Precipitation quantity is measured by a tipping-bucket type rain gage.

### DATA COLLECTION

Samples of precipitation are gathered from the automatic collectors as soon as possible following the end of a precipitation event, in most cases within 24 hours. The samples are immediately tested for acidity through pH measurements. The samples are also tested for specific conductance, which is a measure of the ions in solution -- the dissolved solids in solution -- which is a measure of the pollutant load. The results of this testing for the three precipitation sampling sites are tabulated from 1981 in Tables 28, 29 and 30. The results for 1985 are illustrated in Figures 18 through 26.

Samples from selected precipitation events are also sent to a USGS laboratory for further analyses to determine the concentrations of additional chemical constituents, including major anions, cations, nutrients and trace metals.

Through the Connecticut Atmospheric Deposition Monitoring Program, a network capable of providing uninterrupted baseline data on precipitation quality within the State has been developed. Data collected through the program is currently being published monthly by the USGS in its report, Water Resources Conditions in Connecticut. When using the data, one should note that it is specific only to the time and place of its collection.

### DISCUSSION OF DATA

Presently, data that has been collected in the initial stages of the study is being analyzed to determine, on a preliminary basis, the distribution and magnitude of atmospheric deposition in Connecticut. Because precipitation chemistry is a function of air quality and climate, both of which fluctuate over time and space, several more years of continuous data collection will be necessary to develop an adequate baseline to determine trends accurately and to more fully define the controlling processes. However, a preliminary evaluation of the data indicates that the precipitation occurring within Connecticut has been chemically affected by man-made contaminants. The data show that 24 32 percent of all the precipitation events studied to date have had a pH of 4.0 or below. Moreover, the yearly percentage of these low pH occurrences has increased significantly over the last three years from 23 20% in 1983 to 32% in 1985. Further evaluation of the data may provide more information on the source of the contaminants and the effects upon the environment.

It is important to stress that it is presently difficult to forecast statewide trends in the chemical properties of precipitation, or to perform comparative analyses, because of a lack of a large long-term data base. Generally, a 20-year or greater period of record is an acceptable statistical data base. When performing comparative analyses, some hydrologic data bases use 60 years or more of record keeping. Therefore, it should be apparent that data collection under the Connecticut Atmospheric Deposition Monitoring Program must continue until a sufficient period of record has been obtained.

Further information is available from the Water Resources Division, United States Geological Survey, 450 Main Street, Hartford, Connecticut 06103 at (203) 722-2528, or from the Natural Resources Center, Department of Environmental Protection, 165 Capitol Avenue, Hartford, Connecticut 06106 at (203) 566-3540.



### TABLE 28

## **ATMOSPHERIC DEPOSITION DATA FOR THE PLAINFIELD SITE**

| Event<br><u>Number</u>   | Period of Collection  | Specific<br><u>Conductance</u>   | рH  | Inches of<br>Precipitation   |
|--|---|--|---|--|
| 1<br>2<br>3<br>4<br>5<br>6   | 10/23/81 - 10/27/81<br>11/14/81 - 11/16/81<br>12/01/81 - 12/02/81<br>12/14/81<br>12/15/81 - 12/16/81<br>12/27/81 - 12/28/81   | 15<br>15<br>14<br>12<br>12<br>51   | 4.5<br>4.5<br>4.4<br>4.6<br>4.0   | 2.30<br>1.01<br>2.68<br>0.58<br>2.90<br>0.20   |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10  | 01/04/82 - 01/05/82<br>04/26/82 - 04/27/82<br>05/29/82 - 05/31/82<br>06/02/82<br>06/04/82 - 06/06/82<br>07/28/82 - 07/29/82<br>08/09/82<br>08/09/82<br>11/28/82 - 11/29/82<br>12/16/82  | 15<br>11<br>18<br>5<br>10<br>18<br>25<br>31<br>8<br>16   | 4.8<br>4.4<br>5.0<br>5.1<br>4.4<br>4.2<br>4.8<br>4.9  | 2.70<br>0.99<br>1.43<br>2.86<br>4.28<br>0.11<br>0.96<br>0.71<br>0.98<br>0.85   |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9<br>10<br>11<br>12<br>13<br>14<br>15<br>16<br>17<br>18<br>9<br>20<br>21<br>22<br>23 | 01/05/83 - 01/06/83<br>01/13/83<br>01/22/83 - 01/24/83<br>01/29/83 - 01/31/83<br>02/03/83<br>02/06/83 - 02/07/83<br>02/11/83 - 02/12/83<br>03/02/83<br>03/02/83<br>03/06/83 - 03/09/83<br>03/19/83 - 03/21/83<br>03/27/83 - 03/28/83<br>04/03/83<br>04/10/83<br>04/10/83<br>04/10/83<br>04/16/83 - 04/17/83<br>04/19/83 - 04/20/83<br>04/24/83<br>05/31/83<br>06/04/83<br>06/27/83 - 06/28/83<br>07/06/83<br>07/22/83<br>07/25/83 | 15<br>18<br>8<br>26<br>14<br>13<br>6<br>17<br>26<br>47<br>20<br>22<br>32<br>13<br>16<br>13<br>15<br>30<br>41<br>68<br>27<br>79<br>38 | 4.4<br>4.7<br>4.9<br>4.2<br>4.7<br>4.9<br>4.5<br>4.2<br>4.5<br>4.2<br>4.5<br>4.2<br>4.5<br>4.2<br>4.5<br>4.2<br>4.5<br>4.2<br>4.5<br>4.2<br>4.5<br>4.2<br>4.5<br>4.2<br>4.5<br>4.2<br>4.5<br>4.2<br>4.5<br>4.2<br>4.5<br>4.2<br>4.5<br>4.5<br>4.2<br>4.5<br>4.5<br>4.5<br>4.5<br>4.5<br>4.5<br>4.5<br>4.5<br>4.5<br>4.5 | 0.49<br>0.78<br>1.17<br>0.36<br>1.21<br>0.44<br>0.04<br>1.09<br>0.37<br>1.37<br>1.91<br>1.11<br>0.02<br>2.37<br>0.96<br>2.84<br>2.42<br>1.47<br>0.99<br>1.22<br>0.38<br>0.25<br>0.29 |
| 24<br>25   | 08/11/83 - 08/12/83<br>09/12/83   | 39<br>87   | 4.0<br>3.7  | 1.60<br>0.54   |

## **TABLE 28, CONTINUED**

| Event    |                                 | Specific           |            | Inches of            |
|----------|---------------------------------|--------------------|------------|----------------------|
| Number   | Period of Collection            | <u>Conductance</u> | <u>pH</u>  | <b>Precipitation</b> |
| 26       | 09/23/83                        | 14                 | 4.7        | 0.95                 |
| 27       | 10/01/83 - 10/02/83             | 17                 | 4.4        | 1.33                 |
| 28       | 10/12/83 - 10/13/83             | 4                  | 5.4        | 1.10                 |
| 29       | 10/18/83                        | 45                 | 4.0        | 0.28                 |
| 3U<br>21 | 10/23/83 - 10/25/83             | 8                  | 4.8        | 1.15                 |
| 20       | 11/03/83 - 11/04/83             | 30                 | 4.2        | 0.60                 |
| 32       | 11/15/92 11/16/93               | 17                 | 4.4        | 1.08                 |
| 33       | 11/0/03 - 11/10/03              | 8                  | 4.8        | 2.46                 |
| 35       | 11/21/03                        | 14<br>E            | 4.6        | 0.69                 |
| 36       | 11/28/83 - 11/29/83             | 25                 | 5.2<br>4.3 | 2.89<br>0.97         |
| 1        | 01/10/84 - 01/11/84             | 24                 | 4.2        | 0.81*                |
| 2        | 01/18/84 - 01/19/84             | 52                 | 4.1        | 0.30*                |
| 3        | 01/24/84                        | 25                 | 4.3        | 0.32                 |
| 4        | 02/03/84 - 02/05/84             | 24                 | 4.3        | 1.47                 |
| 5        | 02/11/84                        | 37                 | 4.1        | 0.30                 |
| 6        | 02/14/84 - 02/18/84             | 37                 | 4.9        | 1.58                 |
| /        | 02/24/84 - 02/25/84             | 25                 | 4.4        | 0.81                 |
| 8        | 02/28/84 - 03/01/84             | 11                 | 4.6        | 1.88                 |
| 9        | 03/05/84                        | 54                 | 3.9        | 0.40                 |
| 10       | 03/13/84 - 03/14/84             | 20                 | 4.2        | 1.24                 |
| 12       | 03/16/64 - 03/19/84             | 11                 | 4.5        | 0.42                 |
| 12       | 02/22/04                        | 22                 | 4.3        | 0.58                 |
| 14       | 03/20/04 - 03/30/04             | 10                 | 4.8        | 1.03                 |
| 15       | 04/05/04<br>04/14/84 = 04/15/84 | 21                 | 4.0        | 1.96                 |
| 16       | 04/23/84 = 04/23/84             | 2 I<br>6 2         | 4.5        | 0.07                 |
| 17       | 05/03/84 - 05/04/84             | 02<br>/ Q          | 5.9        | 0.12                 |
| 18       | 05/08/84                        | 40                 | 4.0        | 1.05                 |
| 19       | 05/12/84 - 05/14/84             | 62                 | 30         | 0.42                 |
| 20       | 05/19/84 - 05/21/84             | 69                 | 3.5        | 1.05                 |
| 21       | 05/27/84 - 05/31/84             | 21                 | 43         | 5.85                 |
| 22       | 05/31/84 - 06/03/84             | 8                  | 4.8        | 0.88                 |
| 23       | 06/19/84                        | 71                 | 3.8        | 0.49                 |
| 24       | 06/24/84                        | 16                 | 4.5        | 0.52                 |
| 25       | 06/27/84 - 06/29/84             | 51                 | 4.0        | 0.75                 |
| 26       | 07/09/84                        | 14                 | 4.5        | 3.50                 |
| 27       | 07/16/84                        | 54                 | 3.9        | 0.62                 |
| 28       | 07/19/834                       | 36                 | 4.0        | 1.07                 |
| 29       | 07/23/84                        | 8                  | 5.0        | 1.08                 |
| 30       | 07/27/84                        | 45                 | 4.0        | 0.41                 |
| 31       | 09/04/84                        | 50                 | 3.9        | 0.66                 |
| 32       | 09/12/84                        | 39                 | 4.1        | 0 19                 |

\* Water equivalent of snowfall

( )

## **TABLE 28, CONTINUED**

| Period of Collection | Specific<br>Conductance  | рH   | Inches of<br>Precipitation   |
|----------------------|--|--|--|
|                      |  | <u> <u> </u></u>   |  |
| 09/15/84             | 31   | 4.2  | 1.07   |
| 10/01/84 - 10/02/84  | 12   | 4.6  | 2.31   |
| 10/22/84 - 10/23/84  | 17   | 4.5  | 1 67   |
| 10/23/84 - 10/24/84  | 25   | 4.4  | 0.15   |
| 10/26/84 - 10/29/84  | 38   | 4.0  | 1.22   |
| 11/05/84             | 6  | 5.0  | 0 55   |
| 11/11/84             | 8  | 4.8  | 1.79   |
| 11/15/84             | 55   | 4.0  | 0.18   |
| 11/29/84             | 17   | 4.7  | 0 42   |
| 12/03/84             | 21   | 4.4  | 0.65   |
| 12/05/84 - 12/06/84  | 10   | 4.7  | 1.19*  |
| 12/19/84             | 40   | 4.1  | 0 33   |
| 12/21/84 - 12/22/84  | 47   | 4.0  | 0.91*  |
| 01/01/85 - 01/02/85  | 32   | 4.1  | 0.40   |
| 01/04/85 - 01/05/85  | 73   | 4.1  | 0.23*  |
| 01/08/85             | 34   | 4.2  | 0.99*  |
| 01/17/85             | 40   | 4.4  | 0.19*  |
| 01/19/85 - 01/20/85  | 54   | 4.0  | 0.06*  |
| 02/01/85 - 02/02/85  | 31   | 4.2  | 1.88*  |
| 02/05/85 - 02/06/85  | 23   | 4.3  | 2.01*  |
| 03/04/85 - 03/05/85  | 53   | 4.0  | 3.67*  |
| 03/07/85 - 03/08/85  | 35   | 4.1  | 0.39   |
| 03/12/85             | 32   | 4.2  | 1.09   |
| 03/18/85 - 03/19/85  | 82   | 3.9  | 0.11   |
| 03/31/85 - 04/01/85  | 32   | 4.2  | 0.53   |
| 04/07/85 - 04/08/85  | 32   | 4.3  | 0.32   |
| 04/14/85 - 04/15/85  | 96   | 3.8  | 0.03   |
| 04/22/85             | 70   | 3.8  | 0.05   |
| 04/26/85 - 04/28/85  | 135  | 3.6_   | 0.10   |
| 05/02/85 - 05/06/85  | 25   | 4.4  | 2.31   |
| 05/18/85 - 05/19/85  | 11   | 5.1  | 0.06   |
| 05/27/85 - 05/28/85  | 20   | 4.4  | 1.31   |
| 06/01/85             | 14   | 4.6  | 0.39   |
| 06/05/85             | 24   | 4.3  | 0.80   |
| 06/08/85             | 98   | 3.7  | 0.06   |
| 06/16/85 - 06/17/85  | 37   | 4.1  | 1.15   |
| 06/24/85             | 36   | 4.1  | 0.39   |
| 06/25/85 - 06/29/85  | 15   | 4.5  | 1.15   |
| 07/03/85             | 93   | 3.7  | 0.16   |
| 07/06/85 - 07/07/85  | 41   | 4.1  | 0.25   |
| 07/09/85             | 74   | 3.7  | 0.33   |
| 07/12/85 - 07/14/85  | 113  | 3.6  | 0.35   |
| 07/15/85             | 59   | 3.9  | 0.35   |
|                      | Period of Collection<br>09/15/84<br>10/01/84 - 10/02/84<br>10/22/84 - 10/23/84<br>10/23/84 - 10/24/84<br>10/26/84 - 10/29/84<br>11/05/84<br>11/15/84<br>11/15/84<br>12/03/84<br>12/03/84<br>12/05/84 - 12/06/84<br>12/19/84<br>12/21/84 - 12/22/84<br>01/01/85 - 01/02/85<br>01/04/85 - 01/05/85<br>01/04/85 - 01/02/85<br>01/04/85 - 01/02/85<br>01/04/85 - 01/02/85<br>01/04/85 - 01/02/85<br>01/04/85 - 01/02/85<br>01/04/85 - 01/02/85<br>02/01/85 - 02/02/85<br>02/01/85 - 02/02/85<br>02/01/85 - 02/02/85<br>03/04/85 - 03/08/85<br>03/07/85 - 03/08/85<br>03/12/85<br>03/12/85<br>03/18/85 - 03/19/85<br>03/11/7/85<br>04/07/85 - 04/01/85<br>04/07/85 - 04/01/85<br>04/07/85 - 04/15/85<br>04/14/85 - 04/15/85<br>04/22/85<br>04/26/85 - 04/28/85<br>05/02/85 - 05/06/85<br>05/18/85 - 05/19/85<br>05/27/85 - 05/28/85<br>06/01/85<br>06/05/85<br>06/01/85<br>06/024/85<br>06/024/85<br>06/24/85<br>07/03/85<br>07/06/85 - 07/07/85<br>07/09/85<br>07/12/85 - 07/14/85<br>07/12/85 - 07/14/85<br>07/12/85 - 07/14/85 | Period of Collection Specific<br>Conductance   09/15/84 31   10/01/84 - 10/02/84 12   10/22/84 - 10/23/84 17   10/23/84 - 10/24/84 25   10/26/84 - 10/29/84 38   11/05/84 6   11/11/84 8   11/15/84 55   11/29/84 17   12/03/84 21   12/05/84 - 12/06/84 10   12/19/84 40   12/21/84 - 12/22/84 47   01/01/85 - 01/02/85 32   01/04/85 - 01/02/85 32   01/04/85 - 01/02/85 31   02/05/85 - 02/06/85 23   03/04/85 - 03/05/85 33   03/04/85 - 03/05/85 32   03/12/85 32   03/18/85 - 04/15/85 32   03/18/85 - 04/15/85 32   03/18/85 - 04/15/85 32   03/18/85 - 05/19/85 135   05/02/85 - 04/28/85 135   05/02/85 - 05/28/85 25   05/18/85 - 06/17/85 37< | Period of Collection Specific<br>Conductance pH   09/15/84 31 4.2   10/01/84 - 10/02/84 12 4.6   10/22/84 - 10/23/84 17 4.5   10/23/84 - 10/24/84 25 4.4   10/26/84 - 10/29/84 38 4.0   11/05/84 6 5.0   11/11/84 8 4.8   11/15/84 17 4.7   12/03/84 17 4.7   12/03/84 21 4.4   12/05/84 - 12/06/84 10 4.7   12/21/84 12/22/84 47 4.0   01/01/85 - 01/02/85 32 4.1   01/04/85 - 01/20/85 34 4.2   01/17/85 40 4.4   01/19/85 - 01/20/85 53 4.0   02/01/85 - 02/02/85 31 4.2   01/17/85 40 4.4   01/19/85 - 03/08/85 35 4.1   03/07/85 - 03/08/85 35 4.1   03/12/85 - 03/19/85 82 |

## TABLE 28, CONTINUED

| Event<br><u>Number</u> | Period of Collection | Specific<br><u>Conductance</u> | <u>pH</u> | Inches of<br>Precipitation |
|------------------------|----------------------|--------------------------------|-----------|----------------------------|
| 31                     | 07/21/85             | 80                             | 3.8       | 1 62                       |
| 32                     | 07/26/85 - 07/27/85  | 20                             | 4.3       | 1 30                       |
| 33                     | 07/31/85 - 08/01/85  | 65                             | 3.8       | 2 19                       |
| 34                     | 08/07/85 - 08/08/85  | 29                             | 4.1       | 0.24                       |
| 35                     | 08/15/85             | 74                             | 3.8       | 0.11                       |
| 36                     | 08/25/85 - 08/26/85  | 13                             | 4.4       | 1.51                       |
| 37                     | 08/30/85 - 08/31/85  | 49                             | 3.9       | 1 30                       |
| 38                     | 09/04/85 - 09/05/85  | 58                             | 3.9       | 0.66                       |
| 39                     | 09/06/85 - 09/08/85  | 43                             | 4.0       | 0.99                       |
| 40                     | 09/09/85 - 09/10/85  | 77                             | 3.8       | 0.44                       |
| 41                     | 09/24/85             | 6                              | 5.4       | 0.41                       |
| 42                     | 10/03/85 - 10/04/85  | 87                             | 3.9       | 0.26                       |
| 43                     | 10/05/85             | 21                             | 4.4       | 0.53                       |
| 44                     | 10/13/85 - 10/15/85  | 51                             | 4.1       | 0.41                       |
| 45                     | 10/19/85             | 99                             | 3.6       | 0.19                       |
| 46                     | 10/25/85             | 13                             | 4.6       | 0.22                       |
| 47                     | 11/05/85 - 11/06/85  | 9                              | 4.7       | 2.61                       |
| 48                     | 11/11/85 - 11/12/85  | 44                             | 4.0       | 0.75                       |
| 49                     | 11/14/85             | 50                             | 4.0       | 0.19                       |
| 50                     | 11/16/85 - 11/17/85  | 6                              | 4.8       | 1.23                       |
| 51                     | 11/22/85 - 11/24/85  | 29                             | 4.2       | 0.56                       |
| 52                     | 11/26/85 - 11/27/85  | 35                             | 4.1       | 0.68                       |
| 53                     | 11/28/85 - 11/30/85  | 28                             | 4.2       | 0.82                       |
| 54                     | 12/11/85             | 54                             | 3.9       | 0.50                       |
| 55                     | 12/13/85             | 29                             | 4.3       | 0.14                       |
| 56                     | 12/20/85 - 12/23/85  | 46                             | 4.0       | 0.70*                      |

### TABLE 29

## ATMOSPHERIC DEPOSITION DATA FOR THE MORRIS DAM SITE

| Event         |                      | Specific    |     | Inches of     |
|---------------|----------------------|-------------|-----|---------------|
| <u>Number</u> | Period of Collection | Conductance | Нq  | Precipitation |
|               |                      |             |     |               |
| 1             | 12/16/82             | 22          | 4.5 | 1.18          |
| 1             | 01/05/83 - 01/06/83  | 18          | 4.4 | 0 64          |
| 2             | 01/10/83 - 01/11/83  | 6           | 4.9 | 2.39          |
| 3             | 01/23/83             | 13          | 4.5 | 1.45          |
| 4             | 02/02/83 - 02/03/83  | 19          | 4.4 | 1.89          |
| 5             | 02/06/83 - 02/07/83  | 50          | 4.0 | 0.45*         |
| 6             | 02/11/83 - 02/12/83  | 9           | 4.9 | 1.30*         |
| 7             | 02/17/83             | 46          | 4.0 | 0.21          |
| 8             | 03/02/83             | 22          | 4.3 | 0.27          |
| 9             | 03/07/83 - 03/09/83  | 37          | 4.1 | 1.22          |
| 10            | 03/19/83 - 03/21/83  | 14          | 4.5 | 1.29          |
| 11            | 03/27/83 - 03/28/83  | 18          | 4.4 | 1.29          |
| 12            | 04/03/83             | 11          | 4.7 | 1.07          |
| 13            | 04/10/83             | 9           | 4.6 | 2.70          |
| 14            | 04/16/83 - 04/17/83  | 10          | 4.5 | 2.61          |
| 15            | 04/19/83 - 04/20/83  | 23          | 4.3 | 1.27          |
| 16            | 04/24/83             | 16          | 4.5 | 1.35          |
| 17            | 05/15/83 - 05/16/83  | 35          | 4.1 | 0.87          |
| 18            | 05/29/83 - 05/30/83  | 39          | 4.1 | 0.81          |
| 19            | 06/04/83             | 49          | 3.9 | 1.39          |
| 20            | 06/28/83             | 58          | 3.9 | 1.71          |
| 21            | 07/05/83             | 67          | 3.9 | 1.54          |
| 22            | 07/25/83             | 46          | 4.1 | 0.75          |
| 23            | 08/11/83 - 08/12/83  | 49          | 3.9 | 1.60          |
| 24            | 09/12/83             | 65          | 3.8 | 0.24          |
| 25            | 09/23/83             | 20          | 4.5 | 0.94          |
| 26            | 10/01/83 - 10/02/83  | 9           | 4.6 | 1.18          |
| 27            | 10/12/83 - 10/13/83  | 6           | 4.9 | 3.34          |
| 28            | 10/18/83             | 30          | 4.1 | 0.33          |
| 29            | 10/23/83 - 10/25/83  | 9           | 4.8 | 2.32          |
| 30            | 11/03/83 - 11/04/83  | 80          | 3.8 | 0.11          |
| 31            | 11/10/83             | 40          | 4.2 | 0.94          |
| 32            | 11/15/83 - 11/16/83  | 10          | 4.6 | 1.64          |
| 33            | 11/21/83             | 14          | 4.6 | 0.57          |
| 34            | 11/24/83 - 11/25/83  | 21          | 4.5 | 1.45          |
| 35            | 11/28/83 - 11/29/83  | 24          | 4.3 | 0.71          |
| 30            | 12/06/83             | 32          | 4.2 | 1.04          |
| 3/            | 12/12/83 - 12/14/83  | 26          | 4.5 | 3.41          |
| 1             | 01/10/84 - 01/11/84  | 12          | 4.5 | 0.47*         |

## TABLE 29, CONTINUED

| Event         |                      | Specific           |            | Inches of     |
|---------------|----------------------|--------------------|------------|---------------|
| <u>Number</u> | Period of Collection | <u>Conductance</u> | <u>pH</u>  | Precipitation |
| 2             | 01/18/84 - 01/19/84  | 45                 | 4.0        | 0.21*         |
| 3             | 01/24/84             | 34                 | 4.0        | 0.21          |
| 4             | 01/30/84 - 01/31/84  | 22                 | 43         | 0.43          |
| 5             | 02/03/84 - 02/05/84  | 41                 | 4.0        | 0.69          |
| 6             | 02/11/84             | 43                 | 4.0        | 0.48          |
| 7             | 02/14/84 - 02/16/84  | 23                 | 4.7        | 1.53          |
| 8             | 02/24/84 - 02/25/84  | 80                 | 3.8        | 0.86          |
| 9             | 02/28/84 - 03/01/84  | 10                 | 4.6        | 1.34          |
| 10            | 03/05/84 - 03/06/84  | 25                 | 4.2        | 0.53          |
| 11            | 03/18/84 - 03/19/84  | 30                 | 4.1        | 0.52          |
| 12            | 03/21/84             | 24                 | 4.3        | 0.65          |
| 13            | 03/28/84 - 03/30/84  | 10                 | 4.8        | 1.61*         |
| 14            | 04/05/84             | 25                 | 4.4        | 2.79          |
| 15            | 04/13/04 - 04/10/84  | 32                 | 4.2        | 1.25          |
| 17            | 04/23/84 - 04/24/84  | 1/                 | 4.0        | 0.55          |
| 18            | 05/08/84             | 20                 | 4.2        | 1.24          |
| 19            | 05/12/84 - 05/14/84  | 54<br>55           | 4.2        | 0.99          |
| 20            | 05/19/84 - 05/21/84  | 78                 | 3.3        | 0.77          |
| 21            | 05/25/84             | 19                 | ΔΔ         | 0.21          |
| 22            | 05/27/84 - 05/31/84  | 13                 | 45         | 6 11          |
| 23            | 05/31/84 - 06/03/84  | 5                  | 5.0        | 0.74          |
| 24            | 06/24/84 - 06/25/84  | 20                 | 4.3        | 0.87          |
| 25            | 06/27/84 - 07/01/84  | 39                 | 4.0        | 0.60          |
| 26            | 07/09/84             | 24                 | 4.2        | 0.23          |
| 27            | 07/16/84             | 62                 | 3.9        | 0.71          |
| 28            | 07/19/84             | 52                 | 4.0        | 0.53          |
| 29            | 07/27/84             | 18                 | 4.4        | 0.70          |
| 30            | 09/04/84             | 50                 | 3.9        | 0.80          |
| 31            | 09/12/84             | 20                 | 4.4        | 0.22          |
| 32            | 10/01/84 - 10/02/84  | 8                  | 4.8        | 0.51          |
| 27            | 10/22/84 - 10/23/84  | 20                 | 4.4        | 0.91          |
| 34            | 10/25/64 - 10/24/64  | 55                 | 4.4        | 0.07          |
| 36            | 11/05/84             | 01                 | 3.8<br>E 0 | 0.63          |
| 37            | 11/29/84             | 0<br>15            | 5.0        | 0.96          |
| 38            | 12/03/84             | 33                 | 4.0        | 0.54          |
| 39            | 12/05/84 - 12/06/84  | 10                 | 5.0        | 0.54          |
| 40            | 12/19/84             | 39                 | 4 1        | 0.40          |
| 41            | 12/21/84 - 12/22/84  | 46                 | 3.9        | 0.33          |
| 1             | 01/01/85 - 01/02/85  | 31                 | 4.1        | 0.28          |
| 2             | 01/08/85             | 24                 | 4.3        | 0.10*         |
| 3             | 01/17/85             | 11                 | 4.7        | 0.29*         |

## **TABLE 29, CONTINUED**

| Event   |                      | Specific           |            | Inches of            |
|---------|----------------------|--------------------|------------|----------------------|
| Number  | Period of Collection | <u>Conductance</u> | <u>pH</u>  | <b>Precipitation</b> |
| 4       | 01/19/85 - 01/20/85  | 66                 | 4.1        | 0.13*                |
| 5       | 01/31/85             | 57                 | 3.9        | 0.05*                |
| 6       | 02/01/85 - 02/02/85  | 31                 | 4.2        | 0.30*                |
| /       | 02/05/85 - 02/06/85  | 28                 | 4.2        | 0.64*                |
| 8       | 02/12/85             | 14                 | 4.5        | 1.38                 |
| 9<br>10 | 03/04/85 - 03/05/85  | 60                 | 3.9        | 0.69*                |
| 11      | 03/31/85 - 04/01/85  | 30                 | 4.2        | 1.23                 |
| 12      | 04/07/85 - 04/08/85  | 30<br>15           | 4.1        | 0.30                 |
| 13      | 04/14/85 - 04/15/85  | 40<br>50           | 4.1        | 0.30                 |
| 14      | 04/19/85             | 27                 | 4.1        | 0.00                 |
| 15      | 04/22/85             | 53                 | 4.0        | 0.10                 |
| 16      | 04/26/85 - 04/28/85% | 38                 | 3.6        | 0.04                 |
| 17      | 05/02/85 - 05/06/85  | 25                 | 4.3        | 2.37                 |
| 18      | 05/18/85 - 05/19/85  | 16                 | 4.6        | 0.30                 |
| 19      | 05/27/85 - 05/28/85  | 21                 | 4.4        | 1.56                 |
| 20      | 06/01/85             | 16                 | 4.5        | 1.20                 |
| 21      | 06/05/85             | 25                 | 4.3        | 0.77                 |
| 22      | 06/12/95             | /1                 | 3.9        | 0.22                 |
| 23      | 06/16/95 06/17/95    | 55                 | 3.9        | 0.21                 |
| 25      | 06/18/85             | 28                 | 4.2        | 1.02                 |
| 26      | 06/24/85             | 96                 | 3.9<br>27  | 0.07                 |
| 27      | 06/25/85 - 06/29/85  | 27                 | 4.2        | 0.11                 |
| 28      | 07/03/85             | 80                 | 37         | 0.25                 |
| 29      | 07/06/85 - 07/07/85  | 30                 | 4.2        | 0.47                 |
| 30      | 07/09/85             | 65                 | 3.8        | 0.29                 |
| 31      | 07/12/85 - 07/14/85  | 67                 | 3.8        | 0.77                 |
| 32      | 07/15/85             | 83                 | 3.8        | 0.15                 |
| 33      | 07/21/85             | 108                | 3.7        | 1.44                 |
| 34      | 0//26/85 - 0//27/85  | 21                 | 4.3        | 1.27                 |
| 33      | 07/31/85-08/01/85    | 90                 | 3.7        | 1.35                 |
| 30      | 00/11/00             | /0                 | 3.8        | 0.19                 |
| 38      | 08/30/85 - 08/31/85  | 17                 | 4.2        | 2.48                 |
| 39      | 09/04/85 - 09/05/85  | 22                 | 5.0<br>12  | 0.54                 |
| 40      | 09/06/85 - 09/08/85  | 22                 | 4.5        | 1.03                 |
| 41      | 09/09/85 - 09/10/85  | 33                 | 4.J<br>4 1 | 1.36                 |
| 42      | 09/24/85             | 8                  | 4.9        | 0.54                 |
| 43      | 09/27/85             | 12                 | 5.0        | 3.68                 |
| 44      | 10/03/85 - 10/04/85  | 35                 | 4.1        | 0.47                 |
| 45      | 10/05/85             | 32                 | 4.1        | 1.30                 |
| 46      | 10/13/85 - 10/15/85  | 68                 | 3.8        | 0.36                 |
| 47      | 10/19/85             | 89                 | 3.7        | 0.11                 |
### TABLE 29, CONTINUED

| Event<br><u>Number</u> | Period of Collection  | Specific<br><u>Conductance</u> | <u>pH</u> | Inches of<br>Precipitation |
|------------------------|-----------------------|--------------------------------|-----------|----------------------------|
| 48                     | 10/25/85              | 10                             |           | 0.27                       |
| 49                     | 11/05/85 - 11/06/95   | 15                             | 4.4       | 0.27                       |
|                        | 11/05/05 - 11/00/05   | 0                              | 4.9       | 1.06                       |
| 50                     | 1 1/1 1/85 - 11/12/85 | 43                             | 4.0       | 1.01                       |
| 51                     | 11/14/85              | 54                             | 4.0       | 0.41                       |
| 52                     | 11/16/85 - 11/17/85   | 7                              | 47        | 1 40                       |
| 53                     | 11/22/85 - 11/24/85   | 13                             | 45        | 0.31                       |
| 54                     | 11/26/85 - 11/27/85   | 53                             | 3 9       | 0.51                       |
| 55                     | 11/28/85 - 11/30/85   | 10                             | 1.5       | 0.70                       |
| 56                     | 10/10/05              | 19                             | 4.5       | 0.97                       |
| 50                     | 12/13/85              | 24                             | 4.3       | 0.21                       |
| 57                     | 12/20/85 - 12/23/85   | 41                             | 4.1       | 0.39*                      |

### **ATMOSPHERIC DEPOSITION DATA FOR THE MARLBOROUGH SITE**

| Event  | Deviad of Collection                       | Specific    |           | Inches of     |
|--------|--|-------------|-----------|---------------|
| Number | Period of Collection                       | Conductance | <u>pH</u> | Precipitation |
| 1      | 05/29/83 - 05/31/83                        | 36          | 4.1       | 1.39          |
| 2      | 06/04/83                                   | 42          | 4.1       | 0.99          |
| 3      | 06/27/83 - 06/28/83                        | 75          | 3.8       | 2.63          |
| 4      | 07/05/83 - 07/06/83                        | 89          | 3.7       | 0.27          |
| 5      | 07/21/83                                   | 46          | 4.0       | 0.39          |
| 07     | 09/11/22 00/12/02                          | 40          | 4.0       | 0.91          |
| 2<br>2 | 00/12/02                                   | 27          | 4.2       | 1.75          |
| Ğ      | 03/23/03<br>10/01/82 10/03/93              | 11          | 4./       | 1.18          |
| 10     | 10/07/83 - 10/02/83                        | 5<br>10     | 4.8       | 2.22          |
| 11     | 10/18/83                                   | 20          | 4.0       | 1.22          |
| 12     | 10/23/83 - 10/24/83                        | Σ<br>Δ      | 4.2       | 1 07          |
| 13     | 11/03/83 - 11/04/83                        | 38          | 4.0       | 0.75          |
| 14     | 11/10/83                                   | 20          | 4.4       | 1 27          |
| 15     | 11/15/83 - 11/16/83                        | 6           | 4.9       | 1.73          |
| 16     | 11/21/83                                   | 12          | 4.7       | 0.49          |
| 17     | 11/24/83 - 11/25/83                        | 7           | 4.9       | 2.43          |
| 18     | 11/28/83 - 11/29/83                        | . 21        | 4.4       | 1.04          |
| 19     | 12/06/83                                   | 30          | 4.3       | 0.68          |
| 20     | 12/12/83 - 12/14/83                        | 40          | 4.6       | 1.89          |
| 1      | 01/10/84 - 01/11/84                        | 7           | 4.7       | 0.77*         |
| 2      | 01/18/84 - 01/19/84                        | 38          | 4.1       | 0.62*         |
| 3      | 01/24/84                                   | 23          | 4.4       | 0.18          |
| 4      | 01/30/84 - 01/31/84                        | 36          | 4.1       | 0.64*         |
| 5      | 02/03/84 - 02/05/84                        | 28          | 4.2       | 0.83          |
| 7      | 02/11/84                                   | 50          | 3.9       | 0.20          |
| 8      | 02/14/04 - 02/10/04                        | 16          | 4.9       | 0.83          |
| ğ      | 02/24/84 = 02/23/84<br>02/28/84 = 03/01/84 |             | 4.5       | 1.20          |
| 10     | 03/04/84 - 03/06/84                        | 26          | 4.0       | 1.57          |
| 11     | 03/13/84 - 03/14/84                        | 10          | 4.2       | 0.20          |
| 12     | 03/18/84 - 03/19/84                        | 48          | 39        | 0.27          |
| 13     | 03/21/84                                   | 15          | 4.4       | 0.47          |
| 14     | 03/28/84 - 03/30/84                        | 6           | 5.0       | 0.44*         |
| 15     | 04/05/84                                   | 25          | 4.4       | 2.47          |
| 16     | 04/13/84 - 04/16/84                        | 20          | 4.4       | 2.12          |
| 17     | 04/23/84 - 04/24/84                        | 15          | 4.6       | 0.52          |
| 18     | 05/03/84 - 05/04/84                        | 34          | 4.1       | 1.37          |
| 19     | 05/08/84                                   | 35          | 4.1       | 0.48          |
| 20     | U5/12/84 - 05/14/84                        | 44          | 40        | 0.57          |

### TABLE 30, CONTINUED

| Event    |  | Specific           |            | Inches of            |
|----------|--|--------------------|------------|----------------------|
| Number   | Period of Collection                       | <u>Conductance</u> | рH         | <b>Precipitation</b> |
|          |  |                    |            |                      |
| 21       | 05/19/84 - 05/21/84                        | 60                 | 39         | 0.41                 |
| 22       | 05/25/84                                   | 18                 | 44         | 0.50                 |
| 23       | 05/27/84 - 05/31/84                        | 16                 | 4.5        | 6 35*                |
| 24       | 05/31/84 - 06/02/84                        | 7                  | 4.8        | 1.46                 |
| 25       | 06/19/84                                   | 57                 | 3.9        | 0.12                 |
| 26       | 06/25/84                                   | 11                 | 4.9        | 1.73                 |
| 27       | 06/28/84 - 06/29/84                        | 63                 | 3.9        | 0.21                 |
| 28       | 07/07/84                                   | 13                 | 4.5        | 4.18                 |
| 29       | 07/16/84                                   | 88                 | 3.8        | 0.15                 |
| 30       | 07/18/84 - 07/19/84                        | 26                 | 4.3        | 1.09                 |
| 31       | 07/21/84 - 07/22/84                        | 4                  | 5.1        | 1.35                 |
| 32       | 07/27/84                                   | 32                 | 4.2        | 0.57                 |
| 33       | 09/04/84                                   | 39                 | 4.1        | 3.91                 |
| 34<br>25 | 09/15/84                                   | 30                 | 4.3        | 1.04                 |
| 33       | 10/01/84 - 10/02/84                        | 7                  | 4.8        | 1.96                 |
| 27       | 10/22/84 - 10/23/84                        | 18                 | 4.4        | 2.41                 |
| 38       | 10/25/04 - 10/24/84                        | 33                 | 4.3        | 0.13                 |
| 30       | 11/05/94                                   | 39                 | 4.0        | 1.32                 |
| 40       | 11/11/9/                                   | 8<br>C             | 4.9        | 0.52                 |
| 40       | 11/15/84                                   | 64                 | 5.0        | 1.93                 |
| 42       | 12/03/84                                   | 04<br>22           | 3.9        | 0.10                 |
| 43       | 12/05/84 - 12/06/84                        | 22<br>6            | 4.5        | 0.50                 |
| 44       | 12/19/84                                   | 42                 | 4.9        | 1.19"                |
| 45       | 12/21/84 - 12/22/84                        | 59                 | 4.0<br>3.8 | 0.50                 |
|          |  |                    | 5.0        | 0.54                 |
| 1        | 01/01/85 - 01/02/85                        | 28                 | 4.1        | 0.33                 |
| 2        | 01/04/85 - 01/05/85                        | 38                 | 4.1        | 0.20*                |
| 3        | 01/08/85                                   | 28                 | 4.2        | 0.12*                |
| 4        | 01/17/85                                   | 11                 | 4.7        | 0.11*                |
| 5        | 01/19/85 - 01/20/85                        | 70                 | 3.8        | 0.41*                |
| 6        | 01/31/85                                   | 50                 | 4.0        | 0.10*                |
| /        | 02/01/85 - 02/02/85                        | 22                 | 4.3        | 0.45*                |
| 8        | 02/05/85 - 02/06/85                        | 18                 | 4.3        | 0.59*                |
| 9        | 02/12/85                                   | 13                 | 4.6        | 1.27                 |
| 10       | 03/04/85 - 03/05/85                        | 53                 | 4.0        | 0.83*                |
| 17       | 03/07/85 - 03/08/85                        | 41                 | 4.0        | 0.34                 |
| 13       | 03/12/03<br>03/19/95 03/10/95              | 20                 | 4.2        | 1.19                 |
| 14       | 03/21/25 04/01/05                          | 49                 | 4.0        | 0.15                 |
| 15       | 03/31/03 - 04/01/03<br>04/07/85 - 04/00/05 | 20                 | 4.3        | 0.60                 |
| 16       | 04/07/03 - 04/00/03<br>04/14/85 - 04/15/95 | 41                 | 4.2        | 0.33                 |
| 17       | 04/19/85                                   | 60                 | 3.9        | 0.05                 |
| 18       | 04/22/85                                   | 00                 | 5.9<br>1 1 | 0.10                 |
|          | J-7/22/03                                  | 42                 | 4.1        | 0.70                 |

### **TABLE 30, CONTINUED**

| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | Event<br><u>Number</u> | Period of Collection | Specific<br><u>Conductance</u> | <u>pH</u>  | Inches of<br>Precipitation |
|--|------------------------|----------------------|--------------------------------|------------|----------------------------|
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 19                     | 04/26/85 - 04/28/85  | 59                             | 3.5        | 0.13                       |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 20                     | 05/02/85 - 05/06/85  | 26                             | 4.3        | 2.55                       |
| 22 $05/27/85 - 05/28/85$ 264.3 $1.95$ 23 $06/01/85$ 234.4 $0.51$ 24 $06/05/85$ 314.2 $0.85$ 25 $06/08/85$ 733.8 $0.29$ 26 $06/12/85 - 06/17/85$ 184.4 $1.67$ 28 $06/18/85 - 06/17/85$ 184.4 $1.67$ 29 $06/25/85 - 06/29/85$ 384.1 $0.84$ 30 $06/25/85 - 06/29/85$ 384.1 $0.80$ 31 $07/03/85 - 80$ 3.7 $0.25$ 32 $07/12/85 - 07/14/85 - 95$ 3.7 $0.40$ 33 $07/15/85 - 07/27/85 - 12$ 4.62.5736 $07/21/85 - 07/27/85 - 12$ 4.62.5736 $07/31/85 - 08/01/85 - 69$ 3.82.3037 $08/25/85 - 09/05/85 - 70$ 3.9 $0.266$ 40 $09/06/85 - 09/05/85 - 70$ 3.9 $0.266$ 41 $09/09/85 - 09/05/85 - 70$ 3.9 $0.77$ 42 $09/24/85 - 85 - 4.99 - 0.77$ 4.4 $0.711$ 43 $09/27/85 - 85 - 4.99 - 0.77$ 4.4 $0.711$ 44 $10/03/85 - 10/04/85 - 355 - 4.2 - 0.31$ 45 $10/05/85 - 11/06/85 - 11 - 4.6 - 0.25$ 56 $4.0 - 0.61$ 47 $10/25/85 - 11/17/85 - 56 - 4.0 - 0.61$ 48 $10/25/85 - 11/17/85 - 56 - 4.0 - 0.23$ 57 $11/26/85 - 11/17/85 - 11 - 4.6 - 0.35$ 55 $11/26/85 - 11/29/85 - 47 - 4.0 - 0.55$ 57 $12/31/85 - 10/26/85 - 19 - 4.3 - 0.27$ 56 $10/271/85 - 11/$   | 21                     | 05/18/85 - 05/19/85  | 17                             | 4.6        | 0.11                       |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 22                     | 05/27/85 - 05/28/85  | 26                             | 4.3        | 1.95                       |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 23                     | 06/01/85             | 23                             | 4.4        | 0.51                       |
| 25 $06/08/85$ 73 $3.8$ $0.29$ 26 $06/12/85$ $60$ $3.9$ $0.27$ 27 $06/16/85 - 06/17/85$ $18$ $4.4$ $1.67$ 28 $06/18/85$ $48$ $4.0$ $0.84$ 29 $06/24/85$ $86$ $3.8$ $0.24$ 30 $06/25/85 - 06/29/85$ $38$ $4.1$ $0.80$ $31$ $07/03/85$ $80$ $3.7$ $0.25$ $32$ $07/12/85 - 07/14/85$ $95$ $3.7$ $0.40$ $33$ $07/15/85$ $103$ $3.7$ $0.94$ $35$ $07/26/85 - 07/27/85$ $12$ $4.6$ $2.57$ $36$ $07/31/85 - 08/01/85$ $69$ $3.8$ $2.30$ $37$ $08/25/85 - 08/26/85$ $16$ $4.4$ $3.20$ $38$ $08/30/85 - 08/31/85$ $46$ $4.0$ $1.00$ $39$ $09/04/85 - 09/05/85$ $70$ $3.9$ $0.26$ $40$ $09/06/85 - 09/08/85$ $22$ $4.3$ $1.34$ $41$ $09/09/85 - 09/10/85$ $95$ $3.7$ $0.17$ $42$ $09/24/85$ $85$ $4.9$ $0.77$ $44$ $10/03/85 - 10/15/85$ $56$ $4.0$ $0.61$ $47$ $10/9/85 - 911/85$ $56$ $4.0$ $0.23$ $49$ $11/05/85 - 11/06/85$ $11$ $4.6$ $0.23$ $52$ $11/14/85$ $56$ $4.9$ $1.60$ $53$ $11/22/85 - 11/29/85$ $47$ $4.0$ $0.55$ $55$ $11/28/85 - 11/29/85$ $43$ $0.27$ <td>24</td> <td>06/05/85</td> <td>31</td> <td>4.2</td> <td>0.85</td>  | 24                     | 06/05/85             | 31                             | 4.2        | 0.85                       |
| $26$ $06/12/85$ $60$ $3.9$ $0.27$ $27$ $06/16/85 \cdot 06/17/85$ $18$ $4.4$ $1.67$ $28$ $06/24/85 \cdot 06/29/85$ $86$ $3.8$ $0.24$ $30$ $06/25/85 \cdot 06/29/85$ $38$ $4.1$ $0.80$ $31$ $07/03/85 \cdot 07/14/85$ $95$ $3.7$ $0.40$ $33$ $07/15/85 \cdot 07/14/85$ $95$ $3.7$ $0.40$ $33$ $07/15/85 \cdot 07/14/85$ $103$ $3.7$ $0.94$ $35$ $07/26/85 \cdot 07/27/85 \cdot 12$ $4.6$ $2.57$ $36$ $07/31/85 \cdot 08/26/85 \cdot 16$ $4.4$ $3.20$ $37$ $08/25/85 \cdot 08/26/85 \cdot 16$ $4.4$ $3.20$ $38$ $08/30/85 \cdot 08/31/85 \cdot 466$ $4.0$ $1.00$ $39$ $09/04/85 \cdot 09/05/85 \cdot 70$ $3.9$ $0.26$ $40$ $09/06/85 \cdot 09/08/85 \cdot 95$ $3.7$ $0.17$ $42$ $09/24/85 \cdot 85 \cdot 4.9$ $0.77$ $44$ $10/03/85 \cdot 10/04/85 \cdot 355 \cdot 4.2$ $0.31$ $45$ $10/05/85 \cdot 11/06/85 \cdot 19 \cdot 4.4$ $0.661$ $47$ $10/985 \cdot 91 \cdot 3.7$ $0.14$ $48$ $10/25/85 \cdot 11/06/85 \cdot 10 \cdot 4.7$ $1.79$ $50$ $11/11/85 \cdot 11/12/85 \cdot 40 \cdot 4.0$ $0.23$ $52$ $11/12/85 \cdot 11/28/5 \cdot 47 \cdot 4.0$ $0.23$ $52$ $11/12/85 \cdot 11/28/85 \cdot 11 \cdot 4.6$ $0.35$ $54$ $11/26/85 \cdot 11/29/85 \cdot 47 \cdot 4.0$ $0.55$ $55$ $11/28/85 \cdot 11/29/85 \cdot 47 \cdot 4.0$ $0.55$ $55$ $11/28/85 \cdot 11/29/85 \cdot 47 \cdot 4.0$ $0.56$ $57$ $12/13/85 \cdot 10/2$ | 25                     | 06/08/85             | 73                             | 3.8        | 0.29                       |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 20                     | 06/12/85             | 60                             | 3.9        | 0.27                       |
| 28 $06/18/85$ $48$ $4.0$ $0.84$ $29$ $06/24/85$ $86$ $3.8$ $0.24$ $30$ $06/25/85 - 06/29/85$ $38$ $4.1$ $0.80$ $31$ $07/03/85$ $80$ $3.7$ $0.25$ $32$ $07/12/85 - 07/14/85$ $95$ $3.7$ $0.40$ $33$ $07/15/85$ $51$ $4.0$ $0.19$ $34$ $07/21/85$ $103$ $3.7$ $0.94$ $35$ $07/26/85 - 07/27/85$ $12$ $4.6$ $2.57$ $36$ $07/31/85 - 08/01/85$ $69$ $3.8$ $2.30$ $37$ $08/25/85 - 08/26/85$ $16$ $4.4$ $3.20$ $38$ $08/30/85 - 08/31/85$ $46$ $4.0$ $1.00$ $39$ $09/04/85 - 09/05/85$ $70$ $3.9$ $0.26$ $40$ $09/06/85 - 09/08/85$ $22$ $4.3$ $1.34$ $41$ $09/09/85 - 09/10/85$ $95$ $3.7$ $0.17$ $42$ $09/24/85$ $85$ $4.9$ $0.77$ $44$ $10/03/85 - 10/04/85$ $35$ $4.2$ $0.31$ $45$ $10/05/85$ $19$ $4.4$ $0.71$ $46$ $10/13/85 - 10/15/85$ $56$ $4.0$ $0.61$ $47$ $10/08/85 - 11/12/85$ $10$ $4.7$ $1.79$ $50$ $11/11/85 - 11/12/85$ $56$ $4.9$ $1.60$ $53$ $11/28/85 - 11/29/85$ $47$ $4.0$ $0.55$ $54$ $11/28/85 - 11/29/85$ $47$ $4.0$ $0.55$ $56$ $1.9$ $0.56$ <td>2/</td> <td>06/16/85 - 06/17/85</td> <td>18</td> <td>4.4</td> <td>1.67</td>  | 2/                     | 06/16/85 - 06/17/85  | 18                             | 4.4        | 1.67                       |
| 29 $06/24/85$ $86$ $3.8$ $0.24$ 30 $06/25/85 \cdot 06/29/85$ $38$ $4.1$ $0.80$ $31$ $07/03/85$ $80$ $3.7$ $0.25$ $32$ $07/12/85 \cdot 07/14/85$ $95$ $3.7$ $0.40$ $33$ $07/15/85$ $51$ $4.0$ $0.19$ $34$ $07/21/85 \cdot 07/27/85$ $12$ $4.6$ $2.57$ $36$ $07/21/85 \cdot 08/01/85$ $69$ $3.8$ $2.30$ $37$ $08/25/85 \cdot 08/26/85$ $16$ $4.4$ $3.20$ $38$ $08/30/85 \cdot 08/31/85$ $46$ $4.0$ $1.00$ $39$ $09/04/85 \cdot 09/05/85$ $70$ $3.9$ $0.26$ $40$ $09/06/85 \cdot 09/08/85$ $22$ $4.3$ $1.34$ $41$ $09/09/85 \cdot 09/10/85$ $95$ $3.7$ $0.17$ $42$ $09/24/85$ $85$ $4.9$ $0.77$ $44$ $10/03/85 \cdot 10/04/85$ $35$ $4.2$ $0.31$ $45$ $10/05/85$ $19$ $4.4$ $0.71$ $46$ $10/13/85 \cdot 10/15/85$ $56$ $4.0$ $0.61$ $47$ $10/9/85 \cdot 11/06/85$ $11$ $4.6$ $0.29$ $49$ $11/05/85 \cdot 11/08/5$ $10$ $4.7$ $1.79$ $50$ $11/14/85$ $56$ $4.0$ $0.23$ $52$ $11/16/85 \cdot 11/12/85$ $47$ $4.0$ $0.55$ $55$ $11/28/85 \cdot 11/20/85$ $19$ $4.4$ $1.06$ $56$ $12/11/85$ $56$ $3.9$ $0.56$ $57$ $12/21/85$ $19$ <td< td=""><td>20</td><td>06/24/95</td><td>48</td><td>4.0</td><td>0.84</td></td<>  | 20                     | 06/24/95             | 48                             | 4.0        | 0.84                       |
| 30 $00/23/85 - 00/29/85$ $38$ $4.1$ $0.80$ $31$ $07/03/85$ $80$ $3.7$ $0.25$ $32$ $07/12/85 - 07/14/85$ $95$ $3.7$ $0.40$ $33$ $07/15/85$ $51$ $4.0$ $0.19$ $34$ $07/21/85$ $103$ $3.7$ $0.94$ $35$ $07/26/85 - 07/27/85$ $12$ $4.6$ $2.57$ $36$ $07/31/85 - 08/01/85$ $69$ $3.8$ $2.30$ $37$ $08/25/85 - 08/26/85$ $16$ $4.4$ $3.20$ $38$ $08/30/85 - 08/31/85$ $46$ $4.0$ $1.00$ $39$ $09/04/85 - 09/05/85$ $70$ $3.9$ $0.26$ $40$ $09/06/85 - 09/08/85$ $22$ $4.3$ $1.34$ $41$ $09/09/85 - 09/10/85$ $95$ $3.7$ $0.17$ $42$ $09/24/85$ $85$ $4.9$ $0.77$ $44$ $10/03/85 - 10/18/5$ $35$ $4.2$ $0.31$ $45$ $10/05/85$ $19$ $4.4$ $0.71$ $46$ $10/13/85 - 10/15/85$ $56$ $4.0$ $0.61$ $47$ $10/19/85$ $91$ $3.7$ $0.14$ $48$ $10/25/85$ $11$ $4.6$ $0.23$ $52$ $11/16/85 - 11/17/85$ $6$ $4.9$ $1.60$ $53$ $11/22/85 - 11/29/85$ $47$ $4.0$ $0.55$ $54$ $11/26/85 - 11/29/85$ $47$ $4.0$ $0.55$ $54$ $11/28/85 - 11/29/85$ $47$ $4.0$ $0.55$ $57$ $12/13/85$ $10$ <td>29</td> <td></td> <td>86</td> <td>3.8</td> <td>0.24</td>  | 29                     |                      | 86                             | 3.8        | 0.24                       |
| 31 $07/03/65$ $80$ $3.7$ $0.25$ $32$ $07/12/85 - 07/14/85$ $95$ $3.7$ $0.40$ $33$ $07/15/85$ $51$ $4.0$ $0.19$ $34$ $07/21/85$ $103$ $3.7$ $0.94$ $35$ $07/26/85 - 07/27/85$ $12$ $4.6$ $2.57$ $36$ $07/31/85 - 08/01/85$ $69$ $3.8$ $2.30$ $37$ $08/25/85 - 08/26/85$ $16$ $4.4$ $3.20$ $38$ $08/30/85 - 08/31/85$ $46$ $4.0$ $1.00$ $39$ $09/04/85 - 09/05/85$ $70$ $3.9$ $0.26$ $40$ $09/06/85 - 09/08/85$ $22$ $4.3$ $1.34$ $41$ $09/09/85 - 09/10/85$ $95$ $3.7$ $0.17$ $42$ $09/24/85$ $85$ $4.9$ $0.77$ $44$ $10/03/85 - 10/04/85$ $35$ $4.2$ $0.31$ $45$ $10/05/85$ $91$ $3.7$ $0.14$ $48$ $10/25/85$ $91$ $3.7$ $0.14$ $48$ $10/25/85$ $11$ $4.6$ $0.29$ $49$ $11/05/85 - 11/12/85$ $40$ $4.0$ $1.09$ $51$ $11/14/85$ $56$ $4.0$ $0.23$ $52$ $11/26/85 - 11/29/85$ $47$ $4.0$ $0.55$ $55$ $11/28/5 - 11/28/5$ $19$ $4.4$ $1.06$ $56$ $12/11/85$ $56$ $3.9$ $0.56$ $57$ $12/13/85$ $12/20/95$ $4.3$ $0.27$   | 30                     | 00/23/03 - 00/29/03  | 38                             | 4.1        | 0.80                       |
| 32 $07/12/85 + 07/14/85$ $95$ $3.7$ $0.40$ $33$ $07/15/85$ $51$ $4.0$ $0.19$ $34$ $07/21/85$ $103$ $3.7$ $0.94$ $35$ $07/26/85 + 07/27/85$ $12$ $4.6$ $2.57$ $36$ $07/31/85 + 08/01/85$ $69$ $3.8$ $2.30$ $37$ $08/25/85 + 08/26/85$ $16$ $4.4$ $3.20$ $38$ $08/30/85 + 08/26/85$ $16$ $4.4$ $3.20$ $38$ $08/30/85 + 09/05/85$ $70$ $3.9$ $0.26$ $40$ $09/06/85 + 09/05/85$ $70$ $3.9$ $0.26$ $40$ $09/06/85 + 09/08/85$ $22$ $4.3$ $1.34$ $41$ $09/09/85 + 09/08/85$ $92$ $3.7$ $0.17$ $42$ $09/24/85$ $8$ $5.1$ $0.54$ $43$ $09/27/85$ $85$ $4.9$ $0.77$ $44$ $10/03/85 + 10/04/85$ $35$ $4.2$ $0.31$ $45$ $10/05/85$ $91$ $3.7$ $0.14$ $48$ $10/25/85$ $11$ $4.6$ $0.29$ $49$ $11/05/85 + 11/16/85$ $10$ $4.7$ $1.79$ $50$ $11/11/85 + 11/12/85$ $40$ $4.0$ $1.09$ $51$ $11/12/85 + 11/2/85$ $11$ $4.6$ $0.35$ $54$ $11/26/85 + 11/29/85$ $47$ $4.0$ $0.55$ $55$ $11/28/85 - 11/30/85$ $19$ $4.4$ $1.06$ $56$ $12/11/85$ $56$ $3.9$ $0.56$ $57$ $12/13/85 + 10/20/95$   | 30                     | 07/13/05 07/14/05    | 80                             | 3./        | 0.25                       |
| 33 $07/21/85$ $51$ $4.0$ $0.19$ 34 $07/21/85$ $103$ $3.7$ $0.94$ 35 $07/26/85 - 07/27/85$ $12$ $4.6$ $2.57$ 36 $07/31/85 - 08/01/85$ $69$ $3.8$ $2.30$ 37 $08/25/85 - 08/26/85$ $16$ $4.4$ $3.20$ 38 $08/30/85 - 08/31/85$ $46$ $4.0$ $1.00$ 39 $09/04/85 - 09/05/85$ $70$ $3.9$ $0.26$ 40 $09/06/85 - 09/08/85$ $22$ $4.3$ $1.34$ 41 $09/09/85 - 09/10/85$ $95$ $3.7$ $0.17$ 42 $09/24/85$ $8$ $5.1$ $0.54$ 43 $09/27/85$ $85$ $4.9$ $0.77$ 44 $10/03/85 - 10/04/85$ $35$ $4.2$ $0.31$ 45 $10/05/85$ $19$ $4.4$ $0.71$ 46 $10/13/85 - 10/15/85$ $56$ $4.0$ $0.61$ 47 $10/25/85$ $11$ $4.6$ $0.29$ 49 $11/05/85 - 11/12/85$ $40$ $4.0$ $1.09$ 51 $11/14/85 - 56$ $4.0$ $0.23$ 52 $11/16/85 - 11/17/85$ $6$ $4.9$ $1.60$ 53 $11/22/85 - 11/24/85 - 11$ $4.6$ $0.355$ 54 $11/26/85 - 11/29/85 - 47$ $4.0$ $0.55$ 55 $11/28/5 - 10/20/95 - 43$ $0.27$   | 32                     | 07/15/85             | 95<br>E1                       | 3./        | 0.40                       |
| 35 $07/26/85 - 07/27/85$ $103$ $3.7$ $0.94$ $36$ $07/31/85 - 08/01/85$ $69$ $3.8$ $2.57$ $36$ $07/31/85 - 08/26/85$ $16$ $4.4$ $3.20$ $37$ $08/25/85 - 08/26/85$ $16$ $4.4$ $3.20$ $38$ $08/30/85 - 08/31/85$ $46$ $4.0$ $1.00$ $39$ $09/04/85 - 09/05/85$ $70$ $3.9$ $0.26$ $40$ $09/06/85 - 09/08/85$ $22$ $4.3$ $1.34$ $41$ $09/09/85 - 09/10/85$ $95$ $3.7$ $0.17$ $42$ $09/24/85$ $8$ $5.1$ $0.54$ $43$ $09/27/85$ $85$ $4.9$ $0.77$ $44$ $10/03/85 - 10/04/85$ $35$ $4.2$ $0.31$ $45$ $10/05/85$ $19$ $4.4$ $0.71$ $46$ $10/13/85 - 10/15/85$ $56$ $4.0$ $0.61$ $47$ $10/19/85$ $91$ $3.7$ $0.14$ $48$ $10/25/85$ $11$ $4.6$ $0.29$ $49$ $11/05/85 - 11/106/85$ $10$ $4.7$ $1.09$ $51$ $11/14/85 - 11/17/85$ $6$ $4.9$ $1.60$ $53$ $11/22/85 - 11/28/5$ $11$ $4.6$ $0.35$ $54$ $11/26/85 - 11/29/85$ $47$ $4.0$ $0.55$ $55$ $11/28/85 - 11/30/85$ $19$ $4.4$ $1.06$ $56$ $12/11/85$ $56$ $3.9$ $0.56$ $57$ $12/13/85 - 10/29/85$ $16$ $4.3$ $0.27$   | 32                     | 07/21/85             | 5 I<br>102                     | 4.0        | 0.19                       |
| 36 $07/31/85 - 08/01/85$ $12$ $4.0$ $2.37$ $37$ $08/25/85 - 08/26/85$ $16$ $4.4$ $3.20$ $38$ $08/30/85 - 08/31/85$ $46$ $4.0$ $1.00$ $39$ $09/04/85 - 09/05/85$ $70$ $3.9$ $0.26$ $40$ $09/06/85 - 09/08/85$ $22$ $4.3$ $1.34$ $41$ $09/09/85 - 09/08/85$ $22$ $4.3$ $1.34$ $41$ $09/09/85 - 09/10/85$ $95$ $3.7$ $0.17$ $42$ $09/24/85$ $8$ $5.1$ $0.54$ $43$ $09/27/85$ $85$ $4.9$ $0.77$ $44$ $10/03/85 - 10/04/85$ $35$ $4.2$ $0.31$ $45$ $10/05/85$ $19$ $4.4$ $0.71$ $46$ $10/13/85 - 10/15/85$ $91$ $3.7$ $0.14$ $48$ $10/25/85$ $11$ $4.6$ $0.29$ $49$ $11/05/85 - 11/06/85$ $10$ $4.7$ $1.09$ $51$ $11/14/85 - 11/12/85$ $47$ $4.0$ $0.23$ $52$ $11/16/85 - 11/12/85$ $11$ $4.6$ $0.35$ $54$ $11/26/85 - 11/29/85$ $47$ $4.0$ $0.55$ $55$ $11/28/85 - 11/29/85$ $47$ $4.0$ $0.55$ $57$ $12/13/85$ $56$ $3.9$ $0.56$ $57$ $12/13/85$ $29$ $4.3$ $0.27$   | 35                     | 07/26/85 - 07/27/85  | 105                            | 5.7        | 0.94                       |
| 37 $08/25/85 - 08/26/85$ $16$ $4.4$ $3.20$ $38$ $08/30/85 - 08/31/85$ $46$ $4.0$ $1.00$ $39$ $09/04/85 - 09/05/85$ $70$ $3.9$ $0.26$ $40$ $09/06/85 - 09/08/85$ $22$ $4.3$ $1.34$ $41$ $09/09/85 - 09/10/85$ $95$ $3.7$ $0.17$ $42$ $09/24/85$ $8$ $5.1$ $0.54$ $43$ $09/27/85$ $85$ $4.9$ $0.77$ $44$ $10/03/85 - 10/04/85$ $35$ $4.2$ $0.31$ $45$ $10/05/85$ $19$ $4.4$ $0.71$ $46$ $10/13/85 - 10/15/85$ $56$ $4.0$ $0.61$ $47$ $10/19/85$ $91$ $3.7$ $0.14$ $48$ $10/25/85$ $11$ $4.6$ $0.29$ $49$ $11/05/85 - 11/06/85$ $10$ $4.7$ $1.79$ $50$ $11/11/85 - 11/12/85$ $6$ $4.0$ $1.09$ $51$ $11/26/85 - 11/28/5$ $11$ $4.6$ $0.23$ $52$ $11/28/5 - 11/28/5$ $11$ $4.6$ $0.35$ $54$ $11/26/85 - 11/28/85$ $11$ $4.6$ $0.35$ $54$ $11/26/85 - 11/29/85$ $47$ $4.0$ $0.55$ $55$ $11/28/85 - 11/30/85$ $19$ $4.4$ $1.06$ $56$ $12/11/85$ $56$ $3.9$ $0.56$ $57$ $12/13/85$ $29$ $4.3$ $0.27$   | 36                     | 07/31/85 - 08/01/85  | 69                             | 4.0<br>2 Q | 2.37                       |
| 38 $08/30/85 - 08/31/85$ 464.01.0039 $09/04/85 - 09/05/85$ 70 $3.9$ $0.26$ 40 $09/06/85 - 09/08/85$ 22 $4.3$ $1.34$ 41 $09/09/85 - 09/10/85$ 95 $3.7$ $0.17$ 42 $09/24/85$ 8 $5.1$ $0.54$ 43 $09/27/85$ 85 $4.9$ $0.77$ 44 $10/03/85 - 10/04/85$ 35 $4.2$ $0.31$ 45 $10/05/85$ 19 $4.4$ $0.71$ 46 $10/13/85 - 10/15/85$ 56 $4.0$ $0.61$ 47 $10/19/85$ 91 $3.7$ $0.14$ 48 $10/25/85$ 11 $4.6$ $0.29$ 49 $11/05/85 - 11/06/85$ 10 $4.7$ $1.79$ 50 $11/11/85 - 11/12/85$ 40 $4.0$ $1.09$ 51 $11/12/85 - 11/12/85$ 11 $4.6$ $0.35$ 52 $11/26/85 - 11/12/85$ 11 $4.6$ $0.35$ 54 $11/26/85 - 11/12/85$ 47 $4.0$ $0.55$ 55 $11/28/85 - 11/30/85$ 19 $4.4$ $1.06$ 56 $12/11/85$ 56 $3.9$ $0.56$ 57 $12/13/85$ 29 $4.3$ $0.27$  | 37                     | 08/25/85 - 08/26/85  | 16                             | Δ.Δ        | 2.30                       |
| 39 $09/04/85 - 09/05/85$ 703.9 $0.26$ 40 $09/06/85 - 09/08/85$ 224.31.3441 $09/09/85 - 09/10/85$ 953.70.1742 $09/24/85$ 85.10.5443 $09/27/85$ 854.90.7744 $10/03/85 - 10/04/85$ 354.20.3145 $10/05/85$ 194.40.7146 $10/13/85 - 10/15/85$ 564.00.6147 $10/05/85$ 114.60.2949 $11/05/85 - 11/06/85$ 104.71.7950 $11/11/85 - 11/12/85$ 404.01.0951 $11/12/85 - 11/12/85$ 404.00.2352 $11/16/85 - 11/12/85$ 114.60.3554 $11/26/85 - 11/29/85$ 474.00.5555 $11/28/85 - 11/30/85$ 194.41.0656 $12/11/85$ 563.90.5657 $12/13/85$ 294.30.27  | 38                     | 08/30/85 - 08/31/85  | 46                             | 4.0        | 1.00                       |
| 40 $09/06/85 - 09/08/85$ 224.31.3441 $09/09/85 - 09/10/85$ 953.70.1742 $09/24/85$ 85.10.5443 $09/27/85$ 854.90.7744 $10/03/85 - 10/04/85$ 354.20.3145 $10/05/85$ 194.40.7146 $10/13/85 - 10/15/85$ 564.00.6147 $10/19/85$ 913.70.1448 $10/25/85$ 114.60.2949 $11/05/85 - 11/06/85$ 104.71.7950 $11/11/85 - 11/12/85$ 404.01.0951 $11/14/85$ 564.00.2352 $11/16/85 - 11/17/85$ 64.91.6053 $11/22/85 - 11/24/85$ 114.60.3554 $11/26/85 - 11/29/85$ 474.00.5555 $11/28/85 - 11/30/85$ 194.41.0656 $12/11/85$ 563.90.5657 $12/13/85$ 294.30.27   | 3 <del>9</del>         | 09/04/85 - 09/05/85  | 70                             | 39         | 0.26                       |
| 41 $09/09/85 - 09/10/85$ $95$ $3.7$ $0.17$ 42 $09/24/85$ 8 $5.1$ $0.54$ 43 $09/27/85$ $85$ $4.9$ $0.77$ 44 $10/03/85 - 10/04/85$ $35$ $4.2$ $0.31$ 45 $10/05/85$ $19$ $4.4$ $0.71$ 46 $10/13/85 - 10/15/85$ $56$ $4.0$ $0.61$ 47 $10/19/85$ $91$ $3.7$ $0.14$ 48 $10/25/85$ $11$ $4.6$ $0.29$ 49 $11/05/85 - 11/06/85$ $10$ $4.7$ $1.79$ 50 $11/11/85 - 11/12/85$ $40$ $4.0$ $1.09$ 51 $11/14/85$ $56$ $4.0$ $0.23$ 52 $11/16/85 - 11/12/85$ $11$ $4.6$ $0.35$ 54 $11/26/85 - 11/29/85$ $47$ $4.0$ $0.55$ 55 $11/28/85 - 11/30/85$ $19$ $4.4$ $1.06$ 56 $12/11/85$ $56$ $3.9$ $0.56$ 57 $12/13/85$ $29$ $4.3$ $0.27$   | 40                     | 09/06/85 - 09/08/85  | 22                             | 4.3        | 1 34                       |
| 42 $09/24/85$ $8$ $5.1$ $0.54$ $43$ $09/27/85$ $85$ $4.9$ $0.77$ $44$ $10/03/85 - 10/04/85$ $35$ $4.2$ $0.31$ $45$ $10/05/85$ $19$ $4.4$ $0.71$ $46$ $10/13/85 - 10/15/85$ $56$ $4.0$ $0.61$ $47$ $10/19/85$ $91$ $3.7$ $0.14$ $48$ $10/25/85$ $11$ $4.6$ $0.29$ $49$ $11/05/85 - 11/06/85$ $10$ $4.7$ $1.79$ $50$ $11/11/85 - 11/12/85$ $40$ $4.0$ $1.09$ $51$ $11/16/85 - 11/12/85$ $6$ $4.9$ $1.60$ $53$ $11/22/85 - 11/24/85$ $11$ $4.6$ $0.35$ $54$ $11/26/85 - 11/29/85$ $47$ $4.0$ $0.55$ $55$ $11/28/85 - 11/30/85$ $19$ $4.4$ $1.06$ $56$ $12/11/85$ $56$ $3.9$ $0.56$ $57$ $12/213/85$ $10/20/65$ $10/20/65$ $10/20/65$  | 41                     | 09/09/85 - 09/10/85  | 95                             | 3.7        | 0.17                       |
| 43 $09/27/85$ 85 $4.9$ $0.77$ 44 $10/03/85 - 10/04/85$ $35$ $4.2$ $0.31$ 45 $10/05/85$ $19$ $4.4$ $0.71$ 46 $10/13/85 - 10/15/85$ $56$ $4.0$ $0.61$ 47 $10/19/85$ $91$ $3.7$ $0.14$ 48 $10/25/85$ $11$ $4.6$ $0.29$ 49 $11/05/85 - 11/06/85$ $10$ $4.7$ $1.79$ 50 $11/11/85 - 11/12/85$ $40$ $4.0$ $1.09$ 51 $11/14/85$ $56$ $4.0$ $0.23$ 52 $11/16/85 - 11/17/85$ $6$ $4.9$ $1.60$ 53 $11/22/85 - 11/24/85$ $11$ $4.6$ $0.35$ 54 $11/26/85 - 11/29/85$ $47$ $4.0$ $0.55$ 55 $11/28/85 - 11/30/85$ $19$ $4.4$ $1.06$ 56 $12/11/85$ $56$ $3.9$ $0.56$ 57 $12/13/85$ $29$ $4.3$ $0.27$   | 42                     | 09/24/85             | 8                              | 5.1        | 0.54                       |
| 44 $10/03/85 - 10/04/85$ 35 $4.2$ $0.31$ 45 $10/05/85$ 19 $4.4$ $0.71$ 46 $10/13/85 - 10/15/85$ 56 $4.0$ $0.61$ 47 $10/19/85$ 91 $3.7$ $0.14$ 48 $10/25/85$ 11 $4.6$ $0.29$ 49 $11/05/85 - 11/06/85$ 10 $4.7$ $1.79$ 50 $11/11/85 - 11/12/85$ 40 $4.0$ $1.09$ 51 $11/14/85$ 56 $4.0$ $0.23$ 52 $11/16/85 - 11/17/85$ 6 $4.9$ $1.60$ 53 $11/22/85 - 11/24/85$ 11 $4.6$ $0.35$ 54 $11/26/85 - 11/29/85$ 47 $4.0$ $0.55$ 55 $11/28/85 - 11/30/85$ 19 $4.4$ $1.06$ 56 $12/11/85$ 56 $3.9$ $0.56$ 57 $12/13/85$ $29$ $4.3$ $0.27$   | 43                     | 09/27/85             | 85                             | 4.9        | 0.77                       |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 44                     | 10/03/85 - 10/04/85  | 35                             | 4.2        | 0.31                       |
| 46 $10/13/85 - 10/15/85$ $56$ $4.0$ $0.61$ $47$ $10/19/85$ $91$ $3.7$ $0.14$ $48$ $10/25/85$ $11$ $4.6$ $0.29$ $49$ $11/05/85 - 11/06/85$ $10$ $4.7$ $1.79$ $50$ $11/11/85 - 11/12/85$ $40$ $4.0$ $1.09$ $51$ $11/14/85$ $56$ $4.0$ $0.23$ $52$ $11/16/85 - 11/17/85$ $6$ $4.9$ $1.60$ $53$ $11/22/85 - 11/24/85$ $11$ $4.6$ $0.35$ $54$ $11/26/85 - 11/29/85$ $47$ $4.0$ $0.55$ $55$ $11/28/85 - 11/30/85$ $19$ $4.4$ $1.06$ $56$ $12/11/85$ $56$ $3.9$ $0.56$ $57$ $12/13/85$ $29$ $4.3$ $0.27$  | 45                     | 10/05/85             | 19                             | 4.4        | 0.71                       |
| 47 $10/19/85$ $91$ $3.7$ $0.14$ $48$ $10/25/85$ $11$ $4.6$ $0.29$ $49$ $11/05/85 - 11/06/85$ $10$ $4.7$ $1.79$ $50$ $11/11/85 - 11/12/85$ $40$ $4.0$ $1.09$ $51$ $11/14/85$ $56$ $4.0$ $0.23$ $52$ $11/16/85 - 11/12/85$ $6$ $4.9$ $1.60$ $53$ $11/22/85 - 11/24/85$ $11$ $4.6$ $0.35$ $54$ $11/26/85 - 11/29/85$ $47$ $4.0$ $0.55$ $55$ $11/28/85 - 11/30/85$ $19$ $4.4$ $1.06$ $56$ $12/11/85$ $56$ $3.9$ $0.56$ $57$ $12/13/85$ $29$ $4.3$ $0.27$   | 46                     | 10/13/85 - 10/15/85  | 56                             | 4.0        | 0.61                       |
| 48 $10/25/85$ $11$ $4.6$ $0.29$ $49$ $11/05/85 - 11/06/85$ $10$ $4.7$ $1.79$ $50$ $11/11/85 - 11/12/85$ $40$ $4.0$ $1.09$ $51$ $11/14/85$ $56$ $4.0$ $0.23$ $52$ $11/16/85 - 11/17/85$ $6$ $4.9$ $1.60$ $53$ $11/22/85 - 11/24/85$ $11$ $4.6$ $0.35$ $54$ $11/26/85 - 11/29/85$ $47$ $4.0$ $0.55$ $55$ $11/28/85 - 11/30/85$ $19$ $4.4$ $1.06$ $56$ $12/11/85$ $56$ $3.9$ $0.56$ $57$ $12/13/85$ $29$ $4.3$ $0.27$   | 4/                     | 10/19/85             | 91                             | 3.7        | 0.14                       |
| 49 $11/05/85 - 11/06/85$ 10 $4.7$ $1.79$ 50 $11/11/85 - 11/12/85$ 40 $4.0$ $1.09$ 51 $11/14/85$ 56 $4.0$ $0.23$ 52 $11/16/85 - 11/17/85$ 6 $4.9$ $1.60$ 53 $11/22/85 - 11/24/85$ 11 $4.6$ $0.35$ 54 $11/26/85 - 11/29/85$ 47 $4.0$ $0.55$ 55 $11/28/85 - 11/30/85$ 19 $4.4$ $1.06$ 56 $12/11/85$ 56 $3.9$ $0.56$ 57 $12/13/85$ 29 $4.3$ $0.27$   | 48                     | 10/25/85             | 11                             | 4.6        | 0.29                       |
| 50       11/11/85 - 11/12/85       40       4.0       1.09         51       11/14/85       56       4.0       0.23         52       11/16/85 - 11/17/85       6       4.9       1.60         53       11/22/85 - 11/24/85       11       4.6       0.35         54       11/26/85 - 11/29/85       47       4.0       0.55         55       11/28/85 - 11/30/85       19       4.4       1.06         56       12/11/85       56       3.9       0.56         57       12/13/85       29       4.3       0.27  | 49                     | 11/05/85 - 11/06/85  | 10                             | 4.7        | 1.79                       |
| 51       11/14/85       56       4.0       0.23         52       11/16/85 - 11/17/85       6       4.9       1.60         53       11/22/85 - 11/24/85       11       4.6       0.35         54       11/26/85 - 11/29/85       47       4.0       0.55         55       11/28/85 - 11/30/85       19       4.4       1.06         56       12/11/85       56       3.9       0.56         57       12/13/85       29       4.3       0.27   | 50                     | 11/11/85 - 11/12/85  | 40                             | 4.0        | 1.09                       |
| 52       11/16/85 - 11/1/85       6       4.9       1.60         53       11/22/85 - 11/24/85       11       4.6       0.35         54       11/26/85 - 11/29/85       47       4.0       0.55         55       11/28/85 - 11/30/85       19       4.4       1.06         56       12/11/85       56       3.9       0.56         57       12/13/85       29       4.3       0.27  | 51                     |                      | 56                             | 4.0        | 0.23                       |
| 53       11/22/85 - 11/24/85       11       4.6       0.35         54       11/26/85 - 11/29/85       47       4.0       0.55         55       11/28/85 - 11/30/85       19       4.4       1.06         56       12/11/85       56       3.9       0.56         57       12/13/85       29       4.3       0.27   | 52                     |                      | 6                              | 4.9        | 1.60                       |
| 54       11/20/85 - 11/29/85       47       4.0       0.55         55       11/28/85 - 11/30/85       19       4.4       1.06         56       12/11/85       56       3.9       0.56         57       12/13/85       29       4.3       0.27  | 55                     | 11/22/03 - 11/24/03  | <br>A7                         | 4.6        | 0.35                       |
| 55       11/28/85 - 11/30/85       19       4.4       1.06         56       12/11/85       56       3.9       0.56         57       12/13/85       29       4.3       0.27   | 55                     |                      | 4/                             | 4.0        | 0.55                       |
| 57     12/13/85     29     4.3     0.27  | 56                     | 12/11/85             | 19                             | 4.4        | 1.06                       |
|  | 57                     | 12/13/85             | 20                             | 3.9<br>∕\> | 0.50<br>7 C D              |
| סס 12/20/85 - 12/23/85 46 4.0 0 13*  | 58                     | 12/20/85 - 12/23/85  | 46                             | 4.0        | 0.27                       |



## **INCHES OF PRECIPITATION**

PLAINFIELD SITE, 1985





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# SPECIFIC CONDUCTANCE OF PRECIPITATION

PLAINFIELD SITE, 1985

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## **INCHES OF PRECIPITATION**

**MORRIS DAM SITE, 1985** 

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## ACIDITY OF PRECIPITATION

**MORRIS DAM SITE, 1985** 

ACIDITY = 7 - pH



# SPECIFIC CONDUCTANCE OF PRECIPITATION

**MORRIS DAM SITE, 1985** 





## **INCHES OF PRECIPITATION**

**MARLBOROUGH SITE, 1985** 

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**MARLBOROUGH SITE, 1985** 



ACIDITY = 7 - pH



# SPECIFIC CONDUCTANCE OF PRECIPITATION

**MARLBOROUGH SITE, 1985** 

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### IX. CLIMATOLOGICAL DATA

Weather is often the most significant factor influencing short-term changes in air quality. It also has an affect on long-term trends. Climatological information from the National Weather Service station at Bradley International Airport in Windsor Locks is shown in Table 31 for the years 1984 and 1985. Table 32 contains information from the National Weather Service station located at Sikorsky Memorial Airport near Bridgeport. All data are compared to "mean" or "normal" values. Wind speeds" and temperatures are shown as monthly and yearly averages. Precipitation data includes both the number of days with more than 0.01 inches of precipitation and the total water equivalent. Also shown are degree days<sup>\*\*</sup> (heating requirement) and the number of days with temperatures exceeding 90°F.

Wind roses for Bradley Airport and Newark Airport have been developed from 1985 National Weather Service surface observations and are shown in Figures 28 and 30, respectively. Wind roses from these stations for 1984 are shown in Figures 27 and 29, respectively.

\* The mean wind speed for a month or year is calculated for all the hourly wind speeds, regardless of the wind directions.

\*\* The degree day value for each day is arrived at by subtracting the average temperature of the day from 65°F. This number (65) is used as a base value because it is assumed that there is no heating requirement when the outside temperature is 65°F.

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### 1984 AND 1985 CLIMATOLOGICAL DATA

**BRADLEY INTERNATIONAL AIRPORT, WINDSOR LOCKS** 

|              | DNIN    | (H)            | Mean <sup>d</sup> | 9.0  | 9.4  | 10.0 | 10.1 | 8.9   | 8.1  | 7.5  | 7.1  | 7.2  | 7.7  | 8.4  | 8.6  | 8.5   |  |
|--------------|---------|----------------|-------------------|------|------|------|------|-------|------|------|------|------|------|------|------|-------|--|
|              | ERAGE V | EED (MI        | 1985              | 7.5  | 8.4  | 9.3  | 7.7  | 7.9   | 6.7  | 6.2  | 5.2  | 5.5  | 6.0  | 7.4  | 7.7  | ۲.1   |  |
|              | AVE     | ß              | 1984              | 6.0  | 7.5  | 9.2  | 7.9  | 7.8   | 7.2  | 6.7  | 5.5  | 6.0  | 6.2  | 7.3  | 6.7  | 7.0   |  |
| r'S<br>H A N | OF      | N              | Mean <sup>d</sup> | 11   | 10   | 12   | 11   | 12    | 11   | 10   | 10   | 6    | 8    | 11   | 12   | 127   |  |
| OF DA        | INCHES  | <b>IPITATI</b> | 1985              | 11   | 6    | 6    | 6    | 6     | 13   | 11   | 6    | 10   | 6    | 14   | 10   | 123   |  |
| NO.<br>HTIW  | 0.01    | PREC           | 1984              | 13   | 14   | 14   | 12   | 15    | 10   | 10   | ٢    | 7    | 7    | 7    | 14   | 130   |  |
| NO           | ENT     | ATER           | Mean <sup>a</sup> | 3.51 | 3.24 | 3.74 | 3.78 | 3.62  | 3.54 | 3.52 | 3.81 | 3.61 | 3.16 | 3.77 | 3.74 | 43.05 |  |
| CIPITATI     | QUIVAL  | S OF W         | 1985              | 0.73 | 1.72 | 2.16 | 1.54 | 2.77  | 3.55 | 4.55 | 6.44 | 3.83 | 2.27 | 6.04 | 1.28 | 36.88 |  |
| PRE          | Ξ.      | INCHE          | 1984              | 1.80 | 4.72 | 3.93 | 4.24 | 11.55 | 2.16 | 4.22 | 1.32 | 1.20 | 2.76 | 2.45 | 2.46 | 42.85 |  |
|              |         | AYS            | Normal            | 1234 | 1047 | 874  | 486  | 197   | 20   | 0    | 8    | 102  | 391  | 702  | 1113 | 6174  |  |
|              |         | GREE D         | 1985              | 1341 | 975  | 776  | 428  | 167   | 76   | 0    | 14   | 119  | 401  | 648  | 1157 | 6102  |  |
|              |         | B              | 1984              | 1332 | 884  | 1035 | 503  | 286   | 32   | m    | m    | 186  | 298  | 698  | 896  | 6156  |  |
| AYS          | TEMP.   | <u>30 f</u>    | Mean <sup>b</sup> | 0    | 0    | 0    | *    | -     | 4    | 80   | 2    | 2    | *    | 0    | 0    | 19    |  |
| 0. OF DA     | I MAX.  | EEDED          | 1985              | 0    | 0    | 0    | 0    |       | 0    | -    | 2    | -    | 0    | 0    | 0    | ŝ     |  |
| Ň            | WHEN    | EXC            | 1984              | 0    | 0    | 0    | 0    | 0     | 9    | 2    | 4    | 0    | 0    | •    | 0    | 12    |  |
|              | щ       | 바<br>바         | Mean <sup>a</sup> | 26.5 | 27.8 | 37.0 | 48.1 | 59.1  | 67.9 | 73.2 | 71.0 | 63.5 | 53.0 | 42.0 | 30.4 | 50.0  |  |
|              | AVERAG  | PERATU         | 1985              | 21.5 | 29.9 | 39.7 | 50.7 | 60.6  | 63.7 | 72.4 | 70.2 | 63.4 | 51.9 | 43.2 | 27.5 | 49.6  |  |
|              | `       | TEM            | 1984              | 21.8 | 34.3 | 31.4 | 48.0 | 56.0  | 69.8 | 71.8 | 73.2 | 59.8 | 55.2 | 41.5 | 35.7 | 49.9  |  |
|              |         |                |                   | Jan  | Feb  | Mar  | Apr  | May   | Jun  | InL  | Aug  | Sep  | Oct  | Nov  | Dec  | YEAR  |  |

National Oceanic and Atmospheric Administration Environmental Data Service

Extracted From: Local Climatological Data Charts

U.S. Department of Commerce

\* Less than 0.5 a 1905-1985 b 1960-1985 c 1951-1980 d 1955-1985

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### 1984 AND 1985 CLIMATOLOGICAL DATA

## SIKORSKY INTERNATIONAL AIRPORT, STRATFORD

| QNI                | Ĥ        | Mean <sup>f</sup> | 13.2 | 13.6 | 13.5 | 13.0 | 11.6 | 10.5 | 10.0 | 10.1 | 11.2 | 11.9 | 12.7 | 13.0 | 12.0  |  |
|--------------------|----------|-------------------|------|------|------|------|------|------|------|------|------|------|------|------|-------|--|
| RAGE W             | EED (MP  | 1985              | I    | l    | ł    | ł    | ł    | l    | ł    | ł    | l    | 1    | I    | ł    | 1     |  |
| AVE                | SP       | 1984              | ł    | ł    | ***  | ł    | I    |      |      | ł    | ł    | ţ    | ł    | 1    | I     |  |
| YS<br>FHAN<br>OF   | NO       | Mean <sup>e</sup> | 11   | 10   | 1    | 11   | 11   | 6    | 8    | 6    | 8    | ٢    | 10   | 11   | 117   |  |
| OF DA<br>MORE T    | CIPITATI | 1985              | 12   | ŝ    | 11   | :    | 10   | 12   | 6    | 6    | 9    | ٢    | 14   | 13   | 119   |  |
| NO<br>WITH<br>0.01 | PRE      | 1984              | 13   | 12   | 12   | 7    | 14   | 10   | 11   | 8    | 7    | 80   | 10   | 13   | 125   |  |
| ION<br>ENT         | /ATER    | Meand             | 3.59 | 3.30 | 3.96 | 3.89 | 3.75 | 3.39 | 3.69 | 3.98 | 3.50 | 3.34 | 3.78 | 3.68 | 43.84 |  |
| CIPITAT<br>QUIVAI  | S OF M   | 1985              | 1.25 | 1.72 | 1.93 | 0.69 | 5.11 | 5.34 | 5.19 | 4.62 | 1.60 | 1.48 | 5.67 | 1.25 | 35.85 |  |
| PRE<br>IN E        | INCHE    | 1984              | 1.52 | 4.72 | 3.49 | 4.37 | 8.14 | 3.53 | 6.54 | 1.23 | 2.24 | 2.79 | 1.83 | 2.56 | 42.96 |  |
|                    | AYS      | Normalc           | 1101 | 963  | 831  | 492  | 220  | 20   | 0    | 0    | 49   | 285  | 585  | 955  | 5501  |  |
|                    | GREE D.  | 1985              | 1197 | 908  | 713  | 423  | 138  | 43   | 0    | 7    | 54   | 278  | 541  | 1032 | 5329  |  |
|                    | Ĕ        | 1984              | 1188 | 819  | 952  | 508  | 227  | 18   | 0    | 0    | 104  | 219  | 593  | 761  | 5389  |  |
| AYS<br>TEMP.       | 90 ±F    | Mean <sup>b</sup> | 0    | 0    | 0    | 0    | *    | -    | ĸ    | 2    | *    | 0    | 0    | 0    | 9     |  |
| 0. OF D/           | EEDED    | 1985              | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 7    | -    | 0    | 0    | 0    | e.    |  |
| N N                | EXC      | 1984              | 0    | 0    | 0    | 0    | 0    | 2    | 2    | 2    | 0    | 0    | 0    | 0    | 6     |  |
| щ                  | RE F     | Mean <sup>a</sup> | 28.3 | 30.5 | 37.9 | 48.0 | 58.4 | 67.8 | 73.4 | 71.9 | 65.2 | 54.8 | 44.2 | 33.2 | 51.1  |  |
| AVERAG             | PERATU   | 1985              | 26.2 | 32.3 | 41.8 | 50.8 | 60.9 | 65.6 | 73.6 | 72.8 | 66.6 | 56.0 | 46.6 | 31.4 | 52.1  |  |
|                    | TEM      | 1984              | 26.6 | 36.5 | 34.1 | 47.9 | 57.8 | 71.0 | 73.1 | 74.8 | 63.3 | 57.7 | 45.0 | 40.2 | 52.3  |  |
|                    |          |                   | Jan  | Feb  | Mar  | Apr  | May  | Jun  | InL  | Aug  | Sep  | Oct  | Nov  | Dec  | YEAR  |  |

t 1<del>963-1985</del> 1958-1980

e 1949-1985

National Oceanic and Atmospheric Administration Environmental Data Service

Extracted From: Local Climatological Data Charts

\* Less than 0.5

a 1903-1985 b 1960-1985 c 1951-1980 d 1955-1985

U.S. Department of Commerce

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### ANNUAL WIND ROSE FOR 1984 BRADLEY INTERNATIONAL AIRPORT WINDSOR LOCKS, CONNECTICUT



### ANNUAL WIND ROSE FOR 1985 BRADLEY INTERNATIONAL AIRPORT WINDSOR LOCKS, CONNECTICUT



### ANNUAL WIND ROSE FOR 1984 NEWARK INTERNATIONAL AIRPORT NEWARK, NEW JERSEY







### X. ATTAINMENT AND NON-ATTAINMENT OF NAAQS IN CONNECTICUT'S AQCR'S

The attainment status designations for Connecticut's four Air Quality Control Regions (AQCR's, see Figure 31) with regard to the National Ambient Air Quality Standards (NAAQS) have been determined for 1985 for the following pollutants: total suspended particulates (TSP); sulfur dioxide (SO<sub>2</sub>); ozone (O<sub>3</sub>); nitrogen dioxide (NO<sub>2</sub>); carbon monoxide (CO); and lead (Pb). Table 33 shows the attainment status of each AQCR by pollutant. The AQCR's are classified as attainment, non-attainment or unclassifiable. These classifications conform to federal EPA guidelines and were applied in each case only after federal approval was granted. The federal EPA classifies an AQCR as attainment for a particular pollutant when all standards are attained (i.e., short term, long term, primary and secondary, wherever applicable). This notwithstanding, Table 33 contains the AQCR classifications with respect to all relevant short-term and long-term standards.



### CONNECTICUT'S COMPLIANCE BY AQCR WITH THE NAAQS IN 1985

| Pollutant       | Primary<br>or<br><u>Secondary</u> | NAAQS             | AQCR   | AQCR   | AQCR<br>43 | AQCR<br>44 |
|-----------------|-----------------------------------|-------------------|--------|--------|------------|------------|
| TSP             | Primary                           | Annual<br>24-Hour | A<br>A | A<br>A | A<br>A     | A<br>A     |
|                 | Secondary                         | Annual<br>24-Hour | A<br>X | A<br>X | A<br>X     | A<br>X     |
| SO <sub>2</sub> | Primary                           | Annual<br>24-Hour | A<br>A | A<br>A | A<br>A     | A<br>A     |
|                 | Secondary                         | 3-Hour            | А      | А      | А          | Α          |
| Ozone           | Both                              | 1-Hour            | Х      | x      | x          | х          |
| NO <sub>2</sub> | Both                              | Annual            | A      | А      | А          | А          |
| со              | Both                              | 1-Hour<br>8-Hour  | A<br>U | A<br>X | A<br>X     | A<br>U     |
| Lead            | Both                              | 3-Month           | A      | A      | A          | A          |

X = Non-Attainment U = Unclassifiable A = Attainment

### XI. CONNECTICUT SLAMS AND NAMS NETWORK

On May 10, 1979, the U.S. Environmental Protection Agency made public its final rulemaking for ambient air monitoring and data reporting requirements in the "Federal Register" (Vol. 44, No. 92). These regulations are meant to ensure the acceptability of air measurement data, the comparability of data from all monitoring stations, the cost-effectiveness of monitoring networks, and timely data submission for assessment purposes. The regulations address a number of key areas including quality assurance, monitoring methodologies, network design and probe siting. Detailed requirements and specific criteria are provided which form the framework for ambient air quality monitoring. These regulations apply to all parties conducting ambient air quality monitoring for the purpose of supporting or complying with environmental regulations. In particular, state/local control agencies and industrial/private concerns involved in air monitoring are directly influenced by specific requirements, compliance dates and recommended guidelines.

### **QUALITY ASSURANCE**

The regulations specify the minimum quality assurance requirements for State and Local Air Monitoring Stations (SLAMS) networks, National Air Monitoring Stations (NAMS) networks, and Prevention of Significant Deterioration (PSD) air monitoring. Two distinct and equally important functions make up the quality assurance program: assessment of the quality of monitoring data by estimating their precision and accuracy, and control of the quality of the data by implementation of quality control policies, procedures, and corrective actions. (See Part E of Section I, Quality Assurance).

The data assessment requirements entail the determination of precision and accuracy for both continuous and manual methods. A one-point precision check must be carried out at least once every other week on each automated analyzer used to measure SO<sub>2</sub>, NO<sub>2</sub>, CO and O<sub>3</sub>. Standards from which the precision check test data are derived must meet specifications detailed in the regulations. For manual methods, precision checks are to be accomplished by operating co-located duplicate samplers. In addition, precision checks for lead are also accomplished by analysis of duplicate strips. In 1985, Connecticut maintained three co-located TSP monitors (Bridgeport 009, Hartford 003, and Waterbury 005) and one co-located lead sampler (Waterbury 123), and performed duplicate strip analyses at four sites (Hartford 016, New Haven 018, New Haven 123, and Waterbury 123).

Accuracy determinations for automated analyzers  $(SO_2, NO_2, CO, O_3)$  are accomplished by audits performed by an independent auditor utilizing equipment and gases which are disassociated from the normal network operations. Accuracy determinations are accomplished via traceable standard flow devices for hi-vols and via spiked strip analyses for lead. For SLAMS analyzers, accuracy audits must be performed on each analyzer at least once per calendar year. Each PSD analyzer must be audited at least once each calendar quarter.

All precision and accuracy data are derived through calculation methods specified by the regulations, with the results reported quarterly on Data Assessment Report Forms. The NAMS network is actually part of the SLAMS network; so the SLAMS accuracy determinations also apply to the NAMS network. The distinguishing characteristics of NAMS are: 1) only continuous instruments are used to monitor gaseous pollutants; 2) the regulations specify a minimum number and locations for them; and 3) the data, in addition to being included in the annual report, are reported quarterly to EPA.

In order to control the quality of data, the monitoring program must have operational procedures for each of the following activities:

- 1. Installation of equipment,
- 2. Selection of methods, analyzers, or samplers,
- 3. Zero/span checks and analyzer adjustments,
- 4. Calibration,
- 5. Control limits for zero/span and other control checks, and respective corrective actions when such limits are exceeded,
- 6. Control checks and their frequency,
- 7. Preventive and remedial maintenance,
- 8. Calibration and zero/span checks for multi-range analyzers,
- 9. Recording and validating data, and
- 10. Documentation of quality control information.

### MONITORING METHODOLOGIES

Except as otherwise stated within the regulations, the monitoring methods used must be "reference" or "equivalent," as designated by the EPA. Table 34 lists methods used in Connecticut's network in 1985 which were on the EPA-approved list as of September 18, 1980. Additional updates to these approved methods are provided through the "Federal Register."

### **NETWORK DESIGN**

The regulations also describe monitoring objectives and general criteria to be applied in establishing the SLAMS networks and for choosing general locations for new monitors. Criteria are also presented for determining the location and number of monitors. These criteria serve as the framework for all State Implementation Plan (SIP) monitoring networks that were to be complete and in operation by January 1, 1984.

The SLAMS network must be designed to meet four basic monitoring objectives: (1) to determine the highest pollutant concentration in the area; (2) to determine representative concentrations in areas of high population density; (3) to determine the ambient impact of significant sources or source categories; and (4) to determine general background concentration levels. Proper siting of a monitor requires precise specification of the monitoring objectives, which usually includes a desired spatial scale of representativeness. The spatial scales of representativeness are specified in the regulations for each pollutant and monitoring objective. The 1985 SLAMS and NAMS networks in Connecticut are presented and described in Table 35.

### PROBE SITING

Location and exposure of monitoring probes have been an area of confusion for a number of years because of conflicting guidelines and a lack of guidance or recommended criteria. The probe siting criteria promulgated in the regulations are specific. They are also sufficiently comprehensive to define the requirements for ensuring the uniform collection of compatible and comparable air quality data.

These criteria are detailed by pollutant and include vertical and horizontal probe placement, spacing from obstructions and trees, spacing from roadways, probe material and sample residence time, and various other considerations. A summary of the probe siting criteria is presented in Table 36. The siting criteria generally apply to all spatial scales except where noted. The most notable exception is spacing from roadways which is dependent on traffic volume.

For the chemically reactive gases  $SO_2$ ,  $NO_2$ , and  $O_3$ , the regulations specify borosilicate glass, FEP teflon or their equivalent as the only acceptable probe materials. Additionally, in order to minimize the

effects of particulate deposition on probe walls, sampling probes for reactive gases must have residence times of less than 20 seconds.

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U. S. EPA-APPROVED MONITORING METHODS USED IN CONNECTICUT IN 1985

|                  |  | Monitoring Methods           |                          |
|------------------|--|------------------------------|--------------------------|
| <u>Pollutant</u> | Reference Manual                         | Reference Automated          | Equivalent Automated     |
| TSP              | High Volume Method                       |                              |                          |
| 50 <sub>2</sub>  |  |                              | Thermo Electron 43 (0.5) |
| 03               |  | Bendix 8002 (0.5)            |                          |
| СО               |  | Bendix 8501-5CA (50)         |                          |
| NO <sub>2</sub>  |  | Thermo Electron 14 B/E (0.5) |                          |
| Lead             | High Volume Method<br>Low Volume Method* |                              |                          |
|                  |  |                              |                          |

\* This is a modified reference method approved by EPA on 2/29/84.

( ) = Approved range in ppm

| Town        | <u>Urban Area</u> | Site | SLAMS<br>or<br><u>NAMS</u> | Sampling & Analytic<br>Method | Operating<br>Schedule | Monitoring Objective | Spatial Scale and<br><u>Representativeness</u> |
|-------------|-------------------|------|----------------------------|-------------------------------|-----------------------|----------------------|--|
|             |                   |      |                            | SULFUR DIC                    | XIDE                  |                      |  |
| Bridgeport  | Bridgeport        | 012  | s                          | <b>Pulsed Fluorescence</b>    | Continuous            | High Concentration   | Neichhorhood                                   |
| Bridgeport  | Bridgeport        | 123  | z                          | <b>Pulsed Fluorescence</b>    | Continuous            | Population           | Neighborhood                                   |
| Danbury     | Danbury           | 123  | S                          | Pulsed Fluorescence           | Continuous            | Population           | Neichborhood                                   |
| E. Hartford | Hartford          | 005  | S                          | Pulsed Fluorescence           | Continuous            | Population           | Naiabhorbood                                   |
| East Haven  | New Haven         | 003  | S                          | Pulsed Fluorescence           | Continuous            | Population           | Naiabhorhood                                   |
| Enfield     | Springfield/      | 005  | s                          | Pulsed Fluorescence           | Continuous            | Backaround           | Reginatiou                                     |
|             | Hartford          |      |                            |                               |                       |                      |  |
| Greenwich   | Stamford          | 017  | S                          | Pulsed Fluorescence           | Continuous            | Background           | lirhan   |
| Groton      | New London/       | 007  | s                          | <b>Puised Fluorescence</b>    | Continuous            | Population           | Neighborhood                                   |
|             | Norwich           |      |                            |                               |                       |                      |  |
| Hartford    | Hartford          | 123  | S                          | Puised Fluorescence           | Continuous            | Population           | Nainhharhand                                   |
| Milford     | Bridgeport        | 002  | S                          | <b>Pulsed Fluorescence</b>    | Continuous            | Source               | Middle   |
| New Britain | New Britain       | 011  | s                          | <b>Puised Fluorescence</b>    | Continuous            | High Concentration   | Neighborhood                                   |
| New Haven   | New Haven         | 017  | S                          | <b>Pulsed Fluorescence</b>    | Continuous            | Population           | Neighborhood                                   |
| New Haven   | New Haven         | 123  | z                          | Pulsed Fluorescence           | Continuous            | High Concentration   | Neighborhood                                   |
| Norwalk     | Norwalk           | 013  | S                          | Pulsed Fluorescence           | Continuous            | Population           | Neighborhood                                   |
| Preston     | New London/       | 002  | S                          | Pulsed Fluorescence           | Continuous            | Backaround           | Regional                                       |
|             | Norwich           |      |                            |                               |                       |                      |  |
| Stamford    | Stamford          | 025  | S                          | <b>Pulsed Fluorescence</b>    | Continuous            | Population           | Neighborhood                                   |
| Stamford    | Stamford          | 123  | S                          | Pulsed Fluorescence           | Continuous            | High Concentration   | Neighborhood                                   |
| Waterbury   | Waterbury         | 123  | S                          | Pulsed Fluorescence           | Continuous            | Population           | Neighborhood                                   |
|             |                   |      |                            |                               |                       |                      |  |

# **1985 SLAMS AND NAMS SITES IN CONNECTICUT**

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# **1985 SLAMS AND NAMS SITES IN CONNECTICUT**

| Spatial Scale and<br><u>Representativeness</u> |               | Neighborhood                         | Neighborhood<br>Neighborhood |      |   | Neighborhood     | Urban            | Neiahborhood     | Regional         | Urban              |         | Urban              | Neighborhood     | Urban              | Urban              |           | Micro              | Micro              | Micro                     | Micro              | Micro              |
|--|---------------|--------------------------------------|------------------------------|------|---|------------------|------------------|------------------|------------------|--------------------|---------|--------------------|------------------|--------------------|--------------------|-----------|--------------------|--------------------|---------------------------|--------------------|--------------------|
| <u>Monitoring Objective</u>                    |               | High Concentration                   | High Concentration           |      |   | Population       | Population       | Population       | Background       | High Concentration |         | High Concentration | Population       | High Concentration | High Concentration |           | High Concentration | High Concentration | <b>High Concentration</b> | High Concentration | High Concentration |
| Operating<br><u>Schedule</u>                   | <u>OXIDES</u> | Continuous                           | Continuous                   | ш    |   | Continuous       | Continuous       | Continuous       | Continuous       | Continuous         |         | Continuous         | Continuous       | Continuous         | Continuous         | NOXIDE    | Continuous         | Continuous         | Continuous                | Continuous         | Continuous         |
| Sampling & Analytic<br>Method                  | NITROGEN      | Chemiluminescent<br>Chemiluminescent | Chemiluminescent             | OZON | : | Chemiluminescent | Chemiluminescent | Chemiluminescent | Chemiluminescent | Chemiluminescent   |         | Chemiluminescent   | Chemiluminescent | Chemiluminescent   | Chemiluminescent   | CARBON MO | NDIR               | NDIR               | NDIR                      | NDIR               | NDIR               |
| SLAMS<br>or<br><u>NAMS</u>                     |               | Ś                                    | ŝ                            |      | : | z                | S                | z                | S                | S                  |         | z                  | z                | z                  | z                  |           | s                  | S                  | S                         | S                  | S                  |
| Site   |               | 123<br>003                           | 123                          |      |   | 123              | 123              | 003              | 017              | 008                |         | 007                | 123              | 001                | 007                |           | 004                | 017                | 002                       | 007                | 020                |
| <u>Urban Area</u>                              |               | Bridgeport<br>Hartford               | New Haven                    |      |   | Bridgeport       | Danbury          | Hartford         | Stamford         | New London/        | Norwich | Hartford           | New Haven        | NONE               | Bridgeport         |           | Bridgeport         | Hartford           | New Britain               | New Haven          | Stamford           |
| Town   |               | Bridgeport<br>E. Hartford            | New Haven                    |      |   | Bridgeport       | Danbury          | E. Hartford      | Greenwich        | Groton             |         | Middletown         | New Haven        | Stafford           | Stratford          |           | Bridgeport         | Hartford           | New Britain               | New Haven          | Stamford           |

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|-------------|-------------------|------|---------------------|--------------------|--------------------|-----------------------|---------------------------|---|
| Town        | <u>Urban Area</u> | Site | SLAMS<br>or<br>NAMS | Sampling<br>Method | Analytic<br>Method | Operating<br>Schedule | Monitoring Objective      | Spatial Scale and<br>Representativeners |
|             |                   |      |                     |                    |                    |                       |                           |   |
|             |                   |      |                     | TOTAL              | SUSPENDED PA       | <b>RTICULATES</b>     |                           |   |
| Ansonia     | Bridgeport        | 004  | s                   | Hi-Vol             | Gravimetric        | 6 <sup>th</sup> dav   | Population                | Neighborhood                            |
| Bridgeport  | Bridgeport        | 001  | z                   | Hi-Vol             | Gravimetric        | 6th day               | Population                | Neighborhood                            |
| Bridgeport  | Bridgeport        | 600  | Z                   | Hi-Vol             | Gravimetric        | 6th day               | Population                | Neighborhood                            |
| Bridgeport  | Bridgeport        | 123  | z                   | Hi-Vol             | Gravimetric        | 6th day               | High Concentration        | Neighborhood                            |
| Bristol     | Bristol           | 001  | Ś                   | Hi-Vol             | Gravimetric        | 6th day               | Population                | Neiahborhood                            |
| Burlington  | NONE              | 001  | S                   | Hi-Vol             | Gravimetric        | 6th day               | Background                | Regional                                |
| Danbury     | Danbury           | 002  | z                   | Hi-Vol             | Gravimetric        | 6th day               | High Concentration        | Neiahborhood                            |
| Danbury     | Danbury           | 123  | z                   | Hi-Vol             | Gravimetric        | 6th day               | Population                | Neiahborhood                            |
| E. Hartford | Hartford          | 004  | S                   | Hi-Vol             | Gravimetric        | 6th day               | Population                | Neiahborhood                            |
| Greenwich   | Stamford          | 008  | S                   | Hi-Vol             | Gravimetric        | 6th day               | Population                | Neiahborhood                            |
| Groton      | New London/       | 006  | s                   | Hi-Vol             | Gravimetric        | 6th day               | Population                | Neiahborhood                            |
|             | Norwich           |      |                     |                    |                    | •                     |                           |   |
| Hartford    | Hartford          | 003  | z                   | Hi-Vol             | Gravimetric        | 6 <sup>th</sup> dav   | High Concentration        | Neighborhood                            |
| Hartford    | Hartford          | 013  | z                   | Hi-Vol             | Gravimetric        | 6th day               | High Concentration        | Neiahborhood                            |
| Hartford    | Hartford          | 014  | z                   | Hi-Vol             | Gravimetric        | 6th day               | Population                | Neighborhood                            |
| Manchester  | Hartford          | 001  | s                   | Hi-Vol             | Gravimetric        | 6 <sup>th</sup> day   | Population                | Neiahborhood                            |
| Meriden     | Meriden           | 002  | z                   | Hi-Vol             | Gravimetric        | 6 <sup>th</sup> day   | High Concentration        | Neighborhood                            |
| Middletown  | Hartford          | 003  | S                   | Hi-Vol             | Gravimetric        | 6 <sup>th</sup> day   | Population                | Neighborhood                            |
| Milford     | Bridgeport        | 002  | S                   | Hi-Vol             | Gravimetric        | 6 <sup>th</sup> day   | Population                | Neighborhood                            |
| Morris      | NONE              | 001  | S                   | Hi-Vol             | Gravimetric        | 6 <sup>th</sup> day   | Background                | Regional                                |
| Naugatuck   | Waterbury         | 001  | S                   | Hi-Vol             | Gravimetric        | 6th day               | Population                | Neighborhood                            |
| New Britain | New Britain       | 007  | z                   | Hi-Vol             | Gravimetric        | 6th day               | <b>High Concentration</b> | Neighborhood                            |
| New Britain | New Britain       | 008  | z                   | Hi-Vol             | Gravimetric        | 6th day               | Population                | Neighborhood                            |
| New Britain | New Britain       | 600  | z                   | Hi-Vol             | Gravimetric        | 6th day               | High Concentration        | Neighborhood                            |
| New Haven   | New Haven         | 002  | z                   | Hi-Vol             | Gravimetric        | 6 <sup>th</sup> day   | High Concentration        | Neighborhood                            |
| New Haven   | New Haven         | 013  | z                   | Hi-Vol             | Gravimetric        | 6th day               | Population                | Neighborhood                            |

### TABLE 35, CONTINUED

## **1985 SLAMS AND NAMS SITES IN CONNECTICL**

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# **1985 SLAMS AND NAMS SITES IN CONNECTICUT**

| Spatial Scale and<br>Representativeness |                   | Neichhorhood       | Neighbornood       | Noiabharhaad | Neighborhood |         | Mainthorhood       | Neighborhood       | Neighborhood | Neighborhood | Noiabhachaod | Neigribornood | Regional          | Neighborhood |                          | Neignbornood | Neighborhood        | Neighborhood |      | Neighborhood | Neighborhood |                    |            | Neighborhood        | Neighborhood        | Neiahborhood | Neighborhood        |
|---|-------------------|--------------------|--------------------|--------------|--------------|---------|--------------------|--------------------|--------------|--------------|--------------|---------------|-------------------|--------------|--------------------------|--------------|---------------------|--------------|------|--------------|--------------|--------------------|------------|---------------------|---------------------|--------------|---------------------|
| Monitoring Objective                    |                   | High Concentration | High Concentration | Population   | Population   | -       | High Concentration | High Concentration | Population   | Population   | Population   | Perkaroni     | Periodical Contra | Population   | Population<br>Bonulation | ropulation   | High Concentration  | Population   |      | Population   | Population   | High Concentration |            | Population          | Population          | Population   | Population          |
| Operating<br>Schedule                   | <b>RTICULATES</b> | 6th dav            | 6th day            | 6th day      | 6th day      | •       | 6th dav            | 6th day            | 6th day      | 6th day      | 6th day      | 6 th day      | 6th day           | 6th day      | 6th day                  |              | 6 <sup>th</sup> day | 6th day      |      | 6th day      | 6th day      | 1 month            |            | o <sup>rn</sup> day | 6 <sup>th</sup> day | 6th day      | 6 <sup>th</sup> day |
| Analytic<br>Method                      | SUSPENDED PA      | Gravimetric        | Gravimetric        | Gravimetric  | Gravimetric  |         | Gravimetric        | Gravimetric        | Gravimetric  | Gravimetric  | Gravimetric  | Gravimetric   | Gravimetric       | Gravimetric  | Gravimetric              |              | Gravimetric         | Gravimetric  | IEAD | Atomic Abs.  | Atomic Abs.  | Atomic Abs.        | A42        | Atomic Abs.         | Atomic Abs.         | Atomic Abs.  | Atomic Abs.         |
| Sampling<br><u>Method</u>               | TOTAL             | Hi-Vol             | Hi-Vol             | Hi-Vol       | Hi-Vol       |         | Hi-Vol             | Hi-Vol             | Hi-Vol       | Hi-Vol       | Hi-Vol       | Hi-Vol        | Hi-Vol            | Hi-Vol       | Hi-Vol                   |              | 107-1H              | Hi-Vol       |      | Hi-Vol       | Hi-Vol       | Lo-Vol             |            |                     | Hi-Vol              | Hi-Vol       | Hi-Vol              |
| SLAMS<br>or<br><u>NAMS</u>              |                   | S                  | z                  | z            | s            |         | z                  | z                  | z            | s            | S            | Ś             | 2                 | z            | ŝ                        | , 2          | 2                   | Ś            |      | s            | S            | s                  | v          | <b>n</b> 1          | S                   | S            | Z                   |
| Site                                    |                   | 001                | 005                | 012          | 002          |         | 001                | 007                | 021          | 005          | 001          | 001           | 001               | 005          | 006                      | 200          | 100                 | 002          |      | 004          | <b>6</b> 00  | 010                | 172        | <u>[</u> ]          | 001                 | 002          | 014                 |
| <u>Urban Area</u>                       |                   | Norwalk            | Norwalk            | Norwalk      | New London/  | Norwich | Stamford           | Stamford           | Stamford     | Bridgeport   | NONE         | NONE          | New Haven         | Waterbury    | Waterbury                | Waterhury    | valci Dui y         | NONE         |      | Bridgeport   | Bridgeport   | Bridgeport         | Bridgenort |                     | Bristol             | Danbury      | · Hartford          |
| Town                                    |                   | Norwalk            | Norwalk            | Norwalk      | Norwich      |         | Stamford           | Stamford           | Stamford     | Stratford    | Torrington   | Voluntown     | Wallingford       | Waterbury    | Waterbury                | Waterhury    |                     | Willimantic  |      | Ansonia      | Bridgeport   | Bridgeport         | Bridgenort |                     | Bristol             | Danbury      | Hartford            |

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# **1985 SLAMS AND NAMS SITES IN CONNECTICUT**

| Town        | <u>Urban Area</u> | <u>Site</u> | SLAMS<br>or<br><u>NAMS</u> | Sampling<br><u>Method</u> | Analytic<br>Method | Operating<br>Schedule | Monitoring Objective      | Spatial Scale and<br><u>Representativenes</u> s |
|-------------|-------------------|-------------|----------------------------|---------------------------|--------------------|-----------------------|---------------------------|---|
|             |                   |             |                            |                           | LEAD               |                       |                           |   |
| Hartford    | Hartford          | 015         | S                          | Lo-Vol                    | Atomic Abs.        | 1 month               | High Concentration        | Micro   |
| Hartford    | Hartford          | 016         | z                          | Lo-Vol                    | Atomic Abs.        | 1 month               | High Concentration        | Micro   |
| Meriden     | Meriden           | 002         | S                          | Hi-Vol                    | Atomic Abs.        | 6 <sup>th</sup> day   | Population                | Neighborhood                                    |
| Middletown  | Hartford          | 003         | S                          | Hi-Vol                    | Atomic Abs.        | 6 <sup>th</sup> day   | Population                | Neighborhood                                    |
| New Britain | New Britain       | 007         | S                          | Hi-Vol                    | Atomic Abs.        | 6th day               | Population                | Neighborhood                                    |
| New Haven   | New Haven         | 016         | S                          | Lo-Vol                    | Atomic Abs.        | 1 month               | High Concentration        | Micro   |
| New Haven   | New Haven         | 018         | S                          | Lo-Vol                    | Atomic Abs.        | 1 month               | High Concentration        | Middle  |
| New Haven   | New Haven         | 123         | s                          | Hi-Vol                    | Atomic Abs.        | 6th day               | High Concentration        | Middle  |
| Norwalk     | Norwalk           | 012         | S                          | Hi-Vol                    | Atomic Abs.        | 6th day               | Population                | Neighborhood                                    |
| Stamford    | Stamford          | 001         | S                          | Hi-Vol                    | Atomic Abs.        | 6th day               | Population                | Neighborhood                                    |
| Stamford    | Stamford          | 022         | s                          | Lo-Vol                    | Atomic Abs.        | 1 month               | <b>High Concentration</b> | Neighborhood                                    |
| Wallingford | New Haven         | 001         | S                          | Hi-Vol                    | Atomic Abs.        | 6th day               | Population                | Neighborhood                                    |
| Waterbury   | Waterbury         | 007         | S                          | Hi-Vol                    | Atomic Abs.        | 6th day               | Population                | Neighborhood                                    |
| Waterbury   | Waterbury         | 123         | S                          | Hi-Vol                    | Atomic Abs.        | 6th day               | High Concentration        | Middle  |
| West Haven  | New Haven         | 003         | s                          | Lo-Vol                    | Atomic Abs.        | 1 month               | High Concentration        | Middle  |

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### SUMMARY OF PROBE SITING CRITERIA

|                            | Other Spacing Criteria | <ol> <li>The sampler should be &gt; 20 meters from any trees.</li> <li>The distance from the sampler to an obstacle, such as a building, must be at least twice the height the obstacle protrudes above the sampler.<sup>b</sup></li> <li>There must be unrestricted air flow 270 degrees around the sampler.</li> <li>No furnace or incineration flues should be nearby.<sup>c</sup></li> <li>The sampler must have minimum spacing from roads. This varies with the height of the monitor and the spacial scale.</li> </ol> | <ol> <li>The probe should be &gt; 20 meters from any trees.</li> <li>The distance from the inlet probe to an obstacle, such as a building, must be at least twice the height the obstacle protrudes above the inlet probe.<sup>b</sup></li> <li>There must be unrestricted air flow 270 degrees around the inlet probe, or 180 degrees if the probe is on the side of a building.</li> <li>No furnace or incineration flues should be nearby.<sup>c</sup></li> </ol> | <ol> <li>The probe should be &gt; 20 meters from any trees.</li> <li>The distance from the inlet probe to an obstacle, such as a building, must be at least twice the height the obstacle protrudes above the inlet probe.</li> <li>There must be unrestricted air flow 270 degrees around the inlet probe, or 180 degrees if the probe is on the side of a building.</li> <li>The spacing from roads varies with traffic.<sup>d</sup></li> </ol> |
|----------------------------|------------------------|---|--|---|
| Height<br>Above            | uround<br>(meters)     | 2 - 15  | 7  | 3 - 15  |
| n Supporting<br>(meters)   | Horizontala            | >2  | 7  | 7   |
| Distance fron<br>Structure | Vertical               |   | 3 - 15   | 7   |
|                            | Spatial Scale          | AII   | All  | All   |
|                            | Pollutant              | TSP   | 50 <sub>2</sub>  | °O  |

|                     | A                               |
|---------------------|---------------------------------|
| TABLE 36, CONTINUED | SUMMARY OF PROBE SITING CRITERI |

|                            | and an an and a second second | The second second second second second second second second second second second second second second second se   |   |   |
|----------------------------|-------------------------------|---|---|---|
|                            | Other Spacing Criteria        | <ol> <li>The probe must be &gt;10 meters from any<br/>intersection and should be at a midblock location.</li> <li>The probe must be 2-10 meters from the edge of<br/>the nearest traffic lane.</li> <li>There must be unrestricted airflow 180 degrees<br/>around the inlet probe.</li> </ol> | <ol> <li>There must be unrestricted airflow 270 degrees<br/>around the inlet probe, or 180 degrees if the probe<br/>is on the side of a building.</li> <li>The spacing from roads varies with traffic.<sup>d</sup></li> </ol> | <ol> <li>The probe should be &gt; 20 meters from any trees.</li> <li>The distance from the inlet probe to an obstacle, such as a building, must be at least twice the height the obstacle protrudes above the inlet probe.<sup>b</sup></li> <li>There must be unrestricted air flow 270 degrees around the inlet probe, or 180 degrees if the probe is on the side of a building.</li> <li>The spacing from roads varies with traffic.<sup>d</sup></li> </ol> |
| Height<br>Above            | urouna<br>(meters)            | 2   | 7   | 7   |
| n Supporting<br>(meters)   | Horizontala                   | 7   | 7   | 7   |
| Distance fron<br>Structure | Vertical                      | 3±1/2   | 3 - 15  | 3 - 15  |
|                            | Spatial Scale                 | Micro   | Middle<br>Neighborhood  | AII   |
|                            | Pollutant                     | 9   |   | NO2   |

<sup>a</sup> When the probe is located on a rooftop, this separation distance is in reference to walls, parapets, or penthouses located on the roof.

<sup>b</sup> Sites not meeting this criterion would be classified as middle scale.

<sup>c</sup> Distance is dependent upon height of furnace or incineration flue, type of fuel or waste burned, and quality of fuel (sulfur and ash content). This is to avoid undue influences from minor pollutant sources.

<sup>d</sup> Distance is dependent upon traffic ADT, pollutant, and spatial scale.

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### XII. EMISSIONS INVENTORY

The State of Connecticut maintains a computerized emissions inventory which contains a <u>point</u> <u>source</u> file of approximately 7,000 stationary industrial, commercial, and institutional sources of air pollution. Emissions from these sources are determined on the basis of actual operating data for 1985, such as actual fuel use and actual material throughputs, and with the help of pollutant emission factors contained in the Compilation of Air Pollutant Emission Factors, designated as EPA publication AP-42.

This inventory does not account for all the pollution sources in the state, however. There are a host of other industrial, commercial, agricultural, and human activities that account for most of the pollution emitted into Connecticut's air. These sources cannot be individually inventoried either because of their nature, or large numbers, or widespread occurrence, etc. In spite of this, the emissions from these so-called <u>area souces</u> can be quantified by various means. For example, motor vehicle emissions can be determined from Connecticut Department of Transportation figures on vehicle-miles travelled on interstate and local roads, and from EPA MOBILE 3 emission factors; commercial and residential fuel-burning emissions can be determined from U. S. Department of Energy data, census figures, and AP-42 emission factors; and national per capita emissions, which are available from EPA for a number of pollution-causing activities, can be used in conjunction with census figures to calculate emissions by town, county, region, etc.

Together the computerized point source inventory and the more indirectly arrived at, but much larger, area source inventory provide a good picture of the pollutants that are emitted into Connecticut's air each year. Table 37 summarizes the actual in-state emissions of each of the five (5) major air pollutants in Connecticut -- TSP, SO<sub>2</sub>, CO, NO<sub>2</sub>, and volatile organic compounds or VOC, -- by county, for 1985. The table reveals two things. First, the most populous counties have the largest pollutant totals; second, excluding SO<sub>2</sub>, which is largely generated by utilities, area sources (mobile sources in particular) account for the bulk of the total emissions.

County names and geographic locations are displayed in Figure 32, which also serves as a reference for the charts that follow.

Figures 33 through 47 give various visual displays of the level of emissions for each of the major air pollutants. Figures 33, 36, 39, 42, and 45 are pie charts that show the percent of each air pollutant for Connecticut's eight (8) counties. Figures 34, 37, 40, 43, and 46 are pictorial displays of emissions by county, where the darker areas indicate higher emission levels. Figures 35, 38, 41, 44, and 47 are three dimensional graphs of each county's contribution to statewide emissions.

### **1985 CONNECTICUT EMISSIONS INVENTORY BY COUNTY**

|               |         |                | TONS P          | ER YEAR OF     | EMISSIONS       |                 |
|---------------|---------|----------------|-----------------|----------------|-----------------|-----------------|
| <u>County</u> | Sources | TSP            | <u>SO</u> 2     | <u>co</u>      | voc             | <u>NO</u> x1    |
| Fairfield     | Area    | 8,068.7        | 4,507.6         | 129,306.1      | 31,700.2        | 27,299.1        |
|               | Point   | <u>2,129.1</u> | <u>28,863.2</u> | <u>3,934.7</u> | <u>3,987.3</u>  | <u>13,292.7</u> |
|               | All     | 10,197.8       | 33,370.8        | 133,240.8      | 35,687.5        | 40,591.8        |
| Hartford      | Area    | 8,912.2        | 4,605.5         | 134,872.4      | 32,848.0        | 28,120.2        |
|               | Point   | <u>800.0</u>   | <u>3,582.8</u>  | <u>532.7</u>   | <u>3,942.9</u>  | <u>2,887.7</u>  |
|               | All     | 9,712.2        | 8,188.3         | 135,405.1      | 36,790.9        | 31,007.9        |
| Litchfield    | Area    | 2,553.5        | 914.0           | 29,603.4       | 8,685.6         | 5,414.7         |
|               | Point   | <u>180.3</u>   | <u>682.5</u>    | <u>67.3</u>    | <u>942.7</u>    | <u>299.0</u>    |
|               | All     | 2,733.8        | 1596.5          | 29,670.7       | 9628.3          | 5,713.7         |
| Middlesex     | Area    | 2,296.1        | 915.9           | 28,535.1       | 7,768.7         | 5,604.9         |
|               | Point   | <u>880.1</u>   | <u>7,393.5</u>  | <u>532.9</u>   | <u>728.1</u>    | <u>5,707.5</u>  |
|               | All     | 3,176.2        | 8,309.4         | 29,068.0       | 8,496.8         | 11,312.4        |
| New Haven     | Area    | 7,874.2        | 4,174.2         | 106,698.2      | 28,096.6        | 23,640.6        |
|               | Point   | <u>1,169.5</u> | <u>24,571.9</u> | <u>921.0</u>   | <u>5,117.4</u>  | <u>7,871.5</u>  |
|               | All     | 9,043.7        | 28,746.1        | 107,619.2      | 33,214.0        | 31,512.1        |
| New London    | Area    | 3,849.4        | 1,589.8         | 50,208.3       | 13,575.8        | 9,859.2         |
|               | Point   | <u>1,066.3</u> | <u>13,577.2</u> | <u>477.9</u>   | <u>2,002.2</u>  | <u>4,172.7</u>  |
|               | All     | 4,915.7        | 15,167.0        | 50,686.2       | 15,578.0        | 14,031.9        |
| Tolland       | Area    | 2,104.9        | 709.6           | 26,028.9       | 7,111.2         | 5,280.2         |
|               | Point   | <u>108.8</u>   | <u>935.2</u>    | <u>48.5</u>    | <u>111.5</u>    | <u>321.4</u>    |
|               | All     | 2,213.7        | 1,644.8         | 26,077.4       | 7,222.7         | 5,601.6         |
| Windham       | Area    | 1,897.8        | 562.9           | 20,916.5       | 5,945.4         | 3,734.1         |
|               | Point   | <u>238.5</u>   | <u>549.9</u>    | <u>840.4</u>   | <u>637.9</u>    | <u>320.7</u>    |
|               | All     | 2,136.3        | 1,112.8         | 21,756.9       | 6,583.3         | 4,054.8         |
| TOTAL         | Area    | 37,556.9       | 17,979.5        | 526,168.8      | 135,731.5       | 108,953.0       |
|               | Point   | <u>6,572.6</u> | <u>80,156.1</u> | <u>7,355.5</u> | <u>17,470.0</u> | <u>34,873.2</u> |
|               | All     | 44,129.5       | 98,135.6        | 533,524.3      | 153,201.5       | 143,826.2       |

<sup>1</sup> NO<sub>x</sub> emissions are expressed as NO<sub>2</sub>


### <u>1985 CONNECTICUT EMISSIONS INVENTORY BY COUNTY</u> <u>TOTAL SUSPENDED PARTICULATES</u>

(TOTAL TONS PER YEAR : 44,130)



## 1985 TOTAL SUSPENDED PARTICULATES Total Emissions by County



## 1985 TOTAL SUSPENDED PARTICULATES Total Emissions by County



Three Dimensional View of TSP Emissions

### 1985 CONNECTICUT EMISSIONS INVENTORY BY COUNTY SULFUR DIOXIDE

### (TOTAL TONS PER YEAR : 98,136)











Three Dimensional View of S02 Emissions

### 1985 CONNECTICUT EMISSIONS INVENTORY BY COUNTY CARBON MONOXIDE

### (TOTAL TONS PER YEAR : 533,524)



1985 CARBON MONOXIDE Total Emissions by County





Three Dimensional View of CO Emissions

### <u>1985 CONNECTICUT EMISSIONS INVENTORY BY COUNTY</u> <u>VOLATILE ORGANIC COMPOUNDS</u>

(TOTAL TONS PER YEAR : 153,202)





### 1985 VOLATILE ORGANIC COMPOUNDS Total Emissions by County





Three Dimensional View of VOC Emissions

### 1985 CONNECTICUT EMISSIONS INVENTORY BY COUNTY NITROGEN OXIDES

(Expressed as Nitrogen Dioxide)

### (TOTAL TONS PER YEAR : 143,826)





# 1985 NITROGEN OXIDES (Expressed as Nitrogen Dioxide)

Total Emissions by County





### 1985 NITROGEN OXIDES (Expressed as Nitrogen Dioxide)

Total Emissions by County



Three Dimensional View of NOx Emissions

### XIII. PUBLICATIONS

The following is a partial listing of technical papers and study reports dealing with various aspects of Connecticut air pollutant levels and air quality data.

Bruckman, L., *Asbestos: An Evaluation of Its Environmental Impact in Connecticut*, internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, March 12, 1976.

Lepow, M. L., L. Bruckman, R.A. Rubino, S. Markowitz, M. Gillette and J. Kapish, "Role of Airborne Lead in Increased Body Burden of Lead in Hartford Children," Environ. Health Perspect., May, 1974, pp. 99-102.

Bruckman, L. and R.A. Rubino, "Rationale Behind a Proposed Asbestos Air Quality Standard," paper presented at the 67th Annual Meeting of the Air Pollution Control Association, Denver, Colorado, June 9-11, 1974, J. Air Pollut. Cntr. Assoc., 25: 1207-15 (1975).

Rubino, R.A., L. Bruckman and J. Magyar, "Ozone Transport," paper presented at the 68th Annual Meeting of the Air Pollution Control Association, Boston, Massachusetts, June 15-20, 1975, J. Air Pollut. Cntr. Assoc.: 26, 972-5 (1976).

Bruckman, L., R.A. Rubino and T. Helfgott, "*Rationale Behind a Proposed Cadmium Air Quality Standard*," paper presented at the 68th Annual Meeting of the Air Pollution Control Association, Boston, Massachusetts, June 15-20, 1975.

Rubino, R.A., L. Bruckman, A. Kramar, W. Keever and P. Sullivan, "Population Density and its *Relationship to Airborne Pollutant Concentrations and Lung Cancer Incidence in Connecticut,*" paper presented at the 68th Annual Meeting of the Air Pollution Control Association, Boston, Massachusetts, June 15-20, 1975.

Lepow, M.L., L. Bruckman, M. Gillette, R.A. Rubino and J.Kapish, "Investigations into Sources of Lead in the Environment of Urban Children," Environ. Res., 10: 415-26 (1975).

Bruckman, L., E. Hyne and P. Norton, "A Low Volume Particulate Ambient Air Sampler," paper presented at the APCA Specialty Conference entitled "Measurement Accuracy as it Relates to Regulation Compliance," New Orleans, Louisiana, October 26-28, 1975, APCA publication SP-16, Air Pollution Control Association, Pittsburgh, Pennsylvania, 1976.

Bruckman, L. and R.A. Rubino, "High Volume Sampling Errors Incurred During Passive Sample Exposure Periods," J. Air Pollut. Cntr. Assoc., 26: 881-3 (1976).

Bruckman, L., R.A. Rubino and B. Christine, "Asbestos and Mesothelioma Incidence in Connecticut," J. Air Pollut. Cntr. Assoc., 27: 121-6 (1977).

Bruckman, L., Suspended Particulate Transport in Connecticut: An Investigation Into the *Relationship Between TSP Concentrations and Wind Direction in Connecticut*, internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, December 24, 1976.

Bruckman, L. and R.A. Rubino, "Monitored Asbestos Concentrations in Connecticut," paper presented at the 70th Annual Meeting of the Air Pollution Control Association, Toronto, Ontario, June 20-24, 1977.

Bruckman, L., "Suspended Particulate Transport," paper presented at the 70th Annual Meeting of the Air Pollution Control Association, Toronto, Ontario, June 20-24, 1977.

Bruckman, L., "A Study of Airborne Asbestos Fibers in Connecticut," paper presented at the "Workshop in Asbestos: Definitions and Measurement Methods" sponsored by the National Bureau of Standards/U.S. Department of Commerce, July 18-20, 1977.

Bruckman, L., "Monitored Asbestos Concentrations Indoors," paper presented at The Fourth Joint Conference of Sensing Environmental Pollutants, New Orleans, Louisiana, November 6-11, 1977.

Bruckman, L., paper presented at the Joint Conference on Applications of Air Pollution Meteorology, Salt Lake City, Utah, November 28 - December 2, 1977.

Bruckman, L., E. Hyne, W. Keever, "A Comparison of Low Volume and High Volume Particulate Sampling," internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, 1976.

"Data Validation and Monitoring Site Review," (part of the Air Quality Maintenance Planning Process), internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, June 15, 1976.

"Air Quality Data Analysis," (part of the Air Quality Maintenance Planning Process), internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, August 16, 1976.

Bruckman, L., "Investigation into the Causes of Elevated SO2 Concentrations Prevalent Across Connecticut During Periods of SW Wind Flow," paper presented at the 71st Annual Meeting of the Air Pollution Control Association, Paper #78-16.4, Houston, Texas, June 25-29, 1978.

Anderson, M.K., "Power Plant Impact on Ambient Air: Coal vs. Oil Combustion," paper presented at the 68th Annual Meeting of the Air Pollution Control Association, Paper #75-33.5, Boston, MA, June 15-20, 1975.

Anderson, M.K., G. D. Wight, "New Source Review: An Ambient Assessment Technique," paper presented at the 71st Annual Meeting of the Air Pollution Control Association, Paper #78-2.4, Houston, TX, June 25-29, 1978.

Wolff, G.T., P.J. Lioy, G.D. Wight, R.E. Pasceri, "Aerial Investigation of the Ozone Plume Phenomenon," J. Air Pollut.8 Control Association, 27: 460-3 (1977).

Wolff, G.T., P.J. Lioy, R.E. Meyers, R.T. Cederalll, G.D. Wight, R.E. Pasceri, R.S. Taylor, "Anatomy of Two Ozone Transport Episodes in the Washington, D.C., to Boston, Mass., Corridor," Environ. Sci. Technol., 11-506-10 (1977).

Wolff, G.T., P.J. Lioy, G.D. Wight, R.E. Meyers, and R.T Cederwall, "*Transport of Ozone Associated With an Air Mass*," In: Proceed. 70 Annual Meeting APCA, Paper 377-20.3, Toronto, Canada, June, 1977.

Wight, G.D., G.T. Wolff, P.J. Lioy, R.E. Meyers, and R.T.Cederwall, "Formation and Transport of Ozone in the Northeast Quadrant of the U.S.," In: Proceed. ASTM Sym. Air Quality and Atmos. Ozone, Boulder, Colo., Aug. 1977.

Wolff, G.T., P.J. Lioy, and G.D. Wight, "An Overview of the Current Ozone Problem in the Northeastern and Midwestern U.S.," In: Proceed. Mid-Atlantic States APCA Conf. on Hydrocarbon Control Feasibility, p. 98, New York, N.Y., April, 1977.

Wolff, G.T., P.J. Lioy, G.D. Wight, R.E. Meyers, and R.T.Cederwall, "An Investigation of Long-Range Transport of Ozone Across the Midwestern and Eastern U.S.," Atmos. Environ. 11:797 (1977).

 $\mathbb{P}(\mathbf{r}_{n_{1},\dots,n_{k}}^{(n)}) = \mathbb{E}_{\mathbf{r}_{n_{1},\dots,n_{k}}^{(n)}}$ 

| Pollutant<br>NO2<br>กระวัฒนาไป<br>ประวัญชาติ เป็นสายเหตุ (การเป็นการเป็นการเป็นการเป็นการเป็นการเป็นการเป็นการเป็นการเป็นการเป็นการเป | Town/Site<br>Bridgeport 123<br>East Hartford 003<br>New Haven 123  | <b>Objective</b><br>High Conc.<br>High Conc.<br>High Conc. |
|---|--|--|
| ovati malà e di di Ozone di di  | New Haven 123<br>Stratford 007                                     | Population<br>High Conc.                                   |
| TBREAD AND AND AND AND AND AND AND AND AND A  | Bridgeport 009<br>Danbury 002<br>Danbury 123<br>New Britain 007    | Population<br>High Conc.<br>Population<br>High Conc.       |
| TE mant le groe an leg et an le se<br>Balais I de mart Bagen an agrica  | New Britain 008<br>Stratford 007<br>Waterbury 005<br>Waterbury 007 | Population<br>High Conc.<br>Population<br>High Conc.       |
| tin begensternet i stran en fer SO2 and taken.<br>N   | Bridgeport 123<br>Milford 002<br>New Haven 123                     | High Conc.<br>Source<br>High Conc                          |

• Regarding previous Air Quality Summaries:

- and the second second
  - 1. In Section I.B. of the 1978-1981 editions, a portion of the third sentence in the third paragraph should be rewritten to read: "...the statewide average and standard deviation of the mean pollutant concentrations at the sites..."
- 2. Figure 1 and all references thereto should be ignored in favor of Figure 1 in the 1983 edition.
- 3. Table 2 in the 1978-1981 editions should be ignored in favor of relevant portions of Table 3 in the 1983 edition.

Paragraph I.F.2.b in the 1983 edition should be inserted into the appropriate areas of Section I.F in the 1978-1981 editions.

Table 7 in the 1981 edition is incomplete. The site Stamford 021 should be inserted with a first high of 85 on July 9 and a second high of 83 on March 29.

6. Table 22 in the 1981 edition contains erroneous data. The correct data can be found in Table 22 in the 1983 edition.

- 7. In the 1978-1981 editions, the last sentence in the second paragraph of Section VIII. CLIMATOLOGICAL DATA should be deleted.
- 8. In the 1981 edition, the same corrections should be made to Table 32 that were listed in Item 21 of the foregoing section regarding the 1982 Air Quality Summary.

### ERRATA REPORTED IN THE 1982 AIR QUALITY SUMMARY

 Regarding the 1975 TSP data, all references to the following monitoring sites should be ignored: Enfield 123, Enfield 001/123, Danbury 001, Danbury 123, Danbury 001/123, Groton 001, Groton 123, Groton 001/123, Torrington 001, Torrington 123, Torrington 001/123. These sites either had insufficient data for a valid annual average concentration or they included data from two different sites.

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- Regarding 1976 TSP data, all references to the following monitoring sites should be ignored: Stamford 003, Stamford 123, Stamford 003/123. These sites either had insufficient data for a valid annual average concentration or they included data from two different sites.
- Regarding 1980 TSP data, the following corrections have been made:
  - 1. Bridgeport 001: The number of samples for the year at this site has been changed from 57 to 58, and the annual geometric mean concentration has been changed from 47.8 to 47.6  $\mu$ g/m<sup>3</sup>.
  - 2. Bridgeport 123: the annual geometric mean concentration at this site has been changed from 64.2 to  $63.8 \mu g/m^3$ .
  - 3. Greenwich 016: All references to this site should be ignored. This site is considered to have been unsuitably located for acceptable particulate monitoring.
  - 4. Morris 001: The standard deviation of the sampling data at this site has been changed from 1.567 to 1.557.
- Regarding 1981 TSP data, the following corrections have been made:
  - 1. Bristol 001: The number of samples for the year at this site has been changed from 55 to 58, and the annual geometric mean concentration has been changed from 34.1 to 34.6  $\mu$ g/m<sup>3</sup>.
- Regarding TSP data for the years 1975 through 1981, all references to sites Torrington 123 and Waterbury 123 should be ignored. These sites are now considered to have been unsuitably located for acceptable particulate monitoring.
- The above corrections, where relevant, are implicit in Table 2 and Table 8 of the 1982 Air Quality Summary. Accordingly, versions of these tables found in post-1974 (and pre-1982) editions of this document contain erroneous information and should be ignored or appropriately footnoted.
- Regarding Table 2, some of the earlier editions of this document have contained versions of this table which appeared to present annual "arithmetic" mean data. This is incorrect. All versions of this table contain annual "geometric" mean data.

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