# CONNECTICUT AIR QUALITY SUMMARY

1978

DEPARTMENT
OF
ENVIRONMENTAL
PROTECTION
STANLEY J. PAC, COMMISSIONER

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Cover by Rosemary Gutbrod CONNECTICUT AIR QUALITY SUMMARY - 1978
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April, 1980

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## I. INTRODUCTION

This summary of 1978 ambient air quality levels in Connecticut is a compilation of all air pollutant measurements made at Department of Environmental Protection (DEP) air monitoring network sites in the State.

# A. Overview of Air Pollutant Concentrations in Connecticut

The following paragraphs briefly describe the status of Connecticut's air quality. The measured concentrations of six pollutants are compared to Federal and State air quality standards. There are two categories of air quality standards: primary - established to protect public health; and secondary - established to protect plants and animals and to prevent economic damage. A more detailed discussion of each of these pollutants is provided in subsequent sections of this Annual Summary.

# Total Suspended Particulates (TSP)

The measured TSP level exceeded the primary annual standard (75  $\mu g/m^3$ ) in Waterbury at site 123, and measured TSP levels exceeded the secondary annual standard (60  $\mu g/m^3$ ) at 10 sites in 1978. No sites recorded measured values exceeding the primary 24-hour standard (260  $\mu g/m^3$ ) in 1978, but 9 sites did exceed the secondary 24-hour standard (150  $\mu g/m^3$ ) (see Table 1).

In general, measured Total Suspended Particulate levels in Connecticut showed a small, but significant improvement in 1978 as compared to 1977. This improvement is believed to have been primarily caused by a decreased frequency of southwest winds in 1978, compared to 1977, which reduced the amount of TSP transported into Connecticut from the southwest.

# 2. Sulfur Dioxide (SO<sub>2</sub>)

None of the air quality standards for sulfur dioxide were exceeded in Connecticut in 1978. Measured concentrations were substantially below the 80  $\mu g/m^3$  primary annual standard, the 365  $\mu g/m^3$  primary 24-hour standard, and the 1300  $\mu g/m^3$  secondary 3-hour standard. Measured concentrations were closer to, but were also below, the 60  $\mu g/m^3$  secondary annual standard and the 260  $\mu g/m^3$  secondary 24-hour standard.

The continued attainment of the SO<sub>2</sub> standards is primarily attributable to Connecticut's regulation which restricts the sulfur content in fuel to .5%.

The results of sulfation rate monitoring show that sulfur dioxide levels improved significantly from 1977 to 1978. (However, this improvement was not observed in the data obtained from instruments that measure  $SO_2$  directly, probably because there was insufficient data available in 1977 to compare with 1978.) The general improvement in  $SO_2$  levels was probably primarily due to improved meteorological conditions, most notably a decreased frequency of southwest winds and an associated reduction in the transport of  $SO_2$ .

## 3. <u>Ozone</u> $(0_3)$

New NAAQS - On February 8, 1979 the EPA established a new ambient air quality standard for ozone of 0.12 ppm. This standard replaces the old photochemical oxidant standard of 0.08 ppm. The definition of the pollutant was changed along with the numerical value partly because the instruments used to measure photochemical oxidants in the air really measure only ozone. Ozone is only one of a group of chemicals which are formed photochemically in the air and are called photochemical oxidants. In the past, the two terms have often been used interchangeably. This 1978 Annual Summary uses the term "ozone" in conjunction with the new NAAQS to reflect the changes in both the numerical value of the NAAQS and its definition.

The new primary 1-hour ozone standard was exceeded at all the DEP monitoring sites in 1978 (see Table 1).

The frequency and magnitude of levels in excess of the 0.12 ppm ozone standard decreased from 1977 to 1978. Some of this difference is attributable to the loss of a large amount of data during July of 1978 due to instrument problems. The remainder of this apparent improvement in air quality may be real, but only temporary, because it can be attributed to year-to-year variations in weather conditions. Although the Federal emission controls on motor vehicles should be bringing about a yearly reduction in ozone precursor emissions, these emission reductions are not large enough to account for the improvement in ozone levels.

# 4. <u>Nitrogen Dioxide (NO<sub>2</sub>)</u>

Measured nitrogen dioxide levels were lower than the 100  $\mu g/m^3$  primary annual standard at all the sampling sites in Connecticut. A statistical analysis of the data also demonstrates, with 95% confidence, that every site achieved the annual standard for NO2.

A small improvement in  $NO_2$  levels took place between 1977 and 1978. Since 60% of the  $NO_2$  emissions in Connecticut come from motor vehicles, some of this improvement could be attributable to the Federal emission control program for motor vehicles, but most of the improvement is probably due to meteorological changes.

# 5. <u>Carbon Monoxide (CO)</u>

The primary eight-hour standard of 9 ppm was exceeded at eight of the nine carbon monoxide monitoring sites in Connecticut (Bridgeport 004, Greenwich 001, Hartford 012, New Britain 002, New Haven 007, Norwalk 005, Stamford 020, and Waterbury 004) in 1978. The number of times the 8-hour standard was exceeded ranged from twice each at the Greenwich 001 site and the New Haven 007 site up to 104 times at the New Britain 002 site and 366 times at the Stamford 020 site. Hartford 009 was the only

site that did not exceed this standard.

No site, except Stamford 020, violated the primary one-hour standard of 35 ppm. The one-hour standard was exceeded seven times at the Stamford 020 site in 1978 (see Table 1).

No significant change in carbon monoxide levels took place between 1977 and 1978.

#### 6. <u>Lead (Pb)</u>

New NAAQS - On October 5, 1978, the EPA established a new ambient air quality standard for lead of 1.5  $\mu g/m^3$  for a calendar quarter-year average. The standard is attained only if the quarterly averages of all four calendar quarters in a year do not exceed 1.5  $\mu g/m^3$ .

The newly promulgated primary NAAQS for lead (1.5  $\mu g/m^3$ , calendar quarter average) was exceeded at 16 sites in 1978 (see Table 1).

No significant change in measured concentrations of lead occurred between 1977 and 1978.

TABLE 1 AIR QUALITY STANDARDS EXCEEDED IN CONNECTICUT IN 1978

LEAD Quarterly	Exc	Maximum Number Quarter of			2.24	1	1.82	1.51	1	1:	1.78			1	1	1	1.79		1.74	1.97	1.70	1 7	99.1	1.58	1.85	)   	2.48	- 1	i i	1.95	1 69	- I	2.52 3	1.55
CARBON MONOXIDE 8-Hour/1-Hour	Exce	Level	(9 ppm/35 ppm) Times			13.5/- 27/-	1		1	1		1 6	-/2 -/1.01		1		7 6 6	7/11 -/1.71		1		. 1	15.4/- 104/*		1	12.3/- 2/-		.3/-	27.5/39.0 366/7	1	1	11.4/- 11/-	1	1
0ZONE 1-Hour	2nd High Number		10.12 ppiii) ITIMES	. 1	,	0.201	.211				0.167 48		0.240 75	- ~				0.202		0.162 26	0.184	1		1	1	1 1 2 200 0	0.225	1		í	1	<b>.</b>	1 1	
Secondary 24-Hour Standard Exceeded	2nd High Number	Level of (150 ug/m <sup>3</sup> ) Times	j	182 9	1	184 8	1	•	1	1	1	1	1	1		160		1	1		ı	1		5 +0-		212	162	3	217	237	} I	249 17	1	
TOTAL SUSPENDED Level Exceeding Annual Standard	1	(75 µg/m <sup>3</sup> ) (60 µg/m <sup>3</sup> )		- 62.5	1	- 66.4	1	ı		1	1		1 .	ı	1	- 64.6	1	- 67.1	- 60.7	- 62.2	i 1 1	; t	- 60		1	- 74.0		1		- 62,3		80.0	1	
		TOWN			bridgeport 004			F21 461111	70.03		4					Hartford 003			5		ıck	Ë			_	eu	,		=			waterbury 123		

#### B. Trends

Any attempt to assess statewide trends in air pollution levels must be able to overcome the tendency for local changes to obscure the statewide pattern. In order to reach some statistically valid conclusions concerning trends in pollutant levels in Connecticut, the DEP has applied the Wilcoxon Matched Pairs, Signed Rank Statistical Test to the annual average data for three pollutants. The Wilcoxon test has been applied to 1968-1978 Total Suspended Particulate (TSP) data, to 1968-1978 Sulfation rate/Sulfur Dioxide (SO2) data, and to 1973-1978 Nitrogen Dioxide (NO2) data.

The Wilcoxon Test is a non-parametric test of high power and efficiency which can be used to ascertain if there was a statistically significant change (increase or decrease) in the annual average pollutant concentrations at all the monitoring sites in Connecticut. This test makes it possible to overcome the trend analyses problems which arise due to the changes in the number and location of monitoring sites from year to year and the problems associated with making equitable comparisons among sites. The annual mean levels for consecutive years are compared at each site; there is no inter-site comparison. Data for two consecutive years are required and the size of the change (increase or decrease) is noted. For example, if a high proportion of sites experienced an increase and/or if the magnitude of an increase at several sites is of much greater importance than the magnitude of a decrease at other sites, the test will show if the increase was statistically significant for those two years.

The results of the Wilcoxon test for TSP, Sulfation rate/SO2, and NO2 are presented in Tables 2, 3, and 4, respectively. These analyses were performed only on data computed for sites where the U.S. Environmental Protection Agency (EPA) minimum sampling criteria (see Table 5) were met. The years of data that were paired, the number of sites used, and the statewide arithmetic mean and standard deviation of the pollutant concentrations at the sites are provided in the first four columns of each table. The statistical significance of any changes in the statewide pollutant averages is provided in the last three columns of each table. The significance of change is indicated, by arrows, for two confidence limits, 95% and 99%, and is also given numerically as the number of chances in 10,000 under the heading "actual significance of change". For example, the statewide annual average for TSP decreased between 1968 and 1969 from 73.6 to 66.9. The downward arrows indicate that this change was significant at the 95% and 99% confidence levels. The "actual significance of change" is given as 0.0075. Thus, there are only 75 chances in 10,000 that this measured decrease in TSP levels did not occur.

in Connecticut was limited to a sulfur content not to exceed 1.0%. As of September 1, 1972, the sulfur content of the oil sold in Connecticut could not exceed 0.5%, and the burning of oil with a higher sulfur content than 0.5% was not allowed after April 1, 1973. The inescapable conclusion is that the implementation of these sulfur-in-fuel regulations caused the significant reduction in  $SO_2$  levels from 1970 to 1973, such that all  $SO_2$  standards have been attained in Connecticut. During the winter of 1973 to 1974, certain utilities were given emergency permission to burn higher sulfur oil and coal. The temporary increase in  $SO_2$  levels observed in 1974 could have been due, in part, to this relaxation of the sulfur-infuel limitations.

The long-term trend of  $SO_2$  concentrations, as determined from the sulfation rate data, is shown in graphical form in Figure 2.

## 3. $N0_2$

The Wilcoxon test shows that  $NO_2$  levels in Connecticut have fluctuated up and down over the last five years, but no overall trend can be observed (see Table 4). The  $NO_2$  levels dropped significantly from 1973 to 1974 and from 1977 to 1978, and they rose significantly from 1974 to 1975 and from 1976 to 1977. No significant change in  $NO_2$  levels occurred between 1975 and 1976.

These fluctuations must be largely attributed to year to year changes in meteorology as no corresponding changes in emissions are known to have occurred in the last five years. In the long run, the Federal program to control motor vehicle emissions should bring about a drop in  $NO_2$  levels. The  $NO_2$  measurement method changed several times during 1973, 1974, and 1975 which could have caused some of the fluctuation in levels in those years.

TABLE 2
TSP TREND, 1968-1978 (WILCOXON SIGNED-RANK TEST)

		AVERAGE OF		SIGNIFICANCE LEVEL ACTUAL									
PAIRED YEARS	NUMBER OF SITES	ANNUAL GEOMETRIC MEANS*	STANDARD DEVIATION	TREN 95% level**	<u> 99% level**</u>	SIGNIFICANCE OF CHANGE							
68 69	17 17	73.6 66.9	21.6 18.6	¥	¥	0.0075							
69 70	21 21	69.0 71.7	23.0 25.5	N.C.	N.C.	0.2891							
70 71	23 23	67.8 66.2	20.6 18.2	N.C.	N.C.	0.3458							
71 72	40 40	68.4 61.9	22.5 17.3	<b>†</b>	+	0.0013							
72 73	39 39	59.1 51.9	13.4 10.2	<b>↓</b>	<b>+</b>	<0.00005							
73 74	41 41	51.9 48.3	11.6 10.3	<b>\</b>	N.C.	0.0143							
74 75	40 40	49.9 52.3	10.7 10.1	<b>†</b>	N.C.	0.0101							
75 76	31 31	52.8 53.0	9.8 9.3	N.C.	N.C.	0.7539							
76 77	37 37	54.9 54.7	10.4 10.1	N.C.	N.C.	0.7296							
77 78	32 32	55.9 53.8	10.7 10.2	<b>↓</b>	<b>+</b>	0.0086							

<sup>\*</sup> Note that as the year pairings change, the sites available also change. This explains the different averages for a given year, i.e., the averages are taken from different sets of sites.

N.C. = No Significant Change

<sup>\*\*</sup> Key to Symbols: \(\psi = \text{Significant Downward Trend}\) \(\phi = \text{Significant Upward Trend}\)

TABLE 3
SULFATION RATE/SO<sub>2</sub> TREND, 1968-1978 (WILCOXON SIGNED-RANK TEST)

		AVERAGE OF ANNUAL			SIGNIFICANCE	
PAIRED YEARS	NUMBER OF SITES	ARITHMETIC MEANS*	STANDARD DEVIATION	TRENI 95% level	) AT ** 99% level**	ACTUAL SIGNIFICANCE OF CHANGE
68 69	12 12	75.4 65.3	29.3 21.3	N.C.	N.C.	0.0619
69 70	22 22	56.6 64.4	18.8 20.3	<b>↑</b>	<b>↑</b>	0.0006
70 71	34 34	62.4 50.1	20.9 13.9	<b>\</b>	· <b>↓</b>	< 0.00005
71 72	40 40	51.6 40.3	14.9 6.8	<b>\</b>	<b>\</b>	< 0.00005
72 73	38 38	41.3 34.0	6.9 4.5	<b>.</b>	<b>\</b>	< 0.00005
73 74	25 25	35.4 38.2	5.2 6.3	<b>†</b>	<b>↑</b>	0.0004
74 75	25 25	35.9 33.2	8.2 7.8	<b>.</b>	<b>↓</b>	0.0002
75 76	18 18	33.1 33.6	7.7 6.0	N.C.	N.C.	0.1071
76 77	29 29	35.2 34.9	4.7 4.3	N.C.	N.C.	0.8009
77 78	25 25	35.1 30.4	4.2 3.4	4	<b>\</b>	<0.00005

<sup>\*</sup> Note that as the year pairings change, the sites available also change. This explains the different averages for a given year, i.e., the averages are taken from different sets of sites.

<sup>\*\*</sup> Key to Symbols: ↓ = Significant Downward Trend ↑ = Significant Upward Trend

N.C. = No Significant Change

TABLE 4

NO2 TREND, 1973-1978 (WILCOXON SIGNED-RANK TEST)

		AVERAGE OF			SIGNIFICANCE LEVEL ACTUAL									
PAIRED YEARS	NUMBER OF SITES	ANNUAL ARITHMETIC MEANS*	STANDARD DEVIATION	TRENI 95% level	O AT ** 99% level**	SIGNIFICANCE OF CHANGE								
73 74	7 7	62.0 39.7	32.7 20.0	<b>+</b>	N.C.	0.0180								
74 75	24 24	43.5 49.6	17.2 17.2	<b>†</b>	<b>†</b>	0.0004								
75 76	13 13	58.0 59.4	13.8 10.9	N.C.	N.C.	0.8140								
76 77	20 20	56.9 62.2	11.8 12.2	<b>†</b>	N.C.	0.0158								
77 78	19 19	62.3 59.2	12.6 11.5	+	N.C.	0.0166								

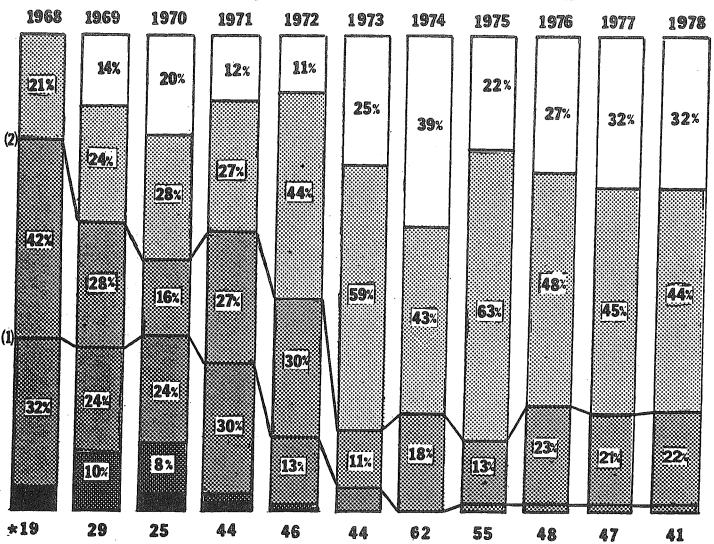
<sup>\*</sup> Note that as the year pairings change, the sites available also change. This explains the different averages for a given year, i.e., the averages are taken from different sets of sites.

<sup>\*\*</sup> Key to Symbols:  $\downarrow$  = Significant Downward Trend

<sup>↑ =</sup> Significant Upward Trend

N.C. = No Significant Change

Figure 1
Total Suspended Particulate Matter Trend



(1) Primary Annual Standard 75 µg/m³

(2)Secondary Annual Standard 60 µg/m<sup>3</sup>

\* Number of Sites

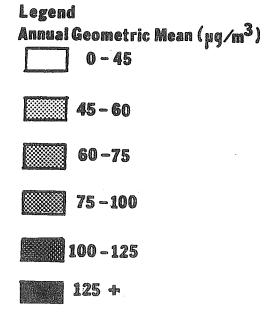
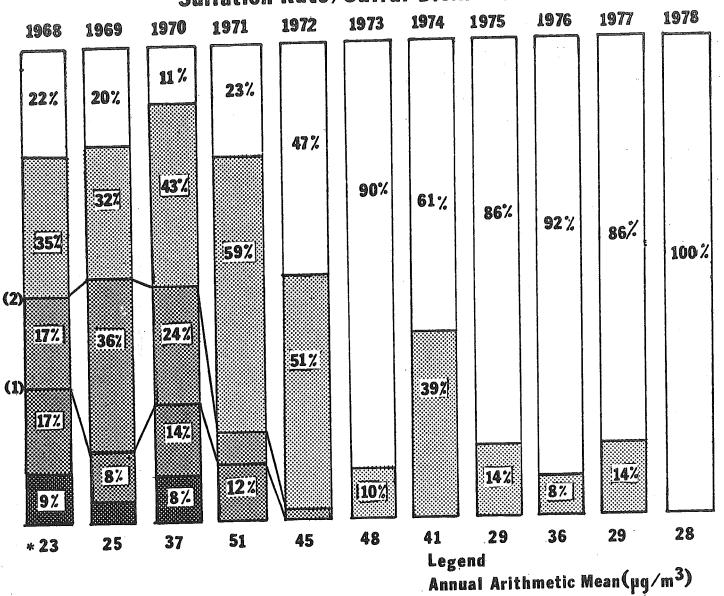
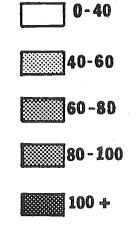


Figure 2
Sulfation Rate/Sulfur Dioxide Trend



- (1) Primary Annual Standard 80 µg/m³
- (2) Secondary Annual Standard 60 μg/m<sup>3</sup>
  - \*Number of Sites



# C. <u>Air Monitoring Network</u>

A computerized Air Monitoring network consisting of an IBM System 7 computer and 12 telemetered monitoring sites was put into full operation in 1975. Presently, up to 12 measurement parameters from each site are transmitted via telephone lines to the System 7 unit located in the DEP Hartford office. The data are then compiled into 24-hour summaries twice daily. The telemetered sites are located in the towns of Bridgeport, Danbury, Derby, Enfield, Greenwich, Groton, Hartford, Middletown, New Britain, New Haven, Stamford, and Waterbury.

Measured parameters include the pollutants sulfur dioxide, particulates (COH), carbon monoxide, ozone, and meteorological data consisting of wind speed and wind direction, wind horizontal sigma, temperature, dew point, precipitation, barometric pressure and solar radiation.

The real-time capabilities of the System 7 telemetry network have enabled the Air Monitoring Unit to report the Pollutant Standards Index for 12 towns on a daily basis while keeping a close watch for high pollution levels which may occur during adverse weather conditions throughout the year.

The complete monitoring network used in 1978 consisted of:

- 44 Total Suspended Particulate and Lead (Hi-Vol) sites
- 11 Total Suspended Particulate (Lo-Vol) sites
- 15 Sulfur Dioxide sites (Continuous Monitors)
- 12 Ozone sites
- 22 Nitrogen Dioxide sites (Bubblers)
- 9 Carbon Monoxide sites

A complete description of all permanent air monitoring sites in Connecticut operated by DEP in 1978 is available from the Department of Environmental Protection, Air Compliance, State Office Building, Hartford, Connecticut, 06115.

# D. <u>Air Quality Standards</u>

Table 5 lists analysis methods and National Ambient Air Quality Standards (NAAQS) for each pollutant. The NAAQS were established by the U.S. Environmental Protection Agency (EPA) and are divided into two categories: primary - established to protect the public health; and secondary - established to protect plants and animals and to prevent economic damage.

Each standard specifies a concentration and an exposure time developed from studies of the effect of various levels of the particular pollutant.

ASSESSMENT OF AMBIENT AIR QUALITY TABLE 5

POLLUTANT	METHOD OF ANALYSIS SAMPLING DATA PERIOD REDUCT	ALYSIS DATA REDUCTION	STATISTICAL PRIMARY BASE STANDARD  BASE STANDARD  LIGHT AIR STANDARD  PRIMARY  STANDARD  LIGHT AIR STANDARD  LIGHT AIR STANDARD  LIGHT AIR STANDARD  LIGHT AIR STANDARDS  LIGHT A	NT AIR STAI PRIMARY STANDARD µg/m³ ppi	TANDARI Y RD PPIII	SECONDARY STANDARD  ug/m³ ppm
Total Suspended Particulates	24-Hours Every Sixth Day <sup>l</sup>	24-Hour Average	Annual Geometric Mean 24-Hour Concentration <sup>3</sup>	75 260		60* 150
Sulfur Oxides (Measured as Sulfur Dioxide)	Continuous <sup>2</sup>	1-Hour Average	Annual Arithmetic Mean 24-Hour Average Concentration <sup>3</sup> 3-Hour Average Concentration <sup>3</sup>	365	.03	60 <sup>†</sup> .02 260 <sup>†</sup> .10 1300 .5
Nitrogen Dioxide	24-Hours Every Sixth Day <sup>l</sup>	24-Hour Average	Annual Arithmetic Mean	100	.05	Same as Primary
Ozone	Continuous <sup>2</sup>	1-Hour Average	1-Hour Average <sup>4</sup>	235	.12 <sup>††</sup>	Same as Primary
Hydrocarbons	Continuous <sup>2</sup>	1-Hour Average	3-Hour Average <sup>3</sup> (6-9 AM)	**09L	.24	Same as Primary
Lead	24 Hours Every Sixth Day <sup>l</sup>	Quarterly Composite	Calendar Quarter Average	1.5		Same as Primary
				mg/m <sup>3</sup>	mdd	mg/m <sup>3</sup> ppm
Carbon Monoxide	Continuous <sup>2</sup>	l-Hour Average	8-Hour Average <sup>3</sup> 1-Hour Average <sup>3</sup>	10 40	35.9	Same as Primary Same as Primary

EPA assessment criteria require at least 5 samples per calendar quarter, and, if one month has no samples, then the other two months in that quarter must have at least two samples each.

EPA assessment criteria require 75% of possible data to compute valid averages. 2 m 4 \*

Not to be exceeded more than once per year.

Not to be exceeded more than an average of once per year in three years. A guide to be used in assessing implementation plans to achieve the 24-hour standard. For use as a guide in devising implementation plans to achieve the (old) 0.08 ppm ozone standards. Secondary Standard applies to State of Connecticut only. \* +

Department of Environmental Protection has commenced a rulemaking proceeding to change the State standards from 0.08 ppm to 0.12 ppm. Units:  $_{\rm Lg/m}^3 = {\rm Milligrams} = {\rm Milligrams} = {\rm Milligram} =$ The Connecticut In 1978, the year covered by this Annual Summary, the Federal ozone standards were 0.08 ppm. +

# E. Pollutant Standards Index

The Pollutant Standards Index (PSI) is a daily air quality index recommended for common use in state and local agencies by the U.S. Environmental Protection Agency. Connecticut switched to reporting the PSI on a 7-day a week basis on November 15, 1976. The PSI incorporates five pollutants – carbon monoxide, sulfur dioxide, total suspended particulates, ozone, and nitrogen dioxide. The index converts each air pollutant concentration into a normalized number where the National Ambient Air Quality Standard for each pollutant corresponds to PSI = 100 and the Significant Harm Level corresponds to PSI = 500.

Figure 3 shows the breakdown of index values for the commonly reported pollutants (TSP, SO<sub>2</sub>, and O<sub>3</sub>) in Connecticut. In 1978, the PSI was reported for the 12 telemetered monitoring sites in Connecticut (Bridgeport, Danbury, Derby, Enfield, Greenwich, Groton, Hartford, Middletown, New Britain, New Haven, Stamford, and Waterbury). Each day the pollutant with the highest PSI value of all the pollutants being monitored is reported for each town, along with the dimensionless PSI number, and a descriptor word to characterize the daily air quality.

A telephone recording of the PSI is taped each afternoon at 3 PM, seven days a week, and can be heard by dialing 566-3449. For residents outside of the Hartford telephone exchange, the PSI is now available toll-free from the DEP representative at the Governor's State Information Bureau. The number is 1-800-842-2220. This information is also available to the public weekday afternoons from the Connecticut Lung Association in East Hartford. The number there is 289-5401.

FIGURE 3

P.S.I.

10001

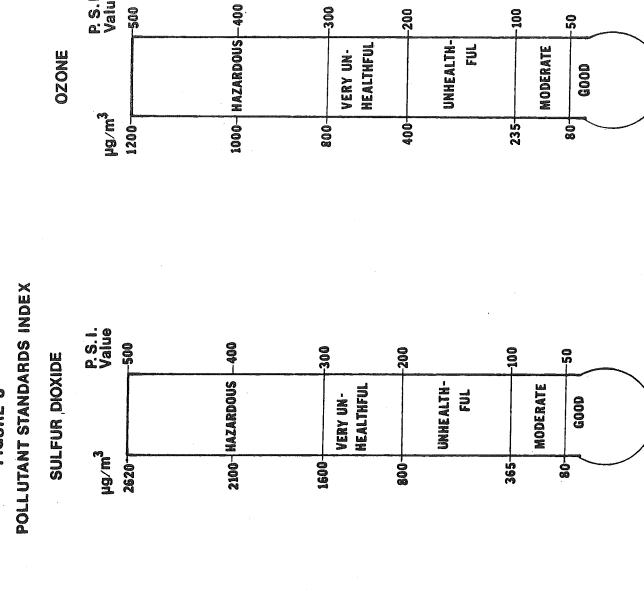
PARTICULATES

500

Value :

OZONE

500



-300

HEALTHFUL

VERY UN-

-200

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3

-100

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0000

MODERATE

875-HAZARDOUS - 400

-300

625-

VERY UN-MEALTHFUL

-200

375-

-100

260-

3

UNNEALTH-

-50

0000

2

MODERATE

#### F. Quality Assurance

A vigorous and comprehensive Quality Assurance Program for air quality data encompasses a multitude of tasks:

Personnel training

· Site selection, evaluation and review

Equipment evaluation, selection and modification when applicable

Purchasing and inventory control of consumable supplies

Instrument preventive maintenance, operation and calibration

Calibration and traceability of working standards

Sample collection and analysis

 Data recording, documentation, reduction, validation and reporting

Intra-agency and interagency cross-checks

Interlaboratory and instrument audits

With the advancement of instrument technology, personnel experience, and improved quality control and quality assurance procedures for the operation, maintenance and calibration of monitoring equipment, the data quality has improved from year to year. However, it appears that these factors could eventually be outweighed by other factors such as instrument degradation due to aging, reduction in resources, and personnel turnover (this turning point has not yet been reached).

#### 1. DEP Data Handling Criteria

The table below briefly summarizes some of the data acceptability criteria used by the DEP on data produced by DEP monitors. Data points are either unadjusted, corrected, or rejected depending upon the % of deviation from a calibrated value:

POLLUTANT	UNADJUSTED	CORRECTED	DISCARDED
	DATA	DATA	DATA
Ozone Carbon Monoxide Sulfur Dioxide Particulate* NO <sub>2</sub> *	< ± 10% < ± 5% < ± 10% < ± 7% < ± 10%	± 10% to ± 20% ± 5% to ± 15% ± 10% to ± 25% ± 7% to ± 14%	> ± 20% > ± 15% > ± 25% > ± 14% > ± 10%

Additional accept/reject criteria apply to deviations due to instrument zero drift. As a result of these checks and corrections, the data accepted for presentation in this summary are probably better than indicated by the EPA audits.

#### 2. EPA Audits

It is essential that data quality be assessed by an impartial source (EPA) who periodically performs quantitative audits on monitoring instruments, calibration systems and laboratory

<sup>\* %</sup> differences based on sampling flow rates

functions. The results of Connecticut DEP's performance are summarized here in an effort to quantify the degree of data accuracy. The following discussion describes the results for the individual pollutants.

a. Integrating Instruments (24-Hour Sample Either Every 3 Or 6 Days)

#### Particulates

a) Connecticut participated in the audits of 10 samplers using an orifice calibrated by EPA at Research Triangle Park (RTP), North Carolina. Each sampler was audited at five different flow rates for a total of 50 data points. There were seven data points, involving four samplers, which were outside the acceptable range. The discrepancies ranged from -9% to -20% (DEP lower than EPA) but six of the seven values occurred at flows which were outside the normal operating range of the instrument.

An analysis of only those 18 audit points (between 41 and 50 ft $^3$ /min.) which fell within the operating range of DEP's hi-vols, indicated that DEP's flow rates were consistently lower than EPA's (-5.3% on the average). This apparent negative bias prompted DEP to send its calibrating orifice (working standard) to EPA Region I in Boston for comparative calibration. In contrast to the results of the audit using the EPA/RTP orifice, all results now indicated that DEP's flow rates were constantly higher than EPA's. The differences ranged from + 0.3% to + 1.7% overall and from +0.3% to +1.3% within the DEP operating range. These apparent minor discrepancies could not be resolved.

b) The 3 and 1 gram weights, which are used for the laboratory balance calibrations, were certified by Connecticut's Consumer Protection Department, Weights and Measures Division, and were found to weigh 2.999746 and 0.999942 grams, respectively.

# 2) Nitrogen Dioxide

Five EPA reagent samples were analyzed at the Environmental Chemistry Laboratory of the Connecticut Health Department to determine the accuracy of DEP's analytical system. All results were within acceptable limits and ranged from +3.1% to +6.8% difference.

#### b. Continuous Instruments

#### 1) Sulfur Dioxide

Nine instrument audits were performed on the  $SO_2$  sampling network, two of which were unacceptable (+ 18% and + 21% difference). Data for that period were eliminated and both units replaced. In addition, an  $SO_2$  network transformation occurred during the year, in which more reliable instrumentation was installed. Audits of this new configuration were all acceptable, having an average difference of +6.2% and a standard deviation of  $\pm$  3.5%. Therefore, with these new instruments, the quality and quantity of the  $SO_2$  data should improve in future years.

#### 2) Ozone

During 1978, there were eight  $0_3$  instrument audits performed in Connecticut. Of these audits, there was one marginal audit (+ 15%) and two unacceptable audits (+ 39% and + 53%) which occurred at the beginning of the ozone season. The unacceptable data were caused by a faulty calibrator and all data for that period were rejected. Subsequent audits on the two problem sites were acceptable; this indicates that the apparent discrepancy had been resolved.

#### Carbon Monoxide

- a) Six CO instrument audits were performed by EPA during the year with a total of 20 data points being documented. All variations were less than 1 ppm or 10% of value, whichever was greater; i.e., all audit points were acceptable.
- b) Thirteen instrument audits were performed by DEP personnel using three tanks of unknown concentrations (low, mid, and high range) received from EPA. All high values (∿40 ppm) were within acceptable limits while the midrange (∿17 ppm) had two of thirteen audit points unacceptable (+ 12% & -22% discrepancy). The low values (in the 5 ppm region) had the tightest criteria. Three of the thirteen audit points were unacceptable although the worst discrepancy was only 1.8 ppm.

#### II. TOTAL SUSPENDED PARTICULATES

#### Conclusions:

The measured TSP level exceeded the primary annual standard in Waterbury at site 123 and measured TSP levels exceeded the secondary annual standard at 10 sites in 1978. No sites had measured values exceeding the primary 24-hour standard in 1978, but 9 sites did exceed the secondary 24-hour standard.

In general, measured total suspended particulate (TSP) levels in Connecticut showed a small, but significant improvement in 1978 as compared to 1977 (see Table 2).

The possible causes of this improvement in TSP levels range from more favorable meteorology to decreased particulate emissions. One of the most evident changes in the meteorology was that there were fewer periods of southwesterly wind flows in 1978 than in 1977. At the National Weather Service station located near Bridgeport this drop amounted to 18%, and at Bradley Airport located in Windsor Locks, the drop was 11%. A decrease in frequency of southwesterly winds causes a reduction in the transport of particulate matter into Connecticut from the New York City Metropolitan area and the other sources of emissions situated further to the southwest. As far as decreased emissions are concerned, the increasing cost of fuel and associated conservation efforts between 1977 and 1978 would be expected to decrease TSP emissions, but these efforts had to offset a 10-12% increase in degree day heating requirements, a 10-25% reduction in precipitation (which washes out particulates) and a 3-4% drop in average wind speed (less wind results in less dilution of emissions) between 1977 and 1978.

There was a 1% decline in the sale of distillate oil (used primarily in space heating) in Connecticut between 1977 and 1978, but there was a 13% increase in the sale of residual oil (used primarily by electric utilities and industries). Thus, distillate oil sales dropped in spite of the colder year, indicating considerable conservation in space heating; but part of the apparent decline in distillate oil combustion may have been offset by the increased combustion of wood, which causes more particulate emissions than oil. The utilities and industry were responsible for most of the increase in sales of residual oil. (Although sales of residual oil increased by 13%, residual oil burned increased by no more than 11% because a 2% increase in sales was due to increased stockpiling by the utilities.)

More than half of the particulate emissions in Connecticut are caused by motor vehicles. One third of these emissions are due to fuel combustion. Most of the remaining two-thirds occur when road dust is stirred up by the motion of the vehicles, so road dust emissions are not dependent upon fuel combustion, but rather, upon vehicle miles traveled (VMT's). Exact VMT's for 1977 and 1978 are unknown at this time, but the Connecticut Department of Transportation expects VMT's to increase each year. Gasoline sales in Connecticut increased by 1.6% from 1977 to 1978.

Since most sources of particulates increased their emissions (those that reduced emissions did so only slightly), and since temperature, precipitation and wind speed favored increased TSP levels, it is remarkable that TSP levels dropped between 1977 and 1978. The only obvious cause is the decreased frequency of southwest winds which reduced the amount of TSP transported into Connecticut from the southwest.

# Sample Collection and Analysis:

<u>Hi-Volume Sampler (Hi-Vol)</u>: "Hi-Vols" resemble vacuum cleaners in their operation, with an  $8" \times 10"$  piece of fiberglass filter paper replacing the vacuum bag. The samplers operate (from midnight to midnight) every sixth day at most sites and every third day at certain urban stations.

The matter collected on the filters is analyzed for weight and chemical composition. The air flow through the filter is recorded during sampling. The weight in micrograms ( $\mu g$ ) divided by the volume of air in cubic meters ( $m^3$ ) yields the pollutant concentration for the day, in micrograms per cubic meter.

The chemical composition of the suspended particulate matter is determined as follows. A standardized strip of every other hi-vol filter collected in each quarter-year is cut-out and composited into one sample.\* This procedure is repeated three times so that three quarterly composited samples are made for each site. One of the composited filter samples is digested in benzene. The organic materials in the sample dissolve and are extracted into the benzene. The benzene is evaporated and the organic residue is weighed. The weight of this residue represents the organic material in the sample and the result is reported as the benzene soluble fraction of the TSP, in  $\mu g/m^3$ . (This method of determining the benzene solubles, or organic, fraction of the particulates was used until 1977 when the analysis for benzene solubles was discontinued because of health hazards associated with the use of benzene, which is a carcinogen.) Another sample is dissolved in water, re-fluxed and the resulting solution is analyzed to determine the water soluble fraction of the TŠP using wet chemistry techniques. Results are reported for each individual constituent of the water soluble fraction in  $\mu g/m^3$ . The last composited sample is digested in acid and the resulting solution is analyzed for the different metals in the TSP using an atomic absorption spectrophotometer. Results are reported for each individual metal in μg/m<sup>3</sup>.

<sup>\*</sup>The National Air Sampling Network (NASN) every-12th - day sampling schedule determines which filters go into the composite. The National Air Sampling Network consists of several sites in each State, selected from among the State-operated monitoring sites. Filters collected on the NASN schedule at these NASN sites are used by the States only to compute TSP levels. The filters are then sent to the EPA for their analysis and use. Connecticut performs chemical analyses on non-NASN sampling day filters from the NASN sites in Connecticut and on the NASN sampling day filters from the non-NASN sites in Connecticut. (The NASN sites in Connecticut are Bridgeport 001, Hartford 002, New Haven 001 and 123, and Waterbury 001 and 123.)

LorVolume Sampler: The low-volume (i.e., Lo-Vol) sampler is a 30-day continuous sampler. It is enclosed in a shelter similar to a hi-vol, uses the same glass fiber filter paper, but operates at an air sampling flow rate approximately one-tenth that used by a standard hi-vol (i.e., 4 cfm as opposed to 40-60 cfm). The air flow through the lo-vol is measured by a temperature compensating dry gas meter. The lo-vol measurement is essentially an arithmetic average for the 30-day sampling interval. The filters are chemically analyzed in the same manner as those from the hi-vol sampler.

#### Discussion of Data:

Monitoring Network - In 1978 both hi-vol and lo-vol particulate samplers were operated in Connecticut (see Figure 4). Because the Federal EPA does not recognize the lo-vol instrument as an equivalent to the reference (hi-vol) method of sampling for TSP, only hi-vol data are analyzed for compliance with NAAQS.

Annual Averages - The Federal EPA has established minimum sampling criteria (see Table 5) for use in determining compliance with either the primary or secondary annual NAAQS for TSP. Using the EPA criteria, the primary annual standard was exceeded in Waterbury at site 123, while the secondary annual standard was exceeded at 10 sites. In 1978, of the sites that had valid annual geometric means, 23 hi-vol sites showed lower annual geometric means than in 1977, with 8 of these decreases being greater than 5  $\mu g/m^3$ . In 1978, 9 hi-vol sites showed higher geometric means than 1977, with 2 of these increases being greater than 5  $\mu g/m^3$ .

Historical Data - The DEP's historical file of annual average TSP data for 1957-1978 is presented in Table 6. The entire file of historic TSP data are presented here because some corrections have been made to the data published in earlier Annual Summaries. This table of historic TSP data invalidates and replaces all previous compilations. This table also includes, for the first time, an indication of whether the aforementioned EPA minimum sampling criteria were met at each site for each year. If the sampling was insufficient to meet the EPA criteria an asterisk appears next to the number of samples.

Statistical Projections - Table 6 is the product of a computer program listing all hi-vol monitoring sites used by DEP. The data for each site and year include the number of samples taken (generally, a maximum of 61 samples per year), the geometric mean, 95% confidence limits about the mean, the standard geometric deviation and a statistical prediction of the number of days in each year the 24-hour primary and secondary NAAQS would have been exceeded if sampling had been conducted every day. This analysis (just as the ambient standards) is based on the assumption that the particulate data are log-normally distributed.

Because manpower and economic limitations dictate that hi-vol sampling for particulate matter can not be conducted every day, a degree of uncertainty as to whether the air quality at a site has either met or exceeded the national standards is introduced. This uncertainty for the annual standard can be quantified by determining 95% confidence limits about each of the annual geometric means. For example (see Table 6), in Wallingford at site 001 in 1978, 61 samples were taken and a geometric mean of 57.0  $\mu g/m^3$  was calculated. However, the columns labeled "95-PCT-LIMITS" show the lower and upper limits for a 95% confidence interval of 50 and 65  $\mu g/m^3$ , respectively. This means that if a larger (i.e., greater than 61 samples) sample set were collected in 1978 at this site there is a 95% chance that the geometric mean would fall between these limits. Since the national secondary standard for particulates (60  $\mu g/m^3$ ) is within this interval, one cannot be 95% confident that the secondary standard was met here in 1978.

In Table 7, the 1978 monitoring sites are examined for compliance with standards, using the State's hi-vol confidence limit criteria. The table shows that no sites exceeded the primary annual standard with 95% confidence. It is uncertain whether the primary standard was achieved or exceeded at 2 sites (i.e., New Haven, site 123 and Waterbury, site 123). The table also shows that the secondary standard was exceeded at 5 sites (i.e., Bridgeport, site 123; Hartford, sites 003 and 123; New Haven, site 123; and Waterbury, site 123). Whether the secondary standard was exceeded is uncertain at 13 other sites. Comparing this to the results using the actual measured levels in the discussion above, the 95% confidence method shows one less site exceeding the primary standard and 5 less sites exceeding the secondary standard.

24-Hour Averages - Table 8 presents 1st and 2nd high 24-hour concentrations recorded at each site. There was no violation of the primary 24-hour standard recorded in 1978 or 1977. Measured violations of the secondary 24-hour standard were recorded at 9 sites in 1978, 1 more than in 1977. The 2nd high 24-hour average increased at 12 of the 32 sites which met the minimum EPA sampling criteria in both 1977 and 1978. 3 of these increases exceeded 25 μg/m³. The 2nd high 24-hour average decreased at 19 of the 32 sites, and 5 of these decreases exceeded 25 μg/m³. The 2nd high at one site (Bridgeport, site 123) remained the same.

Table 9 summarizes the statistical predictions from Table 6 regarding the number of days exceeding the 24-hour standards. This table shows that if sampling had been conducted every day in 1978 there would have been 7 sites with violations of the primary 24-hour standard, and 22 sites with violations of the secondary 24-hour standard. In 1977, only one site was predicted to have exceeded the primary 24-hour standard and 27 sites were predicted to have exceeded the secondary 24-hour standard.

Chemical Analyses - Annual averages of seventeen components or characteristics of the particulate matter collected at each hi-vol sampling location have been computed for the years 1970 through 1978 and are presented in Table 10. (Once again, some corrections have been made to the chemical analyses data reported in previous Annual Summaries, so the data presented in this 1978 Air Quality Summary supercede the data presented in all previous publications.) The abbreviations used in the table are defined below. All values shown are annual arithmetic means, in micrograms per cubic meter, except for pH.

#S		Number of Samples	٧	Vanadium
ÄĨ	-	Aluminum	Zn	Zinc
Вe	-	Berylium	N03	Total Nitrates
Cd	100	Cadmium	S04	Total Sulfates
Cr	-	Chromium	NH4	Ammon <b>i</b> um
Cu	<b>g</b> encek	Copper	Na	Sodium
Fe		Iron	рН	Acidity
Pb	aque-	Lead	BENZ	Total Benzene Solubles
Mn	==	Manganese	TSP*	Total Suspended Particulates
Νi	· -	Nickel		

Lo-Vol Averages - For 5 years, the DEP has been experimenting and gathering data with the lo-vol particulate monitor. Lo-vols operate continuously for 30 day periods. The lo-vol has four advantages and one disadvantage in relation to the hi-vol. First, the lo-vol's continuous operation can provide annual averages which include every day of the year, rather than only the fractional portion of the year sampled by every-sixth- (or third-) day hi-vol operation. Second, there is no passive sampling error (see Special Studies Section) associated with the lo-vol as there is with the standard hi-vol. Third, the lo-vol needs less frequent servicing (12 times/year) than the hi-vol (e.g., 61 times/year), so it is more cost-effective to operate. Fourth, the lo-vol has a higher collection efficiency than the hi-vol, especially for small, respirable particles. But, a disadvantage of the lo-vol is that it does not provide daily samples for direct comparison to the 24-hour TSP standards (although 24-hour averages can be obtained by statistical extrapolation).

In early 1976, hi-vol monitors at 3 remote sites and 5 rural sites were replaced by lo-vols. The use of the lo-vols made it possible to continue to obtain data on annual average particulate levels at these hard-to-service sites. Meanwhile, a lo-vol was operated alongside the hi-vol at the Hartford 003 site for comparison purposes. In 1978, lo-vols were installed at two other hi-vol sites for this purpose also. But, in 1978, hi-vols were returned to 4 of the lo-vol sites, due to the need to obtain data on 24-hour background concentrations.

Annual averages of the chemical components (and pH) of the lo-vol TSP have been computed for 1974 through 1978 and are presented in Table 11. The abbreviations used in Table 11 are identical to those used in Table 10 except for the column which indicates the number of samples. In Table 11 this column is headed "#M" to show that the number of samples and the number of months are equivalent.

<sup>\*</sup> Note that Table 10 gives the arithmetic means of the every-12th-day samples that were used in the composites, whereas Table 6 gives the geometric means of all the scheduled samples.

TABLE 6 1957-1978 TSP, ANNUAL AVERAGES AND STATISTICAL PROJECTIONS CONNECTICUT DEPARTMENT OF ENVIRONMENTAL PROTECTION

AIR COMPLIANCE MONITORING

POLLUTANT--PARTICULATES

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CONNECTICUT	T DEPARTMENT	MENT OF	ENVIRONMENTA	TABLE 6 L PROTECT	(continued ION	J) PAGE	2 AIR	S COMPLIANCE	MONITORING
POLLUTANT	-PARTICULAT	ATES.					<del></del>	DISTRIBUTION-	LOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES	GEOM MEAN	95-PCT-L LOWER	LIMITS UPPER	STD GEOM DEV	PREDICTED DAYS OVER 150 UG/M3	PREDICTED DAYS OVER 260 UG/M3
BRIDGEPORT BRIDGEPORT	02	1974	61 20*	45.7	41	51 55	1.659	<b>\$</b>	
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RIDGEPOR		76	30	• • - ~	44	09	1.550	7 7	
SI	01	76	1.8%	Ô	30		- ·	ţ.	
BRISTOL	01		υ <i>ι</i> υ 4 Φ	50°4	<b>4</b> 4 40	56	1.510	v v	
SI	10	16	58	2	24		-	4	
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IST	01	97	65	-	43		51	e-cel	
BRISTOL	02	1973	19*	28.2	23	35	1.583		i
RIS		16	61	6			69°		
BRISTOL	03	1973	18*	40.1	32	20	1.584	, <b>-4</b>	

COMPLIANCE MONITORING	RIBUTIONLOGNORMAL	AYS OVER DAYS OVER 50 UG/M3 260 UG/M3	red.	. 00	) M		e		*	-	ا ا			_	-	1 3	. 7	200	·	7		4	16		4 00	n (r	. ~	2	m	7	
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ed) PAGE		-LIMITS UPPER	40		55									31	09	. 82.	ഗ	0	101	S	70	58	91	59	. 09	63	21	65	. 67		58
PROTEETION		95-PCT LOWER	31		44									22							49				14	51		64⁄	45	<b>4</b> 8	20
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ENV I RONMENTA		SAMPLES	59	18*	59	€4.	64	19	45%	25*	99	<b>49</b> %	7%	39*	23*	28*	21*	*9I	21*	# œ	38	51	*8	*65	09	58	9	57	18*	58	09
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CONNECTICUT	POLLUTA	N	BRISTOL	BURLINGTON	BURLING	BURLING	BURLING	BURLING	DANBURY	DANBURY	DANBURY	DANBURY	DANBUR	DANBURY	DERBY	DERBY	DERBY														

CONNECTICUT DE	DEPARTMENT	ENT OF	ENVIRONMENTA		TABLE 6 (continued) PROTECTION	ed) PAGE	4 AIR	S COMPLIANCE	MONITORING
POLLUTANTPAR	PARTICULAT	ATES						DISTRIBUTION-	LOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES	GEOM MEAN	95-PCT- LOWER	-LIMITS UPPER	STD GEOM DEV	PREDICTED DAYS OVER 150 UG/M3	PREDICTED DAYS OVER 260 UG/M3
DERBY	123	1978	45*	48.5	42	55	1.604	κi	
EAST HARTFORD	01	1974	45*	2	37	49	1.605	pinel	
<u>ا</u>	01	1975	58	49.3	44		0	-	
S	01	1976	* [	S.	21	09	2.212	13	2
EAST HARTFORD	05	16	37*	41.2	36	47	1.560	[4	
<del>-</del>	02	1975	55	9	42	52		ı F4	
ST	05	16	53	9	36	47	•	2	
S	05		09	47.3	42	53	Q,	2	
F	02	16	58		44	26	9	7	
į	,								
EAST WINDSOR	0	1975	38	51.4	45	65	1,533	2	
ST	01	26		0.69	54		•51	. 10	
ENFIELD	. [0	- C	-2	,_	o ur	7 8	~	٣	
ENFIELD	010	96	4 CJ 1 PV	76.2	40	- C	9 7 0	, k	ſſ
ENFIELD	01	96	*8	0	70	141	9 (	) c	ע ה
ENFIELD	01	96	19%	, 60	52	16	9 (	ر ا ا	
ENFIELD	01	1970	22*		70	16	1.466	50	`
ENFIELD	01	1971	<b>55</b>	ô	70	46	0	45	Ŋ
ENFIELD	01	16	36	4	9	95	1.940	50	10
ENFIELD	01	1973	20	55.6	64	63	1.627	80	
	0	6	. 59	O	45	27	1.654	5	
ENFIELD	0	26	21*	7	25	92	1.558	∞	
ENFIELD	03	1972	<b>\$</b> <b>&amp;</b>	64.3	50	83	1.363	part .	
ENFIELD	123	1975	33*	38.6	33	45	Š		
ENFIELD	123	1976	56	43.2	38	49	Š	2	
ENFIELD	123	1977	. 54	40°4	37	45	8 <b>4</b> 8		
ENFIELD	123	1978	56	41.6	38		1.513		
ENFIELD 01/	123	1975	54	46.6	41	53	1.655	4	

PREDICTED ON PROPERTY OF THE P AIR COMPLIANCE MONITORING 260 UG/M3 DISTRIBUTION--LOGNORMAL -- ¢ PREDICTED DAYS OVER 150 UG/M3 10 24 16 29 5 4 \$ STD GEOM DEV 1.523 1.455 1.600 1.883 . 806 1.5584 1.567 1.600 09997 1.752 .505 •619 1.567 . 459 .624 191. e634 1 .305 1.610 1.702 1.491 S PAGE UPPER 95-PCT-LIMITS 48 48 65 65 46 52 69 60 65 51 59 78 64 61 (continued) LOWER PROTECTION TABLE 6 GEOM MEAN 62°0 55°4 53°9 38.3 65°6 43°9 56.9 46.5 49.8 36.9 43.6 42.3 52°1 62°7 54.4 54.9 44.1 59.2 66,1 **ENVIRONMENTAL** SAMPLES 36% 20% 20 27 46 54 27∜ 35\* 34% 25% ジケケ \$67 26 25 52 58 58 58 56 47 47 CONNECTICUT DEPARTMENT OF 966 967 968 969 975 969 970 971 996 970 968 973 974 975 976 977 978 YEAR 971 1972 1973 1974 972 196 POLLUTANT--PARTICULATES SITE 02 02 02 02 02 02 05 05 05 05 05 05 05 05 1000000000000 FAIRFIELD FAIRFIELD FAIRFIELD FAIRFIELD FAIRFIELD GREENWICH FAIRFIELD FAIRFIELD GREENWICH GREENWICH FAIRFIELD FAIRFIELD FAIRFIELD GREENWICH GREENWICH GREENWICH GREENWICH GREENWICH GREENWICH TOWN NAME GREENWICH GREENWICH GREENWICH

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1971 1972 973 1974 975

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GREENWICH GREENWICH GREENWICH GREENWICH GREENWICH

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CONNECTICUT	DEPARTMENT	ENT OF	ENVIRONMENTAL	TABLE 6 PROTECT	(continued)	d) PAGE	9	AIR	COMPLIANCE	MONI TORING
POLLUTANTP	ARTICUL	ATES						0	ISTRIBUTION-	-LOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES	GEOM MEAN	95-PCT-L LOWER	LIMITS UPPER	STD GEOM	DEV	PREDICTED DAYS OVER 150 UG/M3	PREDICTED DAYS OVER 260 UG/M3
$\alpha$	03		2	3	43	99	J. 6	Ś	7	
REENWIC	03	9	23	•	77	61	4	œ	, passe	
REENWIC	03	97	26	9	48	99	S	0	ı wi	
GREENWICH	.03	1971	54	58.4	53	64	4	55	2	
REENWIC	03	97	9	ę,	51	63	Ŝ	-	5	
REENWIC	03	26	29	4	46	57	 	9	, M	
REENWIC	03	16	59	2,	47	58	e C	Ś	M	
REENWIC	03	<b></b>	65	0	45	55	S	3	2	
REENWIC	03	16	54	Ŋ	50	63	S	8	Ŋ	
REENWIC	03	6	59	<i>ي</i>	54	65	4	4	5	
REENWI	03	16	43%	ထိ	50	19	• •	3	10	
استاسا	04	97		2		64	_ e _	S	4	
EENMIC	04	16		ô		46	1.7	3	m	
<b>EENWIC</b>	40	26		e 		43		ず	2	
GREENWICH	40	1976	57	40.3	35	46	1.07	55	4	
EENWIC	40	16		2		47	ø	$\infty$	pard	
EENWIC	04	97		9		41	•	~	H	
GREENWICH	07	9	*6	32.8			1.6	S		
<b>EENWIC</b>	07	1969		•	32	48	1.6	30	prod	
EENMIC	10	4		6				2	4	
EENWIC	10	6		45.6				Ø	2	
EENWIC	0.7	-		ထု			8	S	5	
GREEN₩ICH	10	1973	99	0		41	1.6	0		
EENWIC		97		Š			0	9	m	
REENWIC		97	**	ω e			•			29
REENWIC		16		* *				S		
EENMIC		-		ô			0	-	16	7
REENWIC		97		2.			9	2		prod
REENWIC		6		4.			•	0		<b>~</b>
GREENWICH	08	6	59	61.5	56	68	1.5	512		
REENWIC		~		ς. •			0	9	80	
FENEIC		16		<del>-</del>			0	4	_	

TE YEAR SAMPLES GEOM MEAN LOWER LIMITS TO GEOM DEV 150 UG/M3 260 UG/M3 261 UG/M3 262 UG/M3 263 UG/M3 263 UG/M3 263 UG/M3 264 U	CONNECTICUT DEPARTMENT POLLUTANTPARTICULATES	RTMEN	4T OF	ENVIRONMENTAL	TABLE 6 PROTECT	(continued) ION	Jed) PAGE	7	AIR COMPLIANCE DISTRIBUTION-	MONI TORING LOGNORMAL
1978         57         51.3         45         59         1.723         8           1974         60         63.0         57         69         1.501         7           1975         28         58.5         52         66         1.363         7           1968         21x         61.2         66         1.653         29         4           1968         25         102.5         66         84         1.653         67         7           1970         25         102.5         86         122         1.653         67         7           1971         53         87.4         77         79         1.653         67         7           1972         16.6         80         1.653         10         67         1         7           1972         16.6         86         1.2         1.653         1         7         1         7           1973         56         44         1.2         1.652         1         1         5         1         1         1         1         1         1         1         1         1         1         1         1         1         1	SITE		ΕA	S	Σ	5-PCT OWER	<b>Б</b> Ш	TD GEOM	PREDICTE DAYS OVE 150 UG/M	REDICTE AYS OVE 60 UG/M
1974         60         63.0         57         69         1.561         7           1975         28 ÷         58.5         52         66         1.363         7           1968         21 ÷         61.2         46         80         1.860         29           1969         21 ÷         61.2         46         80         1.860         29           1970         25         102.5         62         84         1.460         10           1971         53         16.2         1.2         1.638         50           1971         56         46.2         40         53         1.716         50           1972         16.3         31         39         1.674         1         63           1974         61         34.5         31         39         1.674         1         1         1         1         1         1         1         1         67         1         63         1         1         67         1         63         1         1         1         1         1         1         4         1         4         1         4         1         4         1         4	õ		97	57	<b>9</b> 			•72	m	
1967         16*         36.4         28         47         1.631         1           1968         21*         61.2         46         80         1.860         29           1970         25         172.5         62         84         1.460         10           1971         55         102.5         86         122         1.638         50           1971         55         34.8         31         39         1.655         67           1972         55         34.8         31         39         1.652         1           1974         61         34.5         31         39         1.652         1           1975         55         34.8         31         39         1.652         1           1975         44.4         40         55         1.712         3         1           1976         65         44.8         32         47         1.653         1         1           1976         65         44.0         33         34         44         1.465         3         1         1         44         1.465         1         1         44         1.465         1.465			97	$\odot \infty$	8 8		99	50 36		
1968         21*         61.2         46         80         1.860         29           1969         25         12.5         62         84         1.460         10           1970         25         102.5         62         84         1.460         10           1971         53         102.5         1.555         67           1972         56         46.2         40         53         1.716         50           1973         55         34.8         31         39         1.652         1           1974         61         34.5         31         39         1.652         1           1974         61         34.5         32         47         1.635         1           1975         25.8         38.8         34         44         1.635         1           1976         44.0         49         1.562         3           1977         58         44.0         1.44         1.462         3           1976         61         40.7         34         44         1.462         3           1977         61         42.7         34         44         1.462         3 <td>0</td> <td></td> <td>96</td> <td>16*</td> <td>9</td> <td>28</td> <td>14</td> <td>.63</td> <td><b></b>-</td> <td></td>	0		96	16*	9	28	14	.63	<b></b> -	
1969         25         72.5         62         84         1.9460         10           1970         25         102.5         62         184         1.9460         10           1971         53         87.4         77         99         1.638         67           1973         56         46.2         40         53         1.716         50           1974         61         34.5         31         39         1.652         1           1975         25.8         34.5         31         39         1.6574         1           1975         25.8         38.5         32         47         1.635         1           1976         6.         44.8         28         72         1.635         1           1977         14.4         40.3         30         55         1.722         3           1978         61         44.7         44         1.6495         1           1978         61         44.7         44         1.6495         1           1978         61         44.7         44         1.6495         1           1978         61         44.7         1.649 <t< td=""><td><math>\circ</math></td><td></td><td>96</td><td>21*</td><td>•</td><td>46</td><td>80</td><td>.86</td><td>58</td><td>4</td></t<>	$\circ$		96	21*	•	46	80	.86	58	4
1971     53     40.55     67       1971     53     46.2     40     53     67       1972     56     46.2     40     53     1.652     67       1973     55     34.8     31     39     1.652     1       1974     61     34.8     31     39     1.652     1       1975     25*     38.5     32     47     1.635     1       1966     6*     44.8     28     72     1.584     2       1975     35*     38.8     34     44     1.495     3       1976     58     34.9     47     1.562     1       1977     61     40.7     37     44     1.462     1       1978     61     40.7     37     44     1.662     1       1978     61     40.7     37     44     1.662     1       1978     61     40.7     37     44     1.662     1       1978     61     40.7     37     44     1.662     1       1974     44.8     32.9     29     38     1.642     1       1975     59     33.3     31     40     1.646     1	J (		96	25	720	79	œ	•46	0	•
1972     55     46.4     77     99     1.638     50       1972     56     46.2     40     53     1.616     5       1973     55     34.8     31     39     1.674     1       1974     61     34.5     31     39     1.674     1       1975     25.8     38.5     32     47     1.635     1       1966     6.     44.8     28     72     1.584     2       1975     38.8     34     44     1.495     3       1976     58     34.8     34     44     1.495       1977     61     40.7     37     47     1.465       1978     61     40.7     37     44     1.465       1978     61     40.7     37     44     1.465       1975     60     38.7     35     43     1.646       1976     58     33.3     30     37     1.553       1977     59     34.5     31     40     1.649       1977     59     35.4     30     37     1.554       1978     52     40     1.554       1973     11.554     40     1.554	<i>)</i> (		, L	C 7	. 7 n	98	2	e SN	19	7
1973     55     34.8     31     39     1.6452       1974     61     34.8     31     39     1.6454       1975     25*     38.5     32     47     1.6552       1966     6*     44.8     28     72     1.584       1975     35*     38.8     34     44     1.495       1976     58     44.7     41     49     1.506       1977     61     42.7     39     47     1.550       1978     61     42.7     37     44     1.550       1977     61     40.7     37     44     1.550       1978     61     40.7     37     44     1.550       1978     61     40.7     37     44     1.555       1978     61     40.7     37     44     1.562       1978     61     40.7     37     44     1.555       1975     59     38.7     35     43     1.555       1976     59     33.3     30     37     1.554       1977     59     38.7     40     1.554       1978     51     50.7     46     56     1.329       1974     51	0		76	ን የ	e (	7.7	66	•63	50	Ŋ
1974     61     34.55     31     39     1.6074       1975     25*     38.5     32     47     1.635       1966     6*     44.8     28     72     1.584       1967     14*     40.3     30     55     1.722       1975     35*     38.8     34     44     1.495       1976     58     44.7     41     49     1.506       1977     61     42.7     37     44     1.462       1978     61     40.7     37     44     1.642       1978     61     40.7     37     44     1.556       1978     61     40.7     37     44     1.556       1975     59     38.7     35     43     1.564       1976     58     35.4     31     40     1.554       1977     59     34.5     31     38     1.564       1978     52     35.4     31     38     1.554       1978     52     35.4     45     65     1.554       1974     51     56.5     1.552       1975     60     53.7     49     56     1.552       1975     60     53.7 <t< td=""><td></td><td></td><td>97</td><td>יירט ירט</td><td>9 1</td><td>ָר א ה</td><td>0 0</td><td>- 1 U</td><td>Λ,</td><td></td></t<>			97	יירט ירט	9 1	ָר א ה	0 0	- 1 U	Λ,	
1975       25\$       38.5       32       47       1.6535         1966       6\$       44.8       28       72       1.6535         1967       14\$       40.3       30       55       11.552         1975       35\$       38.8       34       44       11.495         1976       58       44.7       41       49       11.552         1977       61       42.7       39       47       11.542         1978       61       40.7       37       44       11.542         1978       61       40.7       37       44       11.542         1978       60       38.7       37       44       11.552         1974       44.8       32.9       29       37       11.552         1975       59       33.3       30       37       11.542         1978       59       34.5       31       40       11.641         1978       52       35.4       45       60       11.548         1978       59       34.5       31       40       11.548         1974       51       56.2       12.512         1975       6	0		16	61	9 9	3 1	, c	0 0 V		
4 1966       6*       44.8       28       72       1.584         4 1967       14*       40.3       30       55       1.584         3 1975       35*       38.8       34       44       1.495         3 1975       58       44.7       41       49       1.506         3 1977       61       42.7       39       47       1.562         3 1978       61       40.7       37       44       1.462         2 1977       60       38.7       35       43       1.649         2 1975       59       33.3       30       37       1.649         2 1976       58       35.4       31       40       1.649         2 1977       59       34.5       31       40       1.649         2 1978       52       35.4       31       40       1.553         2 1978       64.5       68.0       63       73       1.354         2 1974       59       35.4       45       65       1.352         2 1974       50.7       45       56       1.352         2 1975       59       59       1.552         3 10.35       45 </td <td><math>\sim</math></td> <td></td> <td>16</td> <td>25*</td> <td>ထ</td> <td>32</td> <td>14</td> <td>• 63</td> <td>nd pund</td> <td></td>	$\sim$		16	25*	ထ	32	14	• 63	nd pund	
4       1967       14*       40.3       30       55       15.722         3       1975       35*       38.8       34       44       1.495         3       1976       58       44.7       41       49       1.506         3       1977       61       42.7       39       47       1.506         3       1977       61       40.7       37       1.562         2       1978       60       38.7       35       43       1.555         2       1975       60       38.7       35       43       1.555         2       1974       44*       32.9       29       38       1.649         2       1975       59       33.3       30       37       1.523         2       1976       59       34.5       31       40       1.641         2       1977       59       34.5       31       40       1.548         2       1978       52       35.4       32       40       1.554         2       1978       54.2       45       65       1.554         2       1974       50.7       46       56		4	96	*9	4.			r, X	C	
3       1975       35*       38.8       34       44       10.495         3       1976       58       44.7       41       49       10.506         3       1977       61       42.7       39       47       10.542         3       1978       61       40.7       37       10.462         3       1975       60       38.7       35       43       10.555         2       1974       44*       32.9       29       38       10.649         2       1975       59       33.3       30       37       10.523         2       1976       58       35.4       31       40       10.641         2       1977       59       34.5       31       38       10.548         2       1977       59       34.5       32       40       10.548         2       1977       59       35.4       32       45       10.554         2       1978       64.5       68.0       63       73       10.329         2       1974       51       50.7       46       56       10.466         2       1974       59 <t< td=""><td>0</td><td>4</td><td>96</td><td>14%</td><td>°</td><td></td><td></td><td>.72</td><td>3 W</td><td></td></t<>	0	4	96	14%	°			.72	3 W	
3 1976       58       44.7       41       49       1.506         3 1977       61       42.7       39       47       1.556         3 1978       61       40.7       37       44       1.556         2 1975       60       38.7       35       43       1.555         2 1976       59       33.3       30       37       1.649         2 1976       58       35.4       31       40       1.649         2 1977       59       34.5       31       40       1.641         2 1977       59       34.5       31       40       1.641         2 1977       59       35.4       31       40       1.554         2 1978       52       35.4       32       40       1.554         2 1978       54.2       45       65       1.329         2 1974       51       50.7       46       56       1.556         2 1975       51       50.7       46       56       1.556         2 1974       51       50.7       49       59       1.466	$\sim$	M	76	35*	ထိ	34	77	4		
3       1977       61       42.7       39       47       1.5462         3       1978       61       40.7       37       44       1.4662         3       1978       60       38.7       35       43       1.555         2       1974       44*       32.9       29       38       1.649         2       1975       59       33.3       30       37       1.649         2       1976       58       35.4       31       40       1.641         2       1977       59       34.5       31       38       1.641         2       1978       52       35.4       31       38       1.523         2       1978       52       35.4       32       40       1.554         2       1977       68.0       63       73       1.374         2       1973       11*       56.2       45       56       1.512         2       1974       59       1.466       59       1.466	' '	~	16	58	4.	41	. 64	. <u> </u>		
3     1978     61     40.7     37     44     1.462       3     1975     60     38.7     35     43     1.6555       2     1974     44*     32.9     29     38     1.649       2     1975     59     33.3     30     37     1.649       2     1975     58     35.4     31     40     1.641       2     1977     59     34.5     31     38     1.548       2     1977     59     35.4     32     40     1.5548       2     1978     52     35.4     32     40     1.374       2     1978     64*     68.0     63     73     1.374       2     1973     11*     54.2     45     56     1.329       2     1974     51     50.7     46     56     1.512       2     1975     60     53.7     49     59     1.466	N.	3	97	61	2 0	39	74	50.4	pres	
3       1975       60       38.7       35       43       1.555         2       1974       44*       32.9       29       38       1.649         2       1975       59       33.3       30       37       1.523         2       1975       58       35.4       31       40       1.641         2       1977       59       34.5       31       38       1.548         2       1977       52       35.4       32       40       1.5548         2       1978       52       35.4       32       40       1.3548         2       1978       68.0       63       73       1.3554         2       1973       11*       54.2       45       65       1.329         2       1974       51       50.7       46       56       1.512         2       1975       60       53.7       49       59       1.466	$\sim$	m	97	61	o	37	44	.46	4	
2     1974     44*     32.9     29     38     1.649       2     1975     59     33.3     30     37     1.523       2     1976     58     35.4     31     40     1.641       2     1977     59     34.5     31     38     1.641       2     1977     59     34.5     32     40     1.6548       2     1978     64*     68.0     63     73     1.374       2     1973     11*     54.2     45     65     1.329       2     1974     51     50.7     46     56     1.512       2     1975     60     53.7     49     59     1.466		3	16	09	ထိ			.55		
2     1975     59     33.3     30     37     1.523       2     1976     58     35.4     31     40     1.641       2     1977     59     34.5     31     38     1.548       2     1977     52     35.4     32     40     1.554       2     1978     68.0     63     73     1.374       2     1973     11*     54.2     45     65     1.329       2     1974     51     50.7     46     56     1.512       2     1975     60     53.7     49     59     1.466		2	16	***	2	29	38	49		
2     1976     58     35.4     31     40     1.641       2     1977     59     34.5     31     38     1.548       2     1978     52     35.4     32     40     1.554       2     1978     64.*     68.0     63     73     1.374       2     1973     11.*     54.2     45     65     1.329       2     1974     51     50.7     46     56     1.512       2     1975     60     53.7     49     59     1.466		~	97		3	30	37	. 52		
2     1977     59     34.5     31     38     1.548       2     1978     52     35.4     32     40     1.554       2     1967     64.0     68.0     63     73     1.374       2     1973     11.0     54.2     45     65     1.329       2     1974     51     50.7     46     56     1.512       2     1975     60     53.7     49     59     1.466	C)	7	16		5.	31	40	400	property.	
2     1978     52     35.4     32     40     1.554       2     1967     64.8     68.0     63     73     11.374       2     1973     11.8     54.2     45     65     1.329       2     1974     51     50.7     46     56     1.512       2     1975     60     53.7     49     59     1.466	u	2	16		40	31	38	,54	•	
2 1967 64* 68.0 63 73 1.374 2 1973 11* 54.2 45 65 1.329 2 1974 51 50.7 46 56 1.512 2 1975 60 53.7 49 59 1.466	0	2	76		S B	32	40	. C. C.		
2 1973 11% 54°2 45 65 1°329 2 1974 51 50°7 46 56 1°512 2 1975 60 53°7 49 59 1°466		2	96	94%	œ			(.,	r	
2 1974 51 50.7 46 56 1.512 2 1975 60 53.7 49 59 1.466		2 1	76	**	· 4			ם ה ה	7	
2 1975 60 53.7 49 59 1.466		2	16	51	. 0			٠ ١ ١	C	
	$\circ$	2	16	09	6			646	J	

CONNECTICUT	DEPARTMENT	70	ENVIRONMENTAL		TABLE 6 (continued) PROTECTION	red)	8 AIR	R COMPLIANCE	MONITORING
POLLUTANTPA	ARTICULAT	ATES						DISTRIBUTION	LOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES	GEOM MEAN	95-PCT- LOWER	-LIMITS UPPER	STD GEDM DEV	PREDICTED DAYS OVER 150 UG/M3	PREDICTED DAYS OVER 260 UG/M3
HARTFORD HARTFORD HARTFORD	02 02 02	1976 1977 1978	59 59 44*	48.6 50.6 50.2	44 45 43	ሌ የ ት የሪ የ	1.620	4 H 8	
HARTFORD HARTFORD HARTFORD		96 96 96	44* 133* 177	ω	115 95 101		* 64 * 53 * 63		
HAKIFOKO HARTFORO HARTFORO		سما سما سما سم	150 169 139 33*	04° 86° 74° 80°	99 83 70 71	1010	1.639 1.517 1.602 1.474	88 3.5 2.0	гг К СУ тч
HARTFORD HARTFORD HARTFORD HARTFORD HARTFORD	03 03 03	1974 1975 1976 1977 1977	55 60 58 105	62°4 68°5 73°5 66°2 64°6	56 63 67 60	70 75 81 71 69	24450	10 13 13 13	
HARTFORD HARTFORD HARTFORD HARTFORD HARTFORD HARTFORD HARTFORD	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1968 1969 1972 1972 1974 1975	18% 20% 13% 40 47 58 13%	80.6 119.2 158.2 47.8 49.6 48.4 47.1	60 92 104 40 42 43 44	108 155 241 57 57 56 56	1.810 1.770 2.029 1.757 1.635 1.653	126 197 8 4 4 10	8 8 8 8
HARTFORD HARTFORD HARTFORD HARTFORD HARTFORD HARTFORD	05 05 05 05 05 05	1968 1969 1970 1971 1974 1975	16 % 24 13 % 18 % 48 % 58	60.7 53.9 101.8 117.6 43.1 50.2	44 8 8 6 4 4 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	76 69 150 155 49 56	1.550 1.820 1.917 1.761 1.623 1.547	7 16 100 126 2 2	2 29 29
HARTFORD	10	1966	210	100.1	96	104	1.597	19	80

CONNECTICUT	DEPART	PARTMENT OF	ENVIRONMENTAL	TABLE 6 PROTECT	(continued) ION	d) PAGE	6	AIR	COMPLIANCE	MONITORING	
PCLLUTANTP	ARTICULAT	LATES						O	ISTRIBUTION-	LOGNORMAL	
TOWN NAME	SITE	YEAR	SAMPLES	GEOM MEAN	95-PCT-L LOWER	LIMITS UPPER	STD GE	OM DEV	PREDICTED DAYS OVER 150 UG/M3	PREDICTED DAYS OVER 260 UG/M3	
HARTFORD HARTFORD	10	1967	329 96*	90.6	89 90	92 104	<b>-</b>	.658 .510	50 50	7 6	
HARTFORD	11	1961	32*	11301	16	131	<del>,</del>	546	100	10	
RIFOR	2	197		7.	40	57	H	S			
HARTFORD HARTFORD	123 123	1977	60 61	65°7 67°1	59 61	73	-	.542 .519	10		
RTFOR		S		110.4	90	135	pod		Ç	<b>V</b>	
OR	0 0	195		80	99	Ò	استو ا	63	3		
スーナした	⊃ (	195		49	68	9	_		20	-	
RTFOR	00	196		0 0	83 62	123 83		.510 .410	19	'n	
10 R	0	196		2	93	3	<b>-</b>	9		13	
RIFOR	0 (	196		98°	86	-	pour	40			
オープンスワイロンの	0 0	196		ζ,	86	130	-	9		16	
ストコロスター	) C	106		• + -	7.1	$\circ$	prof ;	<b>(L)</b>		2	
RTFOR	0	196		9 4	6 4 2 - 1	2 C C		ひち	3.5	<b>~</b> r	
RIFOR	0	196		o	50	72	नं इन्त्यं	, (O		magn.	
RTFOR	0	196		2.	52	75	· <b></b>	57	10		
ARTFOR	0	197		@ 	52	14	_	56			
HAKIFUKU HARTFORD	A 01	1971	23	63°8 60°5	55 51	74	<b>-</b>	*430 *600	۳ O		
ш		197		00			-	0		, .	
KENT KENT	01	1974	56 38*	31.4	27	37.	d pool pool	. 859 . 628	- 2	<b>∞</b> d	
T	01	197	26*	o	99	66	press.		42	3	
STE	01	197	15*	0	39	57	است	40		<b></b>	
STE	. 01	197	Q	~	40	23	1 par4	<u>-  </u>	7		
MANCHESTER	10	1974	38%	45.2	39	52	part (	.590	2		
 	70	<del>-</del>	90	<b>*</b>	5	50.		Ś	m		

The Test of the Te	CONNECTICUT DEPARTMENT	MENT OF	ENVIRONMENTA	TABLE 6	(continued) ION	ed) PAGE	10 AIR	R COMPLIANCE	MONI TOR ING
YEAR         SAMPLES         GEOM MEAN         LOWER         OPPER         STD GEOM DEV         PREDICTED	_	ш						ISTR	-LOGNORM
1976         55         39.8         35         45         1.604         1           1977         60         43.5         39         46         1.567         1           1978         56         41.8         39         46         1.567         1           1979         14.8         37.9         31         47         1.460         2           1971         22         44.2         40         53         1.593         1           1971         24         46.2         40         53         1.609         1           1972         26.6         43.1         32         58         2.101         16         3           1973         18%         23.2         19         28         1.609         1         4           1974         47         36.5         31         41         1.646         2         1.646         2           1974         47         36.5         31         41         1.648         2         1.0         1         4         1.646         2         1.0         1         1.646         2         1.0         1.646         2         1.0         1.648         1.648	ш	YEA	AMPLES	EOM ME	5-PCT OWER	LIMIT UPPE	TD GEOM DE	REDICTE AYS OVE 50 UG/M	REDICTE AYS OVE 60 UG/M
1978         56         43.5         39         48         1.567         1           1969         14#         37.9         31         47         1.460         2           1970         22         44.8         37.9         31         47         1.460           1971         24.8         37.9         31         47         1.493         2           1972         26.8         46.2         40.5         31         40.497         1.609           1973         18*         23.2         33         41         1.628         1           1974         47         36.5         33         41         1.6497         2           1975         14*         40.5         34.3         41         1.6497         2           1975         14*         40.5         34.3         41         1.6497         2           1976         14*         40.5         31         42         1.6497         2           1976         14*         40.5         31         42         1.6497         2           1977         24         40.5         31         45         1.6497         2           1978	,4	76		6.0			9	,d	
1969   14*   37.9   31   47   1.460   1.541   1970   2.2   44.8   37.9   31   47   1.460   1.541   1.541   1.541   1.542   1.543   1.543   1.543   1.543   1.543   1.543   1.543   1.543   1.543   1.543   1.543   1.543   1.543   1.543   1.543   1.543   1.543   1.543   1.543   1.545   1		76		ر) الــ ا			N I	red	
1969         14**         37.9         31         47         1.460         2         1.593         2         1.593         2         1.593         2         1.543         10 <td>ł</td> <td>•</td> <td></td> <td>9</td> <td></td> <td></td> <td>°54</td> <td></td> <td></td>	ł	•		9			°54		
1970         32, 44,48         37         55         1,593         2           1971         26,**         43,*1         37         58         1,543         1           1972         26,**         43,*1         32         58         1,543         1           1973         18,**         23,*2         19         28         1,497         16           1974         47         34,*3         30         39         1,609         1           1974         47         34,*3         30         39         1,609         1           1975         10,**         40,**         30         39         1,609         1           1975         10,**         40,**         30         33         41         1,609         2           1971         53         40,**         36         45         1,646         2         2           1972         54         56         80         1,484         13         45         57         1,607         4           1974         56         50,**         45         57         1,607         4         50         16         1,607         4         50         1,607		9,6	14%	7			46		
1972     26**     46*2     40     53     1.543     1       1973     18**     23*2     19     28     1.543     1       1974     47     34*3     32     58     1.5497     1       1975     60     36*5     33     41     1.628     1       1975     16**     40*5     31     54     1.646     2       1976     14**     40*5     31     54     1.648     13       1971     53     40*4     36     45     1.648     13       1972     54     72*5     66     80     1.484     13       1973     36**     58.2     48     16     7     1.648       1974     55     50*3     45     67     2.013     24       1975     35**     53*2     42     67     2.013     24       1975     18**     79*8     59     108     1.850     58       1970     14**     66*1     50     87     1.650     58       1971     58     95**     46     59     1.650     42       1972     60     86**     45     76     1.650     42       1974 <td></td> <td>76</td> <td>22</td> <td>4.</td> <td></td> <td></td> <td>59</td> <td>2</td> <td></td>		76	22	4.			59	2	
1973         18%         23.2         19         58         2.101         16           1973         18%         23.2         19         28         1.6497         1           1 1975         60         36.5         33         41         1.646         2           1 1975         14%         40.6         31         54         1.646         2           1 1971         53         40.4         36         45         1.646         2           1 1972         54         72.5         66         80         1.484         13           1 1972         54         72.5         66         80         1.484         13           1 1973         36%         50.3         42         67         1.607         4           1 1974         55         50.3         42         67         1.607         4           2 1969         18         79.8         59         108         1.850         58           2 1970         14         5         79         108         1.650         42           2 1971         58         50.4         45         57         1.650         42           2 1973	4 -	- 6	0. c	o O			• 54	~	
1 1974     47     34.3     19     28     1.497       1 1974     47     34.3     30     39     1.609       1 1975     60     36.5     31     41     1.628     1       1 1976     14.5     40.4     36     45     1.635     2       1 1972     54     72.5     66     80     1.484     13       1 1972     54     72.5     66     80     1.484     13       1 1972     56     66.1     36     45     57     1.607     46       1 1973     36.5     50.3     45     57     1.607     4       1 1974     55     66.1     50     87     1.607     4       2 1974     55     66.1     50     87     1.607     4       2 1975     14.5     57     1.607     42     56       2 1970     14.5     95.4     86     10.6     1.6540     58       2 1971     18.5     56.0     86.2     59     10.6     1.6540     58       2 1974     59     50.4     46     59     1.650     3       2 1975     50     66.2     58     1.650     3       2 1976	٦ -	, C	*97	٠ ا			.10		m
1974	7 7	, t	% 80 !	3			640		
1975   100	7 =	70	747	4.			•60		
1 1971     53     40.4     36     45     1.646     2       1 1972     54     72.5     66     80     1.484     13       1 1972     36*     72.5     66     80     1.484     13       1 1973     36*     72.5     66     80     1.484     13       1 1974     55     50.3     45     57     1.607     4       2 1974     55     50.3     45     57     1.607     4       2 1974     53.2     42     67     2.013     24       2 1976     18*     79.8     59     108     1.850     18       2 1970     14*     66.1     50     87     1.650     58       2 1971     18*     79.8     59     108     1.850     58       2 1972     1973     56     66.2     58     76     1.620     42       2 1973     56     66.2     58     76     1.650     59       2 1974     59     50.4     45     59     1.650     3       2 1975     50     82.3     76     1.650     3       2 1976     51     52.0     46     59     1.650     3       3	-	- 6	** <b>7</b> !	هٔ د			•62	-4	
11     1971     53     40.44     36     45     1.535       11     1972     54     72.5     66     80     1.484     13       11     1973     36*     58.2     48     71     1.683     20       11     1974     55     50.3     45     57     1.607     4       11     1974     55     50.3     45     57     1.607     4       11     1975     35.     53.2     42     67     2.613     24       12     1975     18*     79.8     59     108     1.850     58       12     1970     14*     97.6     79     108     1.850     58       1971     58     95.4     86     106     1.540     58       2     1972     60     82.3     73     92     1.650     42       2     1973     56     66.2     58     76     1.655     29       2     1974     59     1.655     59     1.655     29       2     1975     50.4     45     58     1.656     45       2     1978     60     50.7     47     58     1.650     34	•	•	; ;	٥			•64	2	
11     1972     54     72.5     66     80     1.484     13       11     1973     35*     58.2     48     71     1.839     20       11     1974     55     50.3     45     57     1.607     4       11     1975     35*     53.2     42     67     2.013     24       12     1968     14*     66.1     50     87     1.607     24       12     1969     18*     79.8     59     108     1.850     58       12     1970     14*     97.6     79     108     1.850     58       12     1971     58     95.4     86     106     1.545     50       1972     60     82.3     73     92     1.620     42       2     1974     59     106     1.550     29       2     1974     59     1.650     3       2     1975     51     46     59     1.650     3       2     1976     52.5     47     58     1.550     3       2     1977     60     52.5     47     58     1.550     3       3     1969     19.2     60     <	7	16	53	Ô	36		53		•
11     1973     36**     58.2     48     71     1.839     20       11     1974     55     50.3     45     57     1.607     4       11     1975     35**     53.2     42     67     2.013     24       12     1968     14**     66.1     50     87     1.630     16       12     1969     18**     79.8     59     108     1.850     58       1970     14**     97.6     79     108     1.850     58       1971     58     95.4     86     106     1.650     58       2     1971     58     76     1.650     42       2     1972     60     82.3     73     92     1.655     59       2     1974     59     1.655     59     1.655     59       2     1975     51     52.0     46     59     1.655     59       2     1976     51     54     58     1.550     3       2     1978     60     74     58     1.550     3       3     1969     19*     69.4     51     10       3     1970     20*     85.8     67	Ξ:	16	4	2 •	99		48		
1 1974       55       50.3       45       57       1.607       4         1 1975       35%       53.2       42       67       2.013       24         2 1968       14%       66.1       50       87       1.630       16         2 1969       18%       79.8       59       108       1.850       58         2 1970       14%       97.6       79       121       1.454       50         2 1971       58       95.4       86       106       1.540       58       1         2 1972       60       82.3       73       92       1.620       42         2 1973       56       66.2       58       76       1.650       58         2 1974       59       50.4       45       57       1.655       59         2 1975       51       52.0       46       59       1.580       4         2 1976       51       52.5       47       58       1.550       3         3 1969       19%       60       1.550       3       4       50         3 1970       20%       85.8       67       110       1.721       58	7 :	کر اب	91	ထိ	48		*83		~
2     1968     14%     66.1     50     87     1.630     16       2     1968     14%     66.1     50     87     1.630     16       2     1969     18%     79.8     59     108     1.850     58       2     1970     14%     97.6     79     121     1.454     50       2     1971     58     95.4     86     106     1.540     58       2     1972     60     82.3     73     92     1.620     42       2     1973     56     66.2     58     76     1.620     42       2     1974     59     76     1.650     59       2     1974     59     1.655     5       2     1976     51     51.8     46     59     1.560       2     1976     52.5     47     58     1.550     3       2     1978     60     52.5     47     58     1.550     3       3     1968     12.*     45.0     34     60     1.570     1       3     1970     20.*     85.8     67     110     1.721     58       3     1971     54     70	7 6	ر ا ا	S L	o ,	45		• 60		
1968     14*     66.1     50     87     1.630     16       2 1969     18*     79.8     59     108     1.850     58       2 1970     14*     97.6     79     121     1.654     50       2 1971     58     95.4     86     106     1.554     58       2 1972     60     82.3     73     92     1.650     42       2 1973     56     66.2     58     76     1.762     29       2 1974     59     50.4     45     57     1.550     29       2 1975     51     51.8     46     58     1.550     3       2 1977     60     52.5     47     58     1.550     3       2 1978     60     52.5     47     58     1.550     3       3 1969     19**     69.4     51     95     1.570     1       3 1970     20*     85.8     67     110     1.721     58       3 1971     54     70.2     77     10	4	<u>_</u>	n .	9	45		•01		\$
12     1969     18**     79.8     59     108     1.850     58       2     1970     14**     97.6     79     121     1.4540     58       2     1971     58     95.4     86     106     1.540     58       2     1972     60     82.3     73     92     1.650     42       2     1973     56     56.2     58     76     1.650     42       2     1974     59     50.4     45     57     1.655     5       2     1975     51     51.8     46     59     1.550     3       2     1977     60     52.5     47     58     1.550     3       2     1977     60     52.5     47     58     1.550     3       3     1968     12*     45.0     34     60     1.570     1       3     1969     19*     69.4     51     95     1.950     42       3     1970     20*     85.8     67     110     1.721     58       3     1971     54     70.2     77.7     77.7     58	)2	•	4	Ó	50		7	es.	,
2     1970     14*     97.6     79     121     1.454     50       2     1971     58     95.4     86     106     1.540     58       2     1972     60     82.3     73     92     1.620     42       2     1973     56     66.2     58     76     1.762     29       2     1974     59     1.655     5       2     1975     51     46     59     1.580       2     1976     51     46     58     1.580       2     1977     60     52.5     47     58     1.550     3       2     1978     60     60.7     54     68     1.550     3       3     1968     12*     45.0     34     60     1.570     1       3     1969     19*     69.4     51     95     1.950     42       3     1970     20*     85.8     67     110     1.721     58       3     1971     54     70     70     70     70     70	20	96	œ	0	59		י ער	0 1	
2     1971     58     95.4     86     106     1.540     58       2     1972     60     82.3     73     92     1.620     42       2     1973     56     66.2     58     76     1.762     29       2     1974     59     50.4     45     57     1.655     5       2     1975     51.8     46     59     1.580     4       2     1976     51.8     46     58     1.560     3       2     1977     60     52.5     47     58     1.550     3       3     1968     12*     45.0     34     60     1.570     1       3     1969     19*     69.4     51     95     1.950     42       3     1970     20*     85.8     67     110     1.721     58       3     1971     54     70.2	200	76	4	6	4	2	7 (7)	0 0	
1972     60     82.3     73     92     1.620     42       2 1973     56     66.2     58     76     1.762     29       2 1974     59     50.4     45     57     1.655     29       2 1975     51     52.0     46     59     1.580     4       2 1976     51     51.8     46     58     1.550     3       2 1977     60     52.5     47     58     1.550     3       2 1978     60     60.7     54     68     1.550     10       3 1968     12*     45.0     34     60     1.570     1       3 1969     19*     69.4     51     95     1.950     42       3 1970     20*     85.8     67     110     1.721     58       3 1971     54     70.2     77     77     77     77	7 5	) )   	ک ک	e M	86	0	5	₩ ₩ ₩	14
2     1974     56     66.2     58     76     1.0762     29       2     1974     59     655     5       2     1975     51     52.0     46     59     1.0580     4       2     1976     51     51.8     46     58     1.0560     3       2     1977     60     52.5     47     58     1.050     3       2     1978     60     10.570     1       3     1968     12.8     45.0     34     60     1.050     42       3     1970     20.8     85.8     67     110     1.721     58       3     1971     54     70.2     7.7     7.7     7.7     7.7     7.7     7.7	7 .	7 (	09	2.	73		62	42	. لاـ
2     1974     59     50.4     45     57     1.655     5       2     1975     51     52.0     46     59     1.580     4       2     1976     51     51.8     46     58     1.560     3       2     1977     60     52.5     47     58     1.550     3       2     1978     60.7     54     68     1.596     10       3     1969     19%     69.4     51     95     1.950     42       3     1970     20%     85.8     67     110     1.721     58       3     1971     54     70.2     77     77     77     77	7 (	) (	26	و م	58		76	29	ו (יי
2     1975     52.0     46     59     1.580     4       2     1976     51     51.8     46     58     1.560     3       2     1977     60     52.5     47     58     1.550     3       2     1978     60.7     54     68     1.550     10       3     1968     12*     45.0     34     60     1.570     1       3     1969     19*     69.4     51     95     1.950     42       3     1970     20*     85.8     67     110     1.721     58       3     1971     54     70.2     77     77     77     77     77	7.0	) 	59	0	45		65	) 	•
2     1976     51.8     46     58     1.550     3       2     1977     60     52.5     47     58     1.550     3       2     1978     60.7     54     68     1.550     3       3     1968     12*     45.0     34     60     1.570     1       3     1969     19*     69.4     51     95     1.950     42       3     1970     20*     85.8     67     110     1.721     58       3     1971     54     70.2     77     77     77     77	4 (	- I	71	o N	46		رج 8	4	
2     1977     60     52.5     47     58     1.550     3       2     1978     60     60.7     54     68     1.596     10       3     1968     12*     45.0     34     60     1.570     1       3     1969     19*     69.4     51     95     1.950     42       3     1970     20*     85.8     67     110     1.721     58       3     1971     54     70.2     77     77     77     77	N C	76	27	e —	46		56	· ‹‹	
2     1978     60     60.7     54     68     1.596     10       3     1968     12.*     45.0     34     60     1.570     1       3     1969     19.*     69.4     51     95     1.950     42       3     1970     20.*     85.8     67     110     1.721     58       3     1971     54     70.2     77     67	7	ا بر ا ب	09	را ف	47		Š	) (f	
3 1968 12* 45.0 34 60 1.570 1 3 1969 19* 69.4 51 95 1.950 42 3 1970 20* 85.8 67 110 1.721 58 3 1971 54 79.2 67	V	~ 5	9	0	54		S		-
3 1969 19** 69*4 51 95 1.950 42 3 1970 20** 85.8 67 110 1.721 58		96	$\sim$	ر <u>د</u> م		0	P		
3 1970    20		96	0	6		0 0	- C		
3 1971 54 79.2 47 67	03	16	0	, (t <sub>c</sub>		), h	) () 1 (C) 1 (C)		∞
		16		o		٠ c	7 0		Φ

CONNECTICUT DE	PARTM	DEPARTMENT OF	ENVIRONMENTAL	•	PABLECT (Continued	1) PAGE	11 A	IR COMPLIANCE	MONITORING
POLLUTANTPAR	-PARTICULA	ATES						DISTRIBUTION-	LOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES	GEOM MEAN	95-PCT- LOWER	LIMITS UPPER	STD GEOM DEV	PREDICTED DAYS OVER 150 UG/M3	PREDICTED DAYS OVER 260 UG/M3
		7		c			ŭ		F
		- f		, )			000		<b>-4</b> :
ZITATOTIN		7		<b>4</b>			φ α		7
MERIDEN	03	1974				65	° 79		ed
MERIDEN	03	76	28*		43	69		50	2
RID	04	96	14%	رب ه			.72		
S CX	04	1970	<b>*</b>	98.8	59	166	1.880	88	24
MERIDEN	0.5	9	*8	28.		3	16	9	0
MERIDEN	90	96		56.	0	3	•24	0	0
MERIDEN	05	76	m	4	-	4	e rV	~	(4)
MERIDEN	90	97		57.			-11		100
MERIDEN	0.5	16		ထ		<del></del>	.20	-4	\$
MERIDEN	05	16		6		9	77 0	N	
MERIDEN	0.5	1974	57	63.4	54	74	1.871	59	4
MERIDEN	02	16		ထိ			•84		m
MERIDEN	0.5	97		2			.92		5
MERIDEN	05	97		·			•67		javed
MERIDEN	0.5	97		4.			•65	ω	
ERID	90	97		ထိ			• 54		7
ERID	90	97		ထို			.82		ιΛ
MERIDEN	90	1973	51	49.3	45	58	1.903	16	2
ER ID	90	97		9			e 75		
ERID	90	97		6			16.		4
ER IO	90	97		6			•24		13
MERIDEN	10	1968	*01	61.1	47	79	1.430	2	
MIDDLETOWN	01	96	23*	9			.67	m	
MIDDLETOWN	0	96	38*	ę,			ູ້ ນັ້ນ		
MIDDLETOWN	0	96	22	ô			96°	35	2
MIDDLETOWN	01	96	25	9			090	7	
MIDDLEIDWN	0.7	1970	22	38.6	. 59	25	2 • 003	æ	d
MICCLHICKN	70	97	51	υ e			.57		

CONNECTICUT DEPARTMENT	<b>JEPARTN</b>	MENT OF	ENVIRONMENTAL	TABLE 6 AL PROTECT	(continued) ION	d) PAGE	12 AIR	R COMPLIANCE	MONITORING
POLLUTANTPARTICULAT	ARTICUL	.ATES					_		
TOWN NAME	SITE	YEAR	SAMPLES	GEOM MEAN	95-PCT- LOWER	-LIMITS UPPER	STD GEOM DEV	PREDICTED DAYS OVER 150 UG/M3	PREDICTED DAYS OVER 260 UG/M3
MIDDLETOWN MIDDLETOWN MIDDLETOWN	01 01 01	1972 1973 1974	59 59 59	47.3 50.7 34.6	42 44 31	35 35 35 35 35 35 35 35 35 35 35 35 35 3	1.602 1.880 1.679	16	2
MIDDLETOWN MIDDLETOWN	02	1966	25* 38*	46°8 45°4	39 39	56 52	1.584 1.569	2	
7775		96 96 76			0 to 00 to 0	71 82 78 77	4 4 5 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6	24 5 7 4	2
MIDDLETOWN MIDDLETOWN MIDDLETOWN	03	1972 1973 1974 1975	59 59 55 55		444000		1.043 1.638 1.514 1.585	10 10 4 * * * * * * * * * * * * * * * * * * *	
ವನ ಕ		97 97 97		2 2 8	555 54 54	65 57 72	.52 .52 .77	2 8 8 2 4 5	7
MIDDLETOWN	04	1973	52*	51.4	45	63	2.245	35	ю
MILFORD MILFORD MILFORD MILFORD	001000	96 96 97 97		59.4 59.2 59.0 59.0	44 94 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6	81 53 74 60	$\omega$ $\omega$ $\omega$ $\omega$	29	ľ.
MILFORD MILFORD MILFORD MILFORD MILFORD	0000000	1973 1974 1975 1976 1977 1978	0 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	50 20 20 20 20 20 20 20	1.613 1.552 1.537 1.556 1.556	4 LLWL2	
MILFORD MILFORD	02	1968	18* 20	64°7	56	85	1.750	24	N

MONITORING	LOGNORMAL	PREDICTED DAYS OVER 260 UG/M3
AIR COMPLIANCE MONITORING	DISTRIBUTIONLOGNORMAL	PREDICTED DAYS OVER 150 UG/M3
AIA	J	DEV
13	•	F-LIMITS UPPER STD GEOM DEV
) PAGE 13		IMITS UPPER
TABLE 6 (continued)		95-PCT-LIMITS OM MEAN LOWER UPPER
ABLE 6		MEAN
		GEOM
ENVIRONMEN		SAMPLES GE
ENT OF	ATES	YEAR
DEPARTM	ARTICUL	SITE
CONNECTICUT DEPARTMENT OF ENVIRONMENTAL	POLLUTANTPARTICULATES	TOWN NAME

COMMICCITO		L	T ROMINION T AND	AL FROIECITOR	₹ 0.1	PAG □	13 AIK	CUMPLIANCE	MONITORING
POLLUTANTPARTICULATE	PARTICUL	ATES						DISTRIBUTION-	-LOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES	GEOM MEAN	95-PCT	-LIMITS UPPER	STD GEOM DEV	PREDICTED DAYS GVER 150 UG/M3	PREDICTED DAYS OVER 260 UG/M3
ILFOR		16		رى ق	63	95	44.	0	
MILFORD	. 02	1971	54	65.1	59	72			
ILFOR		16		Š	64	63	.72°	13	<del>  </del>
ILFOR		4		6	46	55	<b>5</b> 50°		
ILFOR		16		•	46	57	• 52	. 2	
ILFOR		61		2.	57	89	e45	4	
ILFOR		67		2.	14	58	e 53	2	
ILFOR		16		<b>6</b>	53	62	.42°		
ILFORD		16		3,	64	59	•43	¥ewa¶ ·	
FOR	90	97		9		84	2	20	2
ILFOR	90	16		2		48	.50		
ILFOR	90	16		9		53	.70	5	
ILFOR	90	6		2.		47	.53	4	
ᄔ.	90	1974	09	6.04	37	45	1.548		
ILFOR	90	97		<b>e</b> 		46	649		
RRI	01	96		6			00.	4	
RRI	01	96		ę,			- L e	13	,d
RRI	01	96					67	. 2	
RRI	01	16		5			, 04	16	2
MORRIS	01	1971	48	35.8	31	41	1 0692	<del>, जर्</del> व	ı
RRI	01	16		4.			69°		
RRI	01	16		•			.81	2	
RRI	01	97		<b>-</b>			<b>9</b> 74		
RR I	01	6		8			,64		
RRI	01	97		S.			e75	2	
RRI	01	97		-			•63		
AUGATUC	01	96	24%	2.	51		<b>-</b>	10	
AUGATUC	01	96	34%	9	63		16	45	'n
AUGATUC	01	96	20	ထ	11	2	5	88	
AUGATUC	01	96	23	2°	74		7	19	
NAUGATUCK	01	1970	52	98°0	80	120	1.676	-	10
AUGATUC	01	97	52	5	16		57	42	7

<u> </u>	DEPARTN	MENT OF	ENVIRONMENTAL	TABLE	6(continued) FION	ed) PAGE	14 AIR	COMPLIANCE	MONITORING
POLLUTANTP	ARTICULATE	ATES						DISTRIBUTION-	LOGNORMAL
NAME	SITE	YEAR	SAMPLES	GEOM MEAN	95-PCT. LOWER	-LIMITS UPPER	STD GEOM DEV	PREDICTED DAYS OVER 150 UG/M3	PREDICTED DAYS OVER 260 UG/M3
$\preceq$	01	16		2	79	80	.67		
$\preceq$	01	6			6.5	70	e u		7
$\exists$	01	97		, ,	) 10 10 10 10 10 10 10 10 10 10 10 10 10	- 1	0 \		7
$\mathcal{Z}$	0 1	67		4 4	י ל ע	60	0 /	51	<b>,</b>
್ಲ	01	76		• ·	10.	66,	.60		
NAUGATUCK	01	1977	09	0 -	ף הי	70	φ τ τ τ	10	
$\tilde{S}$	01	97		50.8	45	57	1.659	n ~	
¥₹	01	\$		7	75		Ľ		(
TAI		96		. 4		) (	4 6		7
ITAIN	† C	1970	92	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1 0	y 9	1.620	29	2
TAT		07		, ,	2 ;		940		
· -		- 6		• † †	99		•63		2
7 F		- 1		•	68		740		
٦ + ٤ + - +	01	<b>~</b> !		6	41		64°		
ਰ ਹ		<u>,</u>		2.	47		* 6 I	i RV	
ITAIN	02	96		6		¢ mar	ָר.	Ċ	ŕ
T A T		96	2	o		-ر ا	, rt	2 0	ำ `
TAI		97		8 8		4 (	8 7 7 7	n c	<b>4</b> (
TAI	05	1971	57				• 	ر م د م	7
TAI		16		2.		0	6 / V	0 c	n i
I A I		16		-			) v	ט טיי	D (
Ι∀Ι		26		ô					η.
IAI		~		٦			) a	2,0	·
IAI		16		100.7	82	123	1.532	£3 £3	- W
IAI	03	9	す	0.5		~	,		1
TAI	03	96		, ,		7 (	) † 1 0	χ,	13
IVI	03	96	<b>(</b>	121	, C	n r	7		54
IAI	03	9		10			9 4 4 6	S	58
IAI	03	67		- C		V F	Ω .		91
TAT	) m	. ,		• •		-	82		16
4 F	n c	- 1		90			78		10
N	0 0	1912	7.7	6.69	61	80	1.724		ا درا
, , , ,	0 0	- 1		3			75		ሌ
- 4 - 1	<b>c</b> >	~		2			<b>-</b>	16	۱ 🗝

MACINDO!NOTTHRIGIOTOR			POLITANTPARTICILIATES.
AIR COMPLIANCE MONITORI	15	PAGE	CONNECTICUT DEPARTMENT OF ENVIRONMENTAL PROTECTION
			IABLE 6 (continued)

S GEOM MEAN         CAPETOR         PREDICTED         PAYS OVER         DAYS OVER         DAYS OVER         PAYS OVER <t< th=""><th>DEPARTMENT ARTICULATE</th></t<>	DEPARTMENT ARTICULATE
2.9     66     80     1.487     13       4.7     77     73     1.688     20       4.7     70     102     1.692     50       5.3     41     60     1.650     3       9.0     41     65     1.506     3       9.0     47     65     1.506     3       9.0     47     64     1.526     2       2.4     47     58     1.726     2       8.0     43     1.744     2       8.0     43     1.744     2       8.0     43     1.744     2       8.0     43     1.5478     2       8.0     40     49     1.6478     2       4.4     40     49     1.6494     1       4.5     53     1.6494     1       4.7     38     53     1.6494     1       4.4     45     55     1.494     1       5.5     40     51     1.638     3       4.8     1.490     1.638     3       8.8     1.672     7       1.0     1.644     2       4.8     1.490     1       1.0     1.607     2	YEAR SAMPLE
4-7         57         73         1-688         20           4-7         70         102         1-692         50           2-4         52         76         1-620         13           9-3         41         60         1-620         13           9-3         47         65         1-506         3           5-3         47         65         1-526         2           2-4         47         58         1-526         2           1-1         45         1-526         2         4           1-1         45         1-526         2         4           1-1         40         49         1-744         2           1-4         40         49         1-690         1           1-4         40         49         1-690         1           1-4         40         49         1-690         1           1-4         49         1-690         1         1           1-4         49         1-690         1         1           1-4         49         1-690         1         1           1-4         49         1-690         1	975 6
2.4         52         76         1.692         50           2.4         52         76         1.620         13           9.3         47         60         1.630         4           5.3         47         65         1.506         3           9.0         47         65         1.556         2           2.4         47         58         1.556         2           2.4         47         58         1.566         6           8.0         43         1.744         2           4.0         49         1.744         2           4.4         49         1.6478         2           4.0         49         1.6478         2           4.0         49         1.6478         2           8.7         1.6490         1         1.6590           1.4         5         1.6490         1           4.7         55         1.6490         1           4.8         5         1.6490         1           4.9         1.6490         1         1           4.9         5         1.6490         1           4.9         1.6490	6 5
2.4     52     76     1.620     13       9.3     41     60     1.630     4       5.3     47     65     1.526     2       2.4     47     58     1.526     2       2.4     47     58     1.556     8       8.0     43     1.744     2       4.0     49     1.678     2       8.7     40     60     1.690     1       1.4     35     50     1.690     1       4.7     38     53     1.690     1       4.7     38     53     1.690     1       5.5     40     51     1.690     1       5.6     40     1.690     1     1       4.7     49     1.690     1     1       5.5     40     51     1.638     3       4.8     1.490     1     7       5.0     49     1.475     7       5.0     49     1.475     7       5.0     49     1.644     2       4.8     1.640     7       5.0     1.644     2       6.1     1.644     2       6.1     1.644     2       6	16
9.3       41       60       1.630       4         5.3       47       65       1.506       3         9.0       44       54       1.526       2         2.4       47       58       1.726       8         8.0       33       43       1.746       2         4.4       40       49       1.747       2         4.4       40       60       1.650       1         8.7       37       49       1.550       1         9.4       45       53       1.656       1         1.4       38       53       1.649       1         5.5       40       51       1.649       1         4.8       53       1.649       1         5.0       49       1.649       1         1.1       63       1.649       1         4.8       1.442       7         4.8       1.647       2         4.9       1.647       2         4.0       51       64       1.644       2         4.9       1.647       2       2         4.9       1.644       2       2	968 2
5.3       47       65       1.506       3         9.0       44       54       1.526       2         2.4       47       58       1.555       4         4.0       49       1.544       2         4.0       49       1.546       2         4.0       49       1.690       7         1.0       40       60       1.690       7         1.0       50       1.690       7         1.0       50       1.690       1         4.0       50       1.690       1         5.1       49       1.690       1         4.0       51       1.690       1         5.1       40       51       1.690       1         5.2       1.490       1.6       1         4.0       51       1.490       1       1         5.1       64       1.640       2       1         6.7       51       63       1.644       2       1         6.1       1.0       1.544       2       1         6.2       64       1.544       8       1       2         6.1 <t< td=""><td>2 696</td></t<>	2 696
9.0     44     54     1.526     2       2.4     47     58     1.565     4       10.1     45     58     1.726     8       40.4     49     1.676     2       40.4     49     1.678     2       80.7     37     64     1.550     1       9.0     40     60     1.690     7       10.4     35     53     1.690     1       4.0     51     1.690     1       5.5     40     51     1.690     1       4.8     64     88     1.490     16       1.0     7     1.644     2       6.7     51     63     1.644     2       6.7     51     64     1.564     8       10.1     56     64     1.564     8       10.2     77     107     1.570     50       10.3     10     1.550     29       12.2     78     86     1.550     29	970 2
2.4     47     58     1.565     4       8.0     33     43     1.726     8       8.0     33     43     1.575     2       4.0     49     1.678     2       9.0     40     60     1.690     7       1.0     40     50     1.690     7       1.0     45     50     1.690     7       9.0     45     55     1.690     1       1.0     45     55     1.694     1       5.0     49     1.816     7       5.0     49     1.863     3       4.0     64     88     1.490     16       1.0     63     81     1.422     7       7     51     63     1.644     2       6.7     51     64     1.564     8       10.1     55     64     1.550     50       1.0     1.644     2     2       1.0     1.570     50       1.0     1.550     29       1.5     2     3       1.6     3     4     3       1.0     1.550     2       2.1     1.550     2       3.2     3 <td>971 5</td>	971 5
10.1       45       58       10.726       8         8.0       33       43       10.744       2         8.1       40       49       10.478       2         8.1       40       60       10.675       2         9.0       40       60       10.690       7         10.4       35       50       10.690       1         10.4       38       53       10.494       1         20.1       37       49       10.494       1         5.0       49       10.494       1       1         5.0       49       10.494       1       1         5.0       49       10.494       1       1         5.0       49       10.494       1       1         6.0       51       10.496       1       1         10.1       63       81       10.422       7       7         10.1       50       7       10.444       2       6         10.2       64       10.544       8       10.444       8         10.2       7       10.7       10.500       7       7         10.2 <td< td=""><td>972 5</td></td<>	972 5
8.0       33       43       1.744       2         4.4       40       49       1.678       2         8.7       37       64       1.575       2         9.0       40       60       1.690       7         1.4       35       50       1.566       1         1.4       45       53       1.6494       1         2.1       37       49       1.863       3         4.8       45       1.863       3       5         4.8       1.494       1       1         4.8       1.463       3       5         4.8       1.463       3       5         4.8       1.463       1       7         1.0       51       63       1.475       5         6.1       1.444       2       2         1.0       1.564       8       1.564       8         1.0       1.564       1.550       50         1.3       1.0       1.650       50         1.3       1.0       1.550       29         1.3       1.5       1.550       29	973 5
4.64     40     49     1.6478     2       8.7     37     64     1.575     2       9.0     40     60     1.690     7       1.4     35     50     1.590     1       1.4     35     53     1.696     1       2.1     45     55     1.494     1       2.1     37     49     1.638     3       4.8     64     88     1.490     16       4.8     64     88     1.475     5       6.7     51     63     1.607     7       7.9     55     61     1.444     2       6.1     1.444     2       6.2     64     1.550     50       7.2     77     110     1.570     50       1.6     77     110     1.550     59       1.6     77     110     1.550     29       1.6     77     110     1.550     29       1.6     76     1.550     29       1.6     77     1.550     29	974 6
9.0 40 60 1.690 7 1.64 35 50 1.590 1 9.4 45 55 1.6494 1 2.1 37 49 1.816 7 5.5 40 51 1.638 3 8.8 33 45 1.663 5 4.8 64 88 1.4490 16 1.1 63 81 1.475 5 6.7 51 63 1.607 7 7.9 55 61 1.444 2 0.1 56 64 1.570 50 1.03 83 100 1.620 58	1975 59 1976 13*
1.4     35     50     1.590     1       4.0     38     53     1.566     1       2.1     37     49     1.816     7       2.1     37     49     1.816     7       5.5     40     51     1.638     3       8.8     33     45     1.863     5       4.8     64     88     1.490     16       1.1     63     1.642     7       7     51     63     1.647     7       6.7     51     63     1.644     2       6.7     51     64     1.550     7       7     107     1.510     42       7     107     1.550     50       1.3     83     100     1.650       1.3     83     100     1.650       1.3     86     1.550     29	968
4.7     38     53     1.566     1       9.4     45     55     1.494     1       2.1     37     49     1.816     7       5.5     40     51     1.8638     3       8.8     33     45     1.863     5       4.8     64     88     1.4490     16       1.1     63     81     1.475     7       6.7     51     63     1.607     7       7.9     55     61     1.444     2       0.1     56     64     1.550     50       2.1     77     110     1.550     50       1.3     83     100     1.620     59       2.2     78     86     1.550     29	969
9.4       45       55       1.494       1         2.1       37       49       1.816       7         5.5       40       51       1.638       3         8.8       33       45       1.863       5         4.8       64       88       1.490       16         1.0       63       1.490       16       7         3.1       50       79       1.475       5         6.7       51       63       1.444       2         6.7       51       64       1.564       8         0.1       56       64       1.550       50         2.1       77       110       1.570       50         2.1       77       110       1.550       50         2.2       78       86       1.550       29	970 2
2.1     37     49     1.816     7       5.5     40     51     1.638     3       8.8     33     45     1.863     5       4.8     64     88     1.422     7       1.1     63     1.672     7       6.7     51     63     1.607     7       7.9     55     61     1.444     2       0.1     56     64     1.564     8       0.5     77     107     1.510     42       2.1     77     110     1.570     50       2.2     78     86     1.550     29	971 5
4.8       45       1.863       5         4.8       64       88       1.490       16         1.1       63       81       1.475       7         3.1       50       79       1.444       2         6.7       51       63       1.444       2         6.1       56       64       1.564       8         0.1       56       64       1.550       50         2.1       77       110       1.570       50         2.2       78       86       1.550       29	1972 59
4.8       4.5       1.863       5         4.8       1.490       16         1.1       63       81       1.422       7         3.1       50       79       1.475       5         6.7       51       63       1.607       7         7.9       55       61       1.444       2         0.1       56       64       1.564       8         0.5       77       107       1.510       42         2.1       77       110       1.570       50         1.3       83       100       1.650       59         2.2       78       86       1.550       29	
4.8       64       88       1.490       16         1.1       63       81       1.422       7         3.1       50       79       1.475       5         6.7       51       63       1.607       7         7.9       55       61       1.444       2         0.1       56       64       1.564       8         0.5       77       107       1.510       42         2.1       77       110       1.570       50         13       83       100       1.550       29         15       78       86       1.550       29	974 5
1.01     63     81     1.0422     7       3.1     50     79     1.0475     5       6.7     51     63     1.0607     7       7.9     55     61     1.0444     2       0.1     56     64     1.564     8       0.5     77     107     1.510     42       2.1     77     110     1.570     50       1.3     83     100     1.650     58       1.2.2     78     86     1.550     29	1966 24*
3.1     50     79     1.475     5       6.7     51     63     1.607     7       7.9     55     61     1.444     2       0.1     56     64     1.564     8       0.5     77     107     1.510     42       2.1     77     110     1.570     50       1.3     83     100     1.620     58       2.2     78     86     1.550     29	967 29
6.7 51 63 1.607 7 7.9 55 61 1.444 2 0.1 56 64 1.564 8 0.5 77 107 1.510 42 2.1 77 110 1.570 50 1.3 83 100 1.620 58 2.2 78 86 1.550 29	975
7.9     55     61     1.444     2       0.1     56     64     1.564     8       0.5     77     107     1.510     42       2.1     77     110     1.570     50       1.3     83     100     1.620     58       2.2     78     86     1.550     29	9 9 9 9 6
0.1     56     64     1.564     8       0.5     77     107     1.510     42       2.1     77     110     1.570     50       1.3     83     100     1.620     58       2.2     78     86     1.550     29	77 12
0.5     77     107     1.510     42       2.1     77     110     1.570     50       1.3     83     100     1.620     58       2.2     78     86     1.550     29	978 12
2.1     77     110     1.570     50       1.3     83     100     1.620     58       2.2     78     86     1.550     29	959 , 2
1.3     83     100     1.620     58       2.2     78     86     1.550     29	1965 26
2.2 78 86 1.550 29	8 296
	1968 178

CONNECTICUT	DEPARTMENT	MENT OF	ENVIRONMENTAL	TABLE 6 PROTECT	(continued)	I) PAGE	16 A	AIR COMPLIANCE	MONITORING
POLLUTANTP	ARTICULAT	ATES						DISTRIBUTION-	LOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES	GEOM MEAN	95-PCT- LOWER	-LIMITS UPPER	STD GEOM DEV	PREDICTED DAYS OVER 150 UG/M3	PREDICTED DAYS OVER 260 UG/M3
NEW HAVEN	01	1969	146	84°4 69°4	. 62	90	1.710	50	
	01	16		ιŲ Φ			431		
	01	16		9			.40		
	01	76		<b>~</b>			56	7	
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	010	- 1		ي ه. رو			69	13	prod
			١	) )			7	ro Ca	
NEW HAVEN		96		ထို			5		ያ የ
E HA		96		9		8	•60	$\sim$	
<b>3</b>		96		<b>-</b>			<b>63</b>		٠
NEW HAVEN	05	1970	21*	107.0	86	133	9	) & ) &	٦ <u>۲</u>
Z ':		67		\$			190		
3 I		76	_	40			55		
Z :		16		2 0			.72		7
<b>Z</b> :		6	9	<b>2</b> °			Ŷ		1 4
ĭ ĭ		<u> </u>		စ			6		· ~
<b>3</b> .		76		0			55		ı
Z :		26		Š			57	. LO	
<b>3</b> €		97		ဗိ		9	52	ı ın	
NEW HAVEN		96	*69	-			9		
		96	92	8			67		
NEW HAVEN		96	69	63.8			55	01	j
		6	*	4			43		
		97	41%	å			63		
		16	69				56	۰ ۳۰	
		6	19	'n			48		
NEW HAVEN	03	1974	19	9	41	52	9	4	
		76	59	52.1			*5°	۰ ۳۰	
		6	15%	0			1.396	1	
NEW HAVEN		96	•	ري ه	50		7	<b>L 7</b> .	ì
Z W	05	1968	*09	69.7	2 2	10	01007	0	<b>57</b>
			).	•	) 1		• 0 0	54	7

Name	CONNECTICUT	DEPARTMENT	MENT OF	ENVIRONMENTA	TABLE 6 TAL PROTECT	(continued)	ed) PAGE	17 AIR	R COMPLIANCE	MONITORING
Site   Feak   Samples Geom   Heave   Lower   Upper   Stock   Company   Com	1		ш					_	ISTRIBUT	-LOGNORMA
05         1969         57*         61.4         54         70         1,670         16           05         1971         63*         67.4         61         74         1,526         10           05         1973         58         57.6         51         60         1,5704         13           05         1974         58         57.6         51         66         1,704         13           05         1975         198         53.4         41         69         1,560         13           05         1975         198         53.4         41         69         1,700         100           06         1967         69%         98.1         85         11,360         100           06         1968         53.4         41         69         1,790         100           06         1967         69         77         113         1,290         100           06         1968         52.4         48         59         1,270         113           07         1960         23         93.5         77         113         1,510         100           193         51         46<		<b>⊥</b>	EA	AMPLE	EOM ME	5-PCT OWER	H H	TD GEOM DE	REDICTE AYS OVE 50 UG/M	REDICTE AYS OVE 60 UG/M
1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1, 1,	Z U		96	<b>-</b> -	-		7.0	.67		proof.
1972   1972   19 54.8   50   60   1.504   2     1973   58   57.6   51   1.504   13     1974   58   57.6   54   1.687   5     1975   1975   58   53.4   48   59   1.552   4     1976   1975   198   53.4   48   59   1.552   4     1976   1967   69%   198.1   185   113   1.950   100     1978   1978   106.5   99.1   132   1.710   113     1971   1966   23%   93.5   77   113   1.578   58     1977   1966   23%   93.5   77   113   1.578   58     1978   1977   65   52.4   48   58   59   1.461   2     1979   1971   64%   54.8   50   61   1.388   2     123   1977   46%   63.2   58   69   1.403   2     124   1958   25   195.6   79   1.403   2     125   1977   25   92.6   78   110   1.550   20     1978   25   1975   69   14.403   2     1988   1989   25   198.1   70   95   1.460   2     1989   25   198.2   86.8   73   104   1.530   35     1989   25   198.2   86.8   73   104   1.530   35     1980   25   198.2   84.8   126   11.403   2     1980   25   198.2   84.8   13   104   1.530   35     1980   26   198.2   84.8   110   1.540   58     1980   26   103.2   84   117   1.500   58     1980   26   103.2   84   117   1.500   58     1980   1980   26   103.2   84   117   1.500   50     1980   26   198.4   58   11   1.510   1.510   10     1980   26   198.4   58   11   1.510   1.510   10     1980   26   198.4   58   11   1.510   1.510   10     1980   26   198.4   58   11   1.510   1.510   10     1980   26   198.4   58   11   1.510   1.510   10     1980   26   198.4   58   11   1.510   1.510   10     1980   27   1.403   28   11   1.510   1.510   10     1980   28   29   20   20   20   20   20     1980   29   20   20   20   20     1980   20   20   20   20   20     1980   20   20   20   20   20   20     1980   20   20   20   20   20   20     1980   20   20   20   20   20   20     1980   20   20   20   20   20   20     1980   20   20   20   20   20   20   20     1980   20   20   20   20   20   20   20     1980   20   20   20   20   20   20   20	ñ N	0	26	3	<u>ا</u>		45	•52		
05         1973         58         57.6         51         66         1,704         13           05         1974         58         57.2         42         59         1,552         4           05         1976         1976         198.1         85         113         1,552         4           06         1967         69*         98.1         85         113         1,550         100         2           06         1968         59*         115.8         106.5         90         126         1,790         100         2           06         1969         42*         106.5         90         126         1,790         100         2           06         1969         42*         106.5         90         126         1,790         100         2           07         1960         42*         93.5         77         113         1,579         58           07         1971         63*         59.4         56         53         1,46         58         10         58           09         1973         61         48.8         45         56         67         1,46         56         1,46<	Z	0	16		4.		09	500	2	
05         1974         58         47.2         42         54         1.687         5           05         1975         198         53.4         48         59         1.552         4           06         1976         198         115.8         102         100         22           06         1968         59%         115.8         102         132         1.710         113           06         1968         59%         115.8         102         135         1.710         113         22           06         1969         42%         106.5         90         126         1.770         113         22           07         1969         42%         106.5         90         126         1.770         110         22           09         1971         63%         93.5         77         113         1.578         58           09         1972         65         52.4         48         56         1.544         3           09         1973         61         48.8         46         56         1.403         58           123         1974         46         53.2         74 <td< td=""><td>2 Ш.</td><td></td><td>26</td><td></td><td>7.</td><td></td><td>99</td><td>.70</td><td></td><td>_</td></td<>	2 Ш.		26		7.		99	.70		_
1,000   1,0000   1,0000   1,0000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1,000   1	EN.		16		<b>~</b>		54	<b>.</b> 68	S	
05         1976         19%         53*3         41         69         1*760         13           06         1968         59%         115*8         102         132         1*710         110         22           06         1969         42%         106*5         90         126         1*710         113         22           06         1969         42%         106*5         90         126         1*710         113         22           06         1969         42%         106*5         90         126         1*710         100         22           07         1972         65         23%         93.4         54         65         1*546         58           09         1972         65         52.4         48         56         1*541         2           09         1973         60         50.4         48         56         61         1*546         5           09         1973         40%         54.8         50         61         1.546         2           09         1975         40%         54.8         50         61         1.546         2           123         1978<	/EN		16		Š		59	e N	4	
06         1967         69**         98*1         85         113         1.950         100         22           06         1968         59**         115.8         102         132         1.710         113         2           06         1969         42*         106.5         93.5         77         113         1.570         113         2           07         1971         63*         59.4         54         56         1.510         58         2           09         1972         65         52.4         46         56         1.540         3           09         1972         65         52.4         46         56         1.546         3           09         1972         65         52.4         46         56         1.546         3           09         1972         60         50.7         46         56         11.546         2           09         1975         40*         56.8         60         11.463         2           123         40*         63.2         58         69         1.440         2           124         10         10         10         10	2 3 3		16	6	53		69	°16		H
06         1968         59%         115.8         102         132         1,710         113         2.           06         1969         42%         106.5         90         126         1,710         113         2.           07         1966         23%         93.5         77         113         1,578         58           09         1972         65         52.4         48         45         58         1,544         3           09         1972         61         48.8         45         53         1,461         2           09         1972         61         48.8         45         53         1,461         3           09         1972         61         48.8         45         53         1,461         2           09         1974         60         55.07         46         56         1,461         2           09         1975         40%         54.8         50         61         1,463         2           123         1977         46%         63.2         58         11403         1,555         20           A         01         1956         23         86.8	VEN		196	O.	ထိ		poud	. 95	0	
06         1969         42%         106.5         90         126         1.790         100         20           07         1966         23%         93.5         77         113         1.578         58         1.578         58           09         1971         63%         59.4         54         65         1.544         3         3         1.544         3         3         1.544         3         3         1.546         3         1.546         3         1.546         3         1.546         3         1.546         3         1.546         3         1.546         3         1.546         3         1.546         3         1.546         3         1.546         3         1.546         3         1.546         2         1.546         2         1.546         2         1.544         2         1.546         2         1.544         2         1.544         2         1.544         2         1.544         2         1.544         2         1.544         2         1.544         2         1.544         2         1.544         2         1.544         2         1.544         2         1.546         2         1.544         2         1.546	Z		196	δ	15	0	ŝ	170	-	
07         1966.         23*         93.5         77         113         1.578         58           09         1971.         63*         59.4         54         65         1.510         5           09         1972.         65         52.4         48.8         45         53         1.546         3           09         1973.         61         48.8         45         56         1.546         5           09         1974.         60         50.7         46.8         56         1.546         2           09         1974.         60         50.7         46.8         50         11.461         2           123         1977.         46.8         53.2         58         69         1.403         2           A         01         1957.         122         74.0         69         79         1.555         20           A         01         1958.         25         79.5         69         92         1.430         13           A         01         1960.         25         86.8         73         104         1.550         20           A         01         1962.         26 <td>VEN VEN</td> <td></td> <td>196</td> <td>2</td> <td>.90</td> <td>6</td> <td>2</td> <td>6 Z ®</td> <td>0</td> <td></td>	VEN VEN		196	2	.90	6	2	6 Z ®	0	
09         1971         63*         59.4         54         65         1.510         5           09         1972         65         52.4         48         65         1.544         3           09         1973         61         48.8         45         53         1.461         3           09         1974         60         50.7         46         56         1.544         2           123         1974         40*         54.8         50         61         1.544         2           123         1975         40*         63.2         58         69         1.403         2           A         01         1958         25         74.0         69         79         1.4403         2           A         01         1958         25         79.5         69         92         1.440         1.555         20           A         01         1950         25         86.8         73         104         1.550         20           A         01         1960         25         84.5         73         104         1.530         35           A         01         1960         26	V E N		96	3	ů		pund	.57		Ŋ
09         1972         65         52.4         48         58         1.5544         3           09         1973         61         48.8         45         53         1.461         2           09         1974         60         50.7         46         56         1.544         2           123         1974         60         54.8         50         61         1.546         2           123         1975         46*         63.2         58         69         1.403         2           A         01         1957         23         92.6         79         1.430         13           A         01         1957         23         92.6         78         110         1.555         20           A         01         1959         23         86.8         73         104         1.555         20           A         01         1960         25         19.6         99         1.4430         13           A         01         1960         25         84.5         73         104         1.540         20           A         01         1964         26         84.5         12	VEN	60	197	(4)	6			51	Ŋ	
09 1973 61 48.8 45 53 1.461 2  1974 60 50.7 46 56 11.544 2  123 1977 46* 63.2 58 69 1.403 2  123 1977 46* 63.2 58 69 1.403 2  123 1977 74.0 69 79 1.655 20  A 01 1958 25 79.5 69 92 1.450 13  A 01 1960 25 81.7 70 95 1.440 20  A 01 1964 26 84.5 73 97 1.440 20  A 01 1964 26 103.2 84 117 1.500 58  A 01 1965 25 100.7 85 119 1.510 56  A 01 1965 26 84.5 73 97 1.450 16  A 01 1965 26 84.5 73 97 1.450 56  A 01 1965 26 84.5 73 97 1.450 56  A 01 1965 26 84.5 73 97 1.450 56  A 01 1965 26 84.5 73 97 1.450 56  A 01 1965 26 84.5 73 97 1.550 58  A 01 1965 26 84.5 73 97 1.550 58  A 01 1965 26 84.5 73 99.2 84 117 1.550 58  A 01 1965 26 88.4 117 1.550 59  A 01 1965 26 88.4 117 1.550 59  A 01 1966 25 100.7 85 119 1.510 59  A 01 1968 26 68.4 58 89 117 1.510 50	/EN	60	197	65	2			54	3	
09 1974         60         50.7         46         56         1.544         2           09 1975         40*         54.8         50         61         1.388         2           123 1977         46*         63.2         58         69         1.403         2           A 01 1958         122         74.0         69         79         1.555         20           A 01 1959         25         79.5         69         92         1.430         13           A 01 1960         25         81.7         70         95         1.440         20           A 01 1961         26         84.5         73         104         1.550         20           A 01 1962         26         84.5         73         97         1.440         20           A 01 1962         26         80.0         71         90         1.340         7           A 01 1964         26         103.2         84         126         1.650         58           A 01 1965         24         99.2         1.450         58           A 01 1966         25         100.7         85         119         1.510           A 01 1966         26 <td>/EN</td> <td>60</td> <td>197</td> <td>61</td> <td>ά</td> <td></td> <td></td> <td>645</td> <td></td> <td></td>	/EN	60	197	61	ά			645		
123         1975         40%         54.8         50         61         1.388           123         1977         46%         63.2         58         69         1.403         2           123         1977         46%         63.2         58         69         1.403         2           A         01         1958         25         79.6         78         110         1.555         20           A         01         1958         25         79.6         69         92         1.4430         13           A         01         1960         25         86.8         73         104         1.550         20           A         01         1961         26         84.5         73         97         1.440         20           A         01         1962         26         80.0         71         90         1.440         20           A         01         1964         26         80.0         73         1.450         7           A         01         1964         26         103.2         84         126         1.650         58           A         01         1965         2	/EN	60	197	9 <b>9</b>	Ô			.54	2	
EN         123         1977         46*         63.2         58         69         1.403         2           EN         123         1978         122         74.0         69         79         1.555         20           EN         A         01         1958         25         79.5         69         92         1.430         42           EN         A         01         1959         23         86.8         73         104         1.530         35           EN         A         01         1960         25         81.7         70         95         1.440         20           EN         A         01         1961         26         84.5         73         97         1.440         20           EN         A         01         1962         26         84.5         73         97         1.440         20           EN         A         01         1962         26         80.0         71         90         1.440         20           EN         A         01         1964         26         103.2         84         126         1.450         1.450         1.6           EN <td>/EN</td> <td>60</td> <td>197</td> <td>0</td> <td><b>4</b> •</td> <td></td> <td></td> <td>38</td> <td></td> <td></td>	/EN	60	197	0	<b>4</b> •			38		
EN 123 1978 122 74.0 69 79 1.555 20  EN A 01 1957 23 92.6 78 110 1.500 42  EN A 01 1959 23 86.8 73 104 1.530 35  EN A 01 1960 25 81.7 70 95 1.450 20  EN A 01 1962 26 84.5 73 97 1.450 20  EN A 01 1964 26 80.0 71 90 1.340 7  EN A 01 1965 26 80.0 71 90 1.550 88  EN A 01 1965 26 84.1 17 1.500 58  EN A 01 1965 26 84.1 17 1.500 58  EN A 01 1965 26 84.1 17 1.500 58  EN A 01 1966 25 84.1 17 1.500 58  EN A 01 1966 25 84.5 67 102 1.510 50  EN A 01 1966 25 88.4 58.1 100.1 100.1 85  EN A 01 1966 26 88.4 58 119 1.510 1.510	/EN	2	197	9	φ			.40	2	
EN A 01 1957 23 92.6 78 110 1.500 42  EN A 01 1958 25 79.5 69 92 1.6430 13  EN A 01 1959 23 86.8 73 104 1.530 35  EN A 01 1960 25 81.7 70 95 1.640 20  EN A 01 1962 26 80.0 71 90 1.340 7  EN A 01 1964 26 103.2 84 126 1.650 88  EN A 01 1965 24 99.2 84 117 1.500 58  EN A 01 1966 25 100.7 85 119 1.510 50  EN A 01 1966 26 83.4 58 80 1.510 102	~	2	197	2	4			• 55		pad .
EN A 01 1958 25 79.5 69 92 1.430 13  EN A 01 1959 23 86.8 73 104 1.530 35  EN A 01 1960 25 81.7 70 95 1.450 20  EN A 01 1961 26 84.5 73 97 1.440 20  EN A 01 1962 25 80.0 71 90 1.340 7  EN A 01 1964 26 103.2 84 126 1.680 88  EN A 01 1965 24 99.2 84 117 1.500 58  EN A 01 1966 25 100.7 85 119 1.510 58  EN A 01 1968 26 68.4 58 80 1.510 100.7	/EN	0	195		2	78	110	.50		2
EN A 01 1959 23 86.8 73 104 1.530 35  EN A 01 1960 25 81.7 70 95 1.450 20  EN A 01 1961 26 84.5 73 97 1.440 20  EN A 01 1962 26 80.0 71 90 1.340 7  EN A 01 1964 26 103.2 84 126 1.680 88  EN A 01 1965 24 99.2 84 117 1.500 58  EN A 01 1966 25 100.7 85 119 1.510 50  EN A 01 1968 26 68.4 58 80 1.510 10	Z !! >	0	195		6	69	95	.43		
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EN A 01 1961 26 84.5 73 97 1.440 20 EN A 01 1962 26 80.0 71 90 1.340 7 EN A 01 1963 25 79.7 69 92 1.450 16 EN A 01 1964 26 103.2 84 117 1.500 58 EN A 01 1966 25 100.7 85 119 1.510 58 EN A 01 1966 26 82.6 67 102 1.510 50 EN A 01 1968 26 58.4 58 80 1.510	/E/S	0	196		<b>0</b>	70	95	645		
EN A 01 1962 26 80.0 71 90 1.340 7  EN A 01 1963 25 79.7 69 92 1.450 16  EN A 01 1964 26 103.2 84 117 1.500 58  EN A 01 1966 25 100.7 85 119 1.510 58  EN A 01 1967 26 82.6 67 102 1.510 50  EN A 01 1968 26 58.4 58 80 1.510	ZUA	0	196		<b>5</b>	73	16	<b>₹</b>		
EN A 01 1963 25 79.7 69 92 1.450 16 EN A 01 1964 26 103.2 84 126 1.680 88 1 EN A 01 1966 25 100.7 85 119 1.510 58 EN A 01 1966 25 82.6 67 102 1.510 50 EN A 01 1968 26 58.4 58 80 1.510	VEN	0	196		0	7.1	06	.34		
EN A 01 1964 26 103.2 84 126 1.680 88 1 EN A 01 1965 24 99.2 84 117 1.500 58 EN A 01 1966 25 100.7 85 119 1.510 58 EN A 01 1967 26 82.6 67 102 1.730 50 EN A 01 1968 26 68.4 58 80 1.510 10	VEN	Ф.	196		6	69	92	645		
EN A 01 1965 24 99.2 84 117 1.500 58 EN A 01 1966 25 100.7 85 119 1.510 58 EN A 01 1967 26 82.6 67 102 1.730 50 EN A 01 1968 26 68.4 58 80 1.510 10	/EN	0	196		03.	84	126	<b>.</b> 68		23
EN A 01 1966 25 100•7 85 119 1•510 58 EN A 01 1967 26 82•6 67 102 1•730 50 EN A 01 1968 26 68•4 58 80 1•510 10	/EN	0	196		9	84	117	.50		3
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EN A UI 1968 26 68.4 58 80 1.510 1	z .	) (	196		* 7	19	$\bigcirc$	e 7.3		-
	Z IJ	)	146		ထိ	<b>ک</b>	80	2		

CONNECTICUT D	DEPARTMENT	MENT OF	ENVIRONMENTAL	TABLE 6 PROTECT	(continued) ION	d) PAGE	18 AIR	COMPLIANCE MONITORING	MONITORING
POLLUTANTPA	ARTICULATE	ATES						DISTRIBUTION-	LOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES G	GEOM MEAN	95_PCT- LOWER	-LIMITS UPPER	STD GEOM DEV	PREDICTED DAYS GVER 150 UG/M3	PREDICTED DAYS OVER 260 UG/M3
NEW HAVEN A NEW HAVEN A NEW HAVEN A	01 01 01	1969 1970 1971 1972	26 26 26 29	85.9 93.2 89.4 59.4	72 80 79 52	102 109 102 69	1.570 1.480 1.390	452 70 70 70	2.2
NEW LONDON	0.1	1966.	14%	59.3	20	71	1.375	, <b></b>	
NORTH CANAAN NORTH CANAAN NORTH CANAAN	01 01 01	1974 1975 1976 1977	58 56 59 41*	38 4 4 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	34 36 36	43 55 46 47	1.687 1.672 1.794 1.574	7 4 2 2 1	
NORWALK NORWALK NORWALK NORWALK NORWALK NORWALK NORWALK NORWALK	01 01 01 01 01 01 01	1968 1969 1970 1971 1972 1973 1975	26 25 25 59 59 10*	444.55	50 50 50 50 50 50 50 50 50 50 50 50 50 5	70 67 74 63 61 60 60	1.630 1.470 1.700 1.469 1.560 1.603 1.619	16 16 22 33 4	
NORWALK	03	196	26	69.8	י ער ת הי	89	ري –		
NORWALK NORWALK NORWALK		197	6 5 8 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6 1 6	0 0 0	0, 4 tr (0, 1)	- L 9 9 1 2 2 4 2 1		0 4 ru 4 (	٠,
NORWALK NORWALK NORWALK NORWALK	0000 0000		50 50 60 60	56.4 56.1 50.8 57.0	51 52 55 50	62 62 67 67	1.640 1.480 1.620 1.471 1.674	20 2 10 4 10	
NORWICH	01	1966	. 43	67.8	61	76	1.450	7	

MONITORING	-LOGNORMAL	PREDICTED DAYS OVER 260 UG/M3																	-4					•	٦.		<b>,—</b>								
COMPLIANCE M	1	PREDICTED PAYS OVER 150 UG/M3	<b>!</b>	5		VI 4	ተ ሆ	ነ ሲ	<b>`</b> '('	١	<b>4</b> ~~	ł		c	Ď	13	í	, )	16	<b>-</b>	10	· ~	. ~ <b>4</b>	Ć	7.0			<b></b> 1 1		ĸ	7	`	1-∞		L
19 AIR	. 0	STD GEOM DEV	S	5 C	υ Ο (	4 4	1.522	53	67	5	4.8	45	41	ď	9	1.490		<b>†</b> •	4	1.490		53		4	ם כ	7 0		, ה י		1.619	ŝ	7	1.470		06/
) PAGE		IMITS UPPER	71													86	7.2	7.	† <b>†</b>	7 /	7.1	99	09	14	, r	17	- 4	o v	+ (	75	58	2	84		7
TABLE 6 (continued) PROTECTION		95-PCT-L LOWER	51	ر بر ر	24	61	54	52	42	43	45	43	42			<b>6</b> 2	54	ר ס ט ע	, ,	60	57	54	50					0 0		4 -	41		57		22
		GEOM MEAN	0.09		4 6	9	9	å	7.	47.8	9.64	47.1	45.7	ري ه	, (	73.5	2		٠	•	63.8	0	5	6		0	. 4	, 4	) 4	0 0	4 x a 4	-		(	0 α7
ENVIRONMENTAL		SAMPLES	27%	7.5	25	55	59	20	58	09	59	19	09	. 26			25*	9	90	) (	58	61	61	1 8 1	12%	17%	47	51	7. 7.	200	30%	S	17*	ć	×
Ü	ATES	YEAR	1967	96	1970	16	16	97	9.7	6	76	7	P	1963	Č	) )	97	76	1975		J (	5	6	96	96	16	76	1972	6	1077	~	96	1968	0.70	0
DEPARTMENT	ARTICULATE	SITE	010	0.1	01	01	01	01	01	01	07	70	01	10	ć	70	01	01	0			70	10	03	03	03	03	03	03	) (	<u>,</u>	01		Ç	
CONNECTICUT DE	POLLUTANTPAR	TOWN NAME	NORWICH	NORWICH	NORWICH	NORWICH	NORWICH	NUKETUL	NORMICE	NOT X	NOREICH		NURWICH	NORWICH	I	5	AYB	SAYB	OLD SAYBROOK	C A V D	2 2 4 0	0 A 4 0	SAYB	ORANGE	ORANGE	ORANGE	ORANGE	ORANGE	ORANGE	ORANGE		PUTNAM	PUTNAM	PLITNAM	

CONNECTICUT D	DEPARTMENT	ENT OF	ENV I RONMENTAL	TABLE 6	(continued)	1) PAGE	20 A	IR COMPLIANCE	MONITORING
POLLUTANTPARTICULATE	RTICUL	ATES						DISTRIBUTION-	LOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES	GEOM MEAN	95-PCT-	LIMITS UPPER	STD GEOM DEV	PREDICTED DAYS OVER 150 UG/M3	PREDICTED DAYS OVER 260 UG/M3
PUTNAM	02.		25	86.3	72 68	103	1.550	3.5	2 u
PUTNAM	02		1 10	e e	ာ ဆ တ	<b>)</b> ~	662		Λ ∞
PUTNAM		16		3	47	9	.61		,
PUTNAM				2.	37		61°		
PUTNAM		6		4.	30		<b>.</b> 83	'n	
PUTNAM		97		<b>~</b>	43		65	7	
PCTNAM		16		رب ه	4.1		-	54	. 2
PUTNAM	03	1966	27%	52.6	46	61	1.458	prond	
- Comp	01	9	21*	ထ		114	S	19	10
-	01	9	33*	9			55		
-	01	96	23	7.0			4		5
_	01	9	25	70.			•56		
_	01	97	22*	ô			•46		2
P	10	~	46	78.			•66		ĸ
	01	26	44	4.			• 74		35
_	01	6	17*	6		2	•48		M
STAMFORD	01	1974	55	66.2	58	16	1.726	24	2
		16	64	i S			•62		
_	01	67	* H	ဆီ			• 60	20	-
STAMFORD		96	~	5			50		
STAMFORD		26	21*	15.		4	•64		
STAMFORD		26	$\infty$	2.			177	N	35
STAMFORD		26	30*	12°		4	.89		
STAMFORD	03	1974	49%	46.7	40	55	1.805	ω	. ~
STAMFORD		6	20	- -			•69	13	<b>~</b>
STAMFORD		97	25*	ى ق			640	_	
STAMFORD	04	96		6			e79		<b>~</b> 4
STAMFORD	04	1970	\$25	55°5	43	72	1.814	16	2
STAMFORD		1971	6	°			16°		3
STAMFORD	04	16		2.			•68		2

MONITORING	-LOGNORMAL	PREDICTED DAYS OVER 260 HG/M3	) m c	1	٢	en red				) 4	) =4 4			<del>(veil</del> )	20	) m								•			-	
COMPLIANCE	ISTRIBUTION-	PREDICTED DAYS OVER 150 UG/M3	67	)	7		<b>-</b>	10 4			16	ſſ	ı so	10		32	~	1	7	٠ ١٠٠	) 00	000	. 4	· ന	2	7	33	'n
21 AIR	<b>Ω</b> .	STD GEOM DEV	.936 .981	1.837	1.846	9.0	50 Y	• 43	• 02		•69°	S		97¢	8	1 • 600	40	1.538			69	64		-4	1.634		S	1.713
d) PAGE		-LIMITS UPPER		49 61	87	73	4 0 4	99		87		99	69	19		66		19	50	51	65	19	71	62	51	68	<b>†</b>	53
(continued)		95-PCT- LOWER		35 34		57				55		50	57	47	76	69	54	55								38		
TABLE 6 L PROTECT		GEOM MEAN	80.6	5.	73.4	401	• 6	ထ		0°69	2。		62.6	ص ص		82.6	•	9.09	0	3	52.4	4.	6	9	4.	51,0	X)	45.7
ENVIRONMENTA		SAMPLES	33 59		<b>48</b> *	4.0 in				41	m	36*	61	09		26		61	30*	S	24	23	21*	44	4.3	14* *	) (	46
	ATES	YEAR			97	1975	16	97	16	1972	5	1976	<b>-</b> 6	<i>-</i>	9.5	1960	<b>,</b>	1976	1966	9	9	96	<u> </u>	76	7 (	1975	- r	<u>ب</u>
EPARTM	ARTICULAT	SITE	40,00	04	07	07	07	0.7		07.		123			01	7 0	ð	123	01	0.1	07	0 7	70	0.5	7 7	7 0	7 6	<b>T</b> O
CONNECTICUT DEPARTMENT OF	POLLUTANTPA	N NAME	AMFORD	X X	MFORD	AMFORD	MFORD	MFORD	AMFORD	3 T C X C C C C C C C C C C C C C C C C C	טאט	MFORD			TAMFORD	MTUKU MTURU	,	MFORD 03/	ATFORD	みっている	AIFUR	A - FUK	A - T CK	AITUK	7 C U F V	ATFOR		
CON	P 01	NAOF	STA	_	-	STA		-	STA	- 20	**	STAM	4 - 0	₹ - -	STAI	STAI	· •	STAI	STR	7	X 1	7 6	7 6	N T Y	410	S T C	O T D	2

CONNECTICUT	DEPARTMENT	MENT OF	ENVIRONMENTAL		TABLE 6 (continued)	I) PAGE	22 AI	IR COMPLIANCE	MONITORING
POLLUTANTP	ARTICULATE	ATES				-		DISTRIBUTION-	LOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES	GEOM MEAN	95-PCT- LOWER	-LIMITS UPPER	STD GEOM DEV	PREDICTED DAYS OVER 150 UG/M3	PREDICTED DAYS OVER 260 UG/M3
TRATFOR	01	6	47	9			9	2	
TRATFOR	01	1977		_		47	1.628	2	
STRATFORD	01	1978	21*		50	7.8	°64	9	<b>≠</b>
TRA		9	20%	76.4	62	66	1.600		5
$\alpha$	05	9	21*	Ð	59	84	1.490	01	
TRA		16	œρ	75.2	09	46	1.596		<b>⊢</b> ≂4
TRA		-	38	ô	19	81	ιζ		<b>←</b>
TRA		16	20*	4	53	78	3	Ø	
	05	1973			48	70	1 . 446	2	
	05	1974		ဆ	51	99	1.621	Φ	
STRATFORD	05	1975	64	52.7	46	9		5	
	05	1976		ő	54	19	1.567	<b>&amp;</b>	
	05	97		-	55	65	$^{\circ}$	7	
	90	97		υ, e	50	62	° 59	7	
THOMASTON	01	1961	33*	82.0	19	101	1.839	58	0.1
THOMASTON	03	96	15*	75.2		96	~	24	<b>,d</b>
<b>THOMASTON</b>	03	96	18*	7		81	64°	ဆ	
THOMASTON	03	16	24%	4.		88	.53		
THOMASTON	. 03	1971	47	72.2	61	85	1.799	45	S
THOMASTON	03	16	45	Š		16	975		7
THOMASTON	03	1973	57	6		45	2	, <b>-</b>	
THOMASTON	03	6	29			48	•76	S	
THOMASTON	03	97	57	0		20	° 58	2	
THOMASTON	04	1966	29*	63.9	53	77	1.644	9 =	pag
TORRINGTON	01	96			33	14	5.9	_	
TORRINGTON	01	9	S		44	19	50	7	
TORRINGTON	01	96		9	50	74	e 57	ထ	
TORRINGTON	01	1969	23	2	53	75	1.530	80	
TORRINGTON	01	~		83.1	7.1	98	<b>6</b> 48	24	Ħ

Declination	CONNECTICUT DEPARTMENT	EPARTM	IENT OF	ENVIRONMENTA	TABLE L. PROT	6 (continued) ECTION	d) PAGE	23 AIR	R COMPLIANCE	MONITORING
National State   Sta	TPA	RTICUL	ATES						ISTRIBUT	
N	ā.	<b>j</b> d	EA	SAMPLES	EOM ME	5-PCT OWER	-LIMITS UPPER	TD GEOM D	OICT S OV UG/	REDICT AYS OV 50 UG/
N	NO	01	97		سما	. 19	8	7	6.7	
N	NO	01	16	55	ゅ	56	75	7,7	7 C	<b>4</b> r
N	NO 1	01	6	29	-	42	53	65	+ 4	n
No.   1977   1978   1988   1582   16     No.   123   1975   28*   45*6   40   52   1*401     No.   123   1975   28*   45*6   40   55   1*401     No.   123   1976   57   67*7   56   77   1*653   16     No.   123   1978   120   59*7   56   77   1*653   16     No.   1973   48   56*2   50   63   1*573   5     No.   1974   48   28*6   24   34   1*858   1     No.   1975   42*   28*8   24   34   1*858   1     No.   1976   42*   28*8   24   34   1*858   1     No.   1976   12*   25*7   26*   43*3   37   51   1*486     No.   1976   58   58*4   52   65   1*601     No.   1978   60   58*4   52   65   1*601     No.   1978   60   58*4   52   65   1*799     No.   1970   9*   39*3   25   61   1*795     No.   1970   9*   42*0   24   72   2*053     No.   1966   34*   84*0   71   10   1*770     No.   1967   6*   6**1   44   99   1*657     No.   1968   24*   88*2   71   10   1*770     No.   1968   24*   88*2   71   70   70     No.   1968   24*   88*2   71   70   70   70     No.   1968   24*	<b>Z</b> Z	01	97	09	(C)	47	9	.68	- დ	
123   1975   28#	2	70	<u>_</u>	30*	ထိ	58	80	* 58		H
National State	NO	~	16	28*	ري ه	40	52	0.40		
N   123   1977   61   62.7   56   71   1.653   165   165   170   123   1978   120   59.7   54   66   1.929   29   29   1.929   29   1.929   29   1.929   29   1.929   29   1.929   1.929   1.929   1.929   1.929   1.929   1.929   1.929   1.697   1.929   1.697   1.929   1.697   1.929   1.697   1.929   1.697   1.929   1.697   1.929   1.697   1.929   1.697   1.929   1.697   1.929   1.697   1.929   1.697   1.929   1.920   1	NO	2	16	57	6	59	7.7	. 70		0
N         123         1978         120         59.7         54         66         1,929         29           N L/         123         1975         58         56.2         56.2         50         63         1,573         59           O1         1975         48         28.6         24         34         1.858         1           O1         1975         42%         28.6         24         34         1.858         1           O1         1975         42%         28.6         24         34         1.554         1           RD         01         1975         42%         28.6         24         34         1.497         1           RD         01         1976         43.3         37         51         1.497         1           RD         01         1977         53         57.0         50         65         1.0497         7           RD         02         1977         53         57.0         50         65         1.799         4           RD         03         1970         9*         42.0         24         72         2.053         13           RD	N :	2	16	61	2.	56	7.1	65		7 -
V 1/ 123 1975         58         56.2         50         63         1.573         5           V 1/ 123 1975         48         28.6         22         30         1.851         1           V 1 1974         56         28.6         22.7         24         34         1.851         1           V 1 1975         42%         28.8         24         34         1.851         1           V 1 1976         42%         28.8         24         34         1.497         1           V 1 1976         60         58.4         26         65         1.601         7           V 2 1 1977         53         57.1         51         64         1.601         7           V 2 1 1978         60         58.4         52         65         1.799         20           V 2 1 1978         61         57.0         50         65         1.799         7           V 2 1 1970         7         43.0         25         65         1.795         4           V 2 1 1970         94         42.0         24         72         2.053         13           V 2 1 196         196         196         1.44         99         1.480 <td>S</td> <td><math>\sim</math></td> <td>97</td> <td>120</td> <td><b>6</b></td> <td>54</td> <td>99</td> <td>.92</td> <td></td> <td>4 IV</td>	S	$\sim$	97	120	<b>6</b>	54	99	.92		4 IV
01         1973         48         28.6         22         30         1.858         1           01         1974         56         25.6         22         30         1.851         1           01         1975         42*         28.8         24         34         1.754         1           01         1975         42*         28.8         24         34         1.697         1           00         1 1976         60         58.4         52         65         1.6608         1           00         1 1976         60         58.4         52         65         1.608         8           00         1 1977         53         57.1         51         64         1.601         7           00         1 1977         53         57.1         51         64         1.608         8           00         1 1978         61         57.0         50         65         1.799         20           00         1 970         7         43.0         25         75         1.826         4           00         1 970         9*         42.0         24         72         2.053         13		2	97		9			.57	ĸ	
01     1974     56     25.6     22     30     1.851     1       01     1975     42*     28.8     24     34     1.754     1       01     1976     12*     26.4     24     34     1.754     1       01     1976     12*     26.4     24     29     1.497     1       00     1978     26.4     43.3     37     51     1.486     8       00     1976     60     58.4     52     65     1.608     8       01     1978     61     57.0     50     65     1.799     20       00     02     1970     7     43.0     25     61     1.795     4       00     03     1970     9*     42.0     24     72     2.053     13       00     04     1970     9*     42.0     24     72     2.053     13       01     1966     34*     84.0     71     99     1.657     50       01     1967     60     80.0     70     91     1.720     50       01     1968     24*     88.2     71     110     1.720     50	Z	01	1973	48	α	24	34	.85		
01       1975       42*       28.8       24       34       1.754       1         01       1976       12*       22.7       18       29       1.497       1         01       1976       26.4       24       29       1.497       1         00       1976       60       58.4       52       65       1.608       8         00       1977       53       57.0       50       65       1.601       7         01       1978       61       57.0       50       65       1.799       20         00       02       1970       7       43.0       25       75       1.826       7         00       03       1970       9*       42.0       24       72       2.053       13         00       04       1970       9*       42.0       24       72       2.053       13         00       1967       60       80.0       70       91       1.770       58         01       1968       24*       88.2       71       110       1.720       5.8	zi	01	9 /	99	Š	22	30	85	فسم ا	
01       1976       112**       22.7       18       29       1.497         01       1978       119       26.4       24       24       29       1.697         00       01       1975       26.*       43.3       37       51       1.486         00       01       1976       60       58.4       52       65       1.608       8         00       01       1977       53       57.0       50       65       1.799       20         00       02       1970       7       43.0       25       61       1.799       7         00       04       1970       9*       42.0       24       72       2.053       13         00       04       1970       9*       42.0       24       72       2.053       13         00       04       1970       9*       42.0       24       72       2.053       13         00       196       34*       84.0       71       99       1.480       7         01       1967       60       80.0       70       91       1.720       50         01       1968       24*	<b>z</b> :	01	16	45%	မ	24	34	5		
01       1978       119       26.4       24       29       1.697         00       01       1975       26.8       43.3       37       51       1.486       8         00       01       1976       60       58.4       52       65       1.608       8         00       01       1977       53       57.0       50       65       1.501       7         00       01       1978       61       57.0       25       75       1.826       7         00       02       1970       7       43.0       25       61       1.795       4         00       03       1970       9*       42.0       24       72       2.053       13         00       04       1970       9*       42.0       24       72       2.053       13         00       1960       34*       84.0       71       99       1.480       7         01       1968       24*       88.0       71       110       1.770       50         01       1968       24*       88.2       71       110       1.720       50	z :	01	76		2	18	29	648	•	
LD         01         1975         26*         43.3         37         51         65         1.6486         8           LD         01         1976         60         58.4         52         65         1.6608         8           LD         01         1977         53         57.0         50         65         1.601         7           LD         02         1978         7*         43.0         25         75         1.826         7           LD         03         1970         9*         42.0         24         72         2.053         13           LD         04         1970         9*         42.0         24         72         2.053         13           LD         196         6*         66.1         44         99         1.480         7           LD         196         34*         84.0         70         91         1.770         50           LD         196         24*         88.2         71         110         1.770         58	<b>Z</b> .	01	26	<del></del> 4	9	54	59	69.		
20     01     1976     60     58.4     52     65     1.608     8       20     01     1977     53     57.1     51     64     1.601     7       20     01     1978     61     57.0     50     65     1.826     7       20     02     1970     7     43.0     25     61     1.7795     4       20     04     1970     9*     42.0     24     72     2.053     13       20     05     1970     6*     66.1     44     99     1.480     7       21     1966     34*     84.0     70     91     1.770     50       21     1968     24*     88.2     71     110     1.770     58	ORD	01	97	26*	•	37	51	9		
(2)     (1) <td>O.K.O.</td> <td>01</td> <td>97</td> <td>09</td> <td>0</td> <td>55</td> <td>65</td> <td>•</td> <td>∞</td> <td></td>	O.K.O.	01	97	09	0	55	65	•	∞	
(1)     (1) <td>2 2 2</td> <td>7 6</td> <td>) ) (</td> <td>53</td> <td>9</td> <td>51</td> <td>64</td> <td><b>O</b></td> <td>_</td> <td></td>	2 2 2	7 6	) ) (	53	9	51	64	<b>O</b>	_	
20         1970         7*         43.0         25         75         1.826         7           20         03         1970         9*         39.3         25         61         1.795         4           20         04         1970         9*         42.0         24         72         2.053         13           20         05         1970         6*         66.1         44         99         1.480         7           01         1966         34*         84.0         71         99         1.6770         50           01         1967         60         80.0         70         91         1.770         50           01         1968         24*         88.2         71         110         1.770         58	2 K	10	~	19	0	20	65	6	20	2
10         03         1970         9*         39.3         25         61         1.795         4           10         04         1970         9*         42.0         24         72         2.053         13           10         05         1970         6*         66.1         44         99         11.480         7           01         1966         34*         84.0         71         99         11.657         50           01         1967         60         80.0         70         91         11.770         58           01         1968         24*         88.2         71         110         1.0720         58	ORD	05	97	7%	3	25	75	.82	_	
10     04     1970     9*     42.0     24     72     2.053     13       10     05     1970     6*     66.1     44     99     1.480     7       01     1966     34*     84.0     71     99     1.657     50       01     1967     60     80.0     70     91     1.770     50       01     1968     24*     88.2     71     110     1.720     58	ORD	03	97	*6	•	25	61	• <b>7</b> 9	<b>,</b>	
10     05     1970     6*     66*1     44     99     1*480     7       01     1966     34*     84*0     71     99     1*657     50       01     1967     60     80*0     70     91     1*770     50       01     1968     24*     88*2     71     110     1*720     58	ORD	04	1970	*6	2	24	72	•05		2
01 1966 34* 84.0 71 99 1.657 50 01 1967 60 80.0 70 91 1.770 50 01 1968 24* 88.2 71 110 1.720 58	ORD	0.5	16	*9	0	44	66	•48	7	
$01 \ 1968 \ 24 \approx 88.2 \ 71 \ 110 \ 1.0720 \ 58$	<b>≻</b> ≻	100	1966	34%	84.0	71	66	65	50	S
	<b>&gt;</b>	01	1968	24%	88.2	71		011	u D	<b>-</b> 00

CONNECTICUT	DEPARTMENT		OF ENVI	ENVIRONMENTAL	TABLE 6 PROTECT	(continued) ION	) PAGE	24	AIR COM	COMPLIANCE	MONITORING
POLLUTANTPARTICULAT	PARTICL	JLATES							DISTR	IBUTION-	-LOGNORMAL
TOWN NAME	SITE	YEA	R SAI	AMPLES (	GEOM MEAN	95-PC.T-I	LIMITS UPPER	STD GEOM D	PRE DAY EV 150	DICTED S OVER UG/M3	PREDICTED DAYS OVER 260 UG/M3
WATERBURY WATERBURY	00	prod prod	<b>6</b> С	25		82 76		.46			2
WATERBURY WATERBURY	010	1 1971	, <b>, ,</b> ,	55		75	9 20	1.588		42	i m m
WATERBURY	ō	i ,	ım	\$97	9	65		, e , v			) ~
WATERBURY	0	prod P	<b>√</b> 1.	51	2	63		•72 -			41
WA I EKBÜRY	0	<del>pred</del>	v	\$0 <i>2</i>	2.	64		•74			-
WATERBURY	0		<b>.</b>	\$02	3,	42	68	e 7 1		10	<b>-</b>
WATERBURY	Ö		S	59	65.5	59	73			10	
WATERBURY	02	2 1976	9	09	60.1	54	29	• 9		10	
WATERBURY	Ö	_	7	09	0	64	11	1.505	er.	10	
WATERBURY	Ö		8	09		54	7.2	• 84		53	7
ATER		197	5		<b>~</b>			53		4	
ERBUR	0		9	13*	65.0	24	89	1.9711		20	2
TER	12	3 197	5	37*	4	74		53			2
TER	12	3 197	9	09	9	76		•68			_
WATERBURY	12	3 197	7	118	81.3	75.	88			42	4
TER	12	3 197	80	122	ô			• 7 J			S
WATERBURY	0	1 196				54	77	Ωi.	-	0	
WATERBURY	0 V	1 196	ທູ	56	105.2	85	130	1.740	•	100	20
WATERBURY	0	1 196			9	68	26	<b>9</b>	0	50	
WATERBURY	0	1 197			ν, e	71	104	9.	•	42	4
WATERBURY		1 197			0	75	0	<b>7</b> •	0	29	-
WATERBURY		1 . 197			ထ	58	82	e M	•	16	7
WATERFORD	0	1 197	4	48*	• -				10	md	
WATERFORD	0	1 197	'n	09	2.			• 75	•		
WATERFORD	0	197	9.	57	4 .			•63			
WATERFORD	0 0	197	<b>-</b>	61	32.2	29	36	I • 66	ъ (		
MAINKIDKU	כ	161 1	<b>x</b>	19	9			• 52	m	,	

CUNNECTIONT DEPARTMENT DE ENVIRONMENTAL PROTECTION PAGE 25	. 52	AIR COMPLIANCE MONITORING
JFANTPARTICULATES	•	DISTRIBUTIONLOGNORMAL

PREDICTED DAYS OVER 260 UG/M3			·				C	) =				,							2	•		
PREDICTED DAYS OVER 150 UG/M3		1	p-cd	^	j			) (r			_		<b>†</b> (	<b>x</b> 0	m	ĸ	۱ ۱	S	42		2	2 2
STD GEOM DEV	7	- (  -	٥ ٧			,	1.868				1.420	Ľ	1 1	0,00	9	1.722	•	Ç	1.886		1 . 536	52
LIMITS UPPER	r r	י ני	<b>4</b>	54	99	į	717	77	. u	``	49	49	~ a	2 4	Ç :	2	ď	2	100			89
95-PCT-LIMI LOWER UPP	56	76	0	<b>44</b>	45	ù	20	50	77	- 0	φ.	53	7	- h	) )	39	44	2	47		40	39
GEOM MEAN	45.7	( · U 7)	) (	$\mathfrak{A}$	54.7	c	9	œ H	51.0	کیا ا	٦	58.2		; c	,	/ e t t	52.0	,	68.7		48.7	51.8
SAMPLES		61		7		(4	) (	2	23*	75	) i	99	20	S.C.	0 4	00	58	. (	1.5%		20%	11%
YEAR	1973	1	0	ا س	16	96	, (	9	1969	97	· (	5	6	~	7	-	~	,	1910	,	1966	96
SITE	01	01		70	10	C		10	01	0	, ,	70	01	01	5	4	01	ċ	70	(	03	03
TOWN NAME	WILLIMANTIC	ILLIMANTI	TIMANTITI	1	ILLIMANII	INCHESTE	11001	TINCUL ON T	N S	WINCHESTER	CTC	INCHEST	STE	INCHESTE	STF	1 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	<u>۷</u> ۳	MINCHESTED	11011011	L	WINCHEN	_ T

SAMPLING NOT RANDOM OR OF INSUFFICIENT SIZE FOR REPRESENTATIVE ANNUAL STATISTICS. \*\*

TABLE 7

CONFIDENCE OF COMPLIANCE WITH ANNUAL TSP STANDARDS (1978)

SECONDARY STANDARD

PRIMARY ST.ANDARD

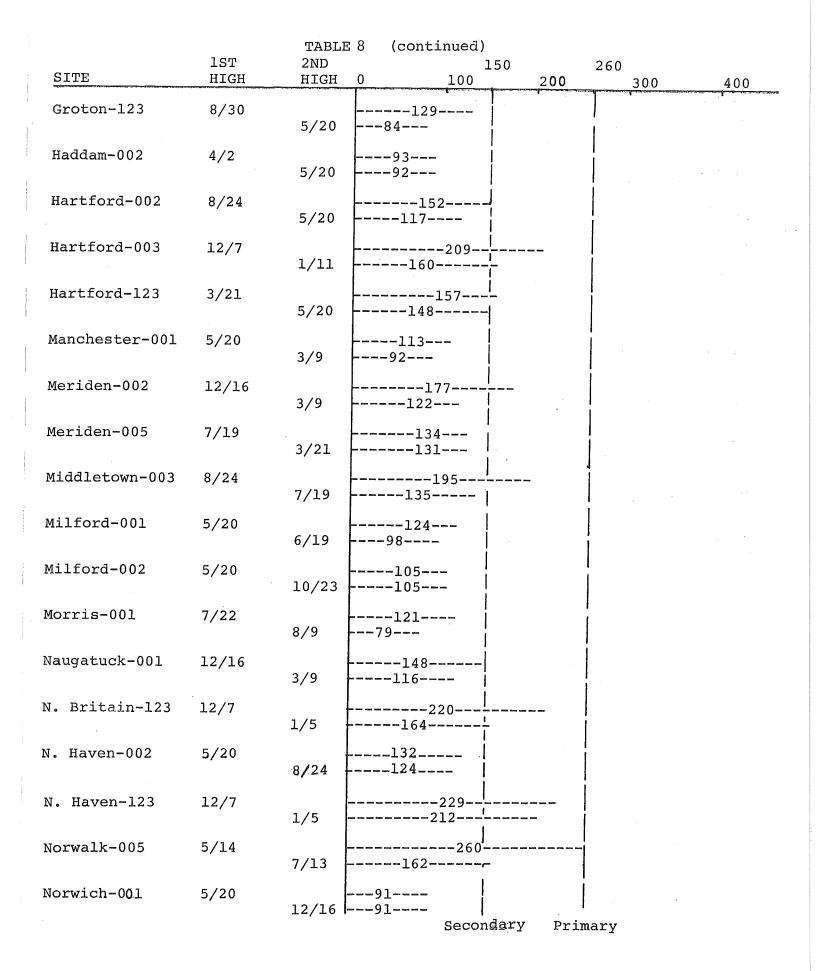
UNCERTAIN WHETHER STANDARD HAS BEEN ACHIEVED OR EXCEEDED	Ansonia 03 Meriden 02 Meriden 05 Middletown 03 New Britain 123 Norwalk 05 Stamford 07 Stamford 123 Stratford 05 Torrington 123 Wallingford 01
95% CONFIDENT STANDARD HAS BEEN EXCEEDED (> 60)	Bridgeport 123 Hartford 03 Hartford 123 New Haven 123 Waterbury 123
UNCERTAIN WHETHER STANDARD HAS BEEN ACHIEVED OR EXCEEDED	New Haven 123 Waterbury 123
95% CONFIDENT STANDARD HAS BEEN EXCEEDED (> 75)	

TABLE 8

1978 MAXIMUM 24-HOUR TSP CONCENTRATIONS\*

SITE	lst HIGH	2nd HIGH	0 100	150	200	260 300	4 Öʻ0
Ansonia-003	12/16	3/18	183				
Berlin-001	1/26	5/20	91 90				
Bridgeport-001	5/20	8/24	112 106				
Bridgeport-123	1/5	4/29	194 184				
Bristol-001	12/16	5/20	131 129				
Bristol-004	5/20	3/21	127 102				
Burlington-001	8/9	10/23	97 94	1			
Danbury-123	12/16	3/21	187 124	<u> </u>			
Derby-123	8/24	5/20	128 110				
E. Hartford-002	4/2	12/16	176 123				
Enfield-123	5/20	12/16	98 90	]	•		
Greenwich-001	3/21	8/24	146 128	-	. 1		
Greenwich-003	3/21	3/15	132 129	1			
Greenwich-04	8/24	6/7	128 99				
Greenwich-08	7/13	7/7	159 124	İ			
*	2		Sec	condar	y Pr	imary	

<sup>\*</sup> Units in  $\mu g/m^3$ 



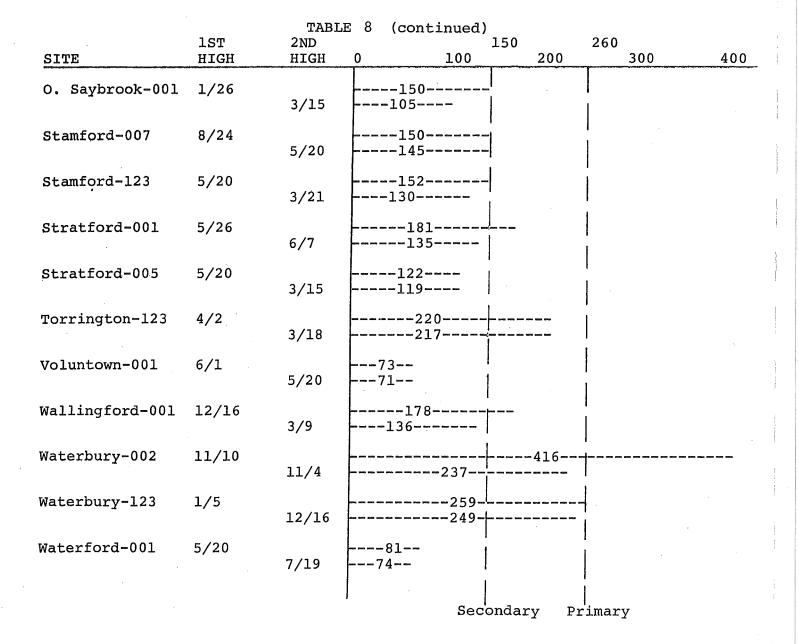


TABLE 9 SUMMARY OF THE STATISTICALLY PREDICTED NUMBER OF SITES

## EXCEEDING THE 24-HOUR TSP STANDARDS

## 1971-1978

TOTAL #	OF HI-VOL SITES	44	46	44	. 62	55	41	39	36
NYS EXCEEDING RD (260 µg/m³)	% of Total Sites	45%	28%	25%	%8	4%	%/	3%	%6L
SITES WITH > 2 DAYS EXCEEDING THE PRIMARY STANDARD (260 µg/m <sup>3</sup>	Number of Sites	20	13	11		2	က	٦	7
				,					
DAYS EXCEEDING IDARD (150 µg/m <sup>3</sup> )	Total Sites	84%	83%	70%	%62	75%	88%	%69	%19
SITES WITH > 2 DAYS THE SECONDARY STANDARD	Number of Sites	37	43	31	49	41	36	27	22
	YEAR	1971	1972	1973	1974	1975	1976	1977	1978

TABLE 10 CHEMICAL CHARACTERIZATION OF HI-VOL TSP, 1970-1978

TOWN	ANSDNIĀ	ANSONIA	BERLIN	BRIDGE PORT	BRIDGEPORT	BRIDGEPORT	BRISTOL	BRISTOL	BRISTOL
SITE	00	E 000	00	.00	000	2. 2.	00	002	000
YR #S	70 25 71 7	71 18 72 30 74 26 75 28 75 28 77 30 78 30	73 28 74 28 75 27 76 7	70 26 71 72 24 73 25 74 75 30 77 75 29 78 20 78 20 78 20	72 4 73 30 74 30 75 8	75 21 76 31 77 29 78 31	71 22 77 22 27 73 29 24 75 29 77 75 29 77 78 31 91 91 91	27 20 40 40 80 80 80 80 80 80 80 80 80 80 80 80 80	73 9
. AL			00	0000	B000	ວວວ ພໍລໍພໍ	000	0 C m	<b>0</b> O
BE		0.0000 0.0000 0.0000 0.0000 0.0000 0.0000	000000000000000000000000000000000000000	0.0000 6 0.0000 6 0.0000 0.0000 0.0000	0.0002	5 0.0000 6 0.0000	000000	0.0000	0.0000
8	0.03	0000000	00000	00000000	0000	0000		000	00
CR	0366 0.009 0406 0.003	07 0.011 36 0.015 86 0.006 59 0.009 59 0.006 59 0.006 603 0.008 64 0.005	017 0.005 027 0.005 020 0.005 015 0.002	110 0.005 079 0.006 078 0.006 046 0.005 065 0.005	0651 0.009 0244 0.010 0123 0.010 0056 0.013	0042 0.004 0071 0.011 0066 0.013	0026 0.007 2210 0.005 3337 0.009 3370 0.003 3314 0.007 3084 0.009	0224 0.000 0241 0.000 0041 0.004	.0095 0.01
3		24.000000000000000000000000000000000000	0.37 0.26 0.13 0.20	68 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	9 0.56 0 0.28 0 0.21 3 0.19	4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	20000000000000000000000000000000000000	9 0.78 4 0.95	5 0.84 3 0.57
Œ.	3.30	2 0 0 0 0 0 0 0 0 0 0 0 0 0	00000		0.66	0.11	0.00000	0.26	0.54
8	1.57		0.57 0.59 0.49 0.36 0.36	7.4.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7.7	3.33 1.45 1.25		0.78 0.03 0.98 0.96 72	0 0 0 0 0 0 0 0 0 0	0.04
₹	0.109 (	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.008	0.0000000000000000000000000000000000000	0.030 0.082 0.014 0.023	0.031	0000000	0.000	0.016
¥.	0.080	0.020 0.022 0.022 0.024 0.019 0.017 0.017	0.007 0.008 0.008 0.008	0.050 0.033 0.015 0.015 0.015 0.015	0.028 0.019 0.016	0.018 0.024 0.024	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.006 0.008 0.005	0.012
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ĸ	4.45 1.94	22 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.29	21.000.00 61.000.00 61.000.00 61.000.00	0.54 0.26 0.37	0.30 0.64 0.24	0.20 0.39 0.39 0.32 0.20 0.20	400 400	0.78
<b>KO3</b>	404	4 6 6 7 6 4 6 6 7 6 7 6 7 6 7 6 7 6 7 6	-0000 8000 4000 4000 4000 4000 4000	- w w w o w w 4	24.80 0.110 0.80	0 4 4 6 2 7 7 0 2 8 8 8 2 8 8 8		0 0 0 0 0 0 0 0 0 0 0 0	0 0 8 6
SD4	19.67	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	7.00 8.00 9.00 9.00 9.00 9.00 9.00	87.77 88.59 89.59 9.66 9.56 2.20 2.20	23 9 . 2 . 9 9 . 2 1 3 0	12.06 14.28 11.56 15.31	7.50 8 0 5 7 6 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6 7 6	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	8
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<b>3</b>	·	សេខាមេក ឯ ឯកង ឧបកឧប	ស ខា ខា ខា ខា ខា ខា ខា ខា ភា ខា ភា	<b>- Խ</b> Ա.Ծ. Ռ	60 60 - CO		8.48.86 1.7.48 1.00.88	4 6 0 4 0 4	9
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	4	24444	000	4004	000000	0.0270 0.0454 0.0690 0.0165	0.001 0.005 0.005 0.007 0.003	0.0000	0.70 0.70 0.77 0.93 7.03	2.55 0.90 1.68 0.1.68 0.02 0.02	00000 00000 00000	00000 1100000 110000000000000000000000	00000	7.00.00.00.00.00.00.00.00.00.00.00.00.00	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	4000000 4040	0000 0000 0000 0000 0000	64787 6406 6406 6406 6406 6406 6406 6406 640	ൻ സ ന ഒ ഒ ല ധ വ — 4 വ 4 ധ ന ര ല ല പ	6446 555 555 555 555 555	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
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	123	75 76 2 77 3	000	. 327 0 0 0 0	00000	0.0029 0.0035 0.0079	0.002	0.00 0.00 0.00 0.00	0.0 0.0 0.0 0.0 0.0 0.0	1.30 0.79 0.89 0.57	.014 0 .017 0 .023 0	0100.	0000 - 800	0.18 0.28 0.28	6.04 6.04 7.05 7.05 7.05	0 80 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.00 2.00 4.00 6.00 6.00	* 4 8 0 8 0 0 4 7 4 0	0 0 0 0 6 4 - 6 0 0 0 0	e e o o o o	0 0 0 4 4 0 7 0
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, (p:	<b>2</b>	0.015	0.051	0.073	0.009 0.012 0.084 0.008	- N - O	4000000000	0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.0035 0.0013 0.0013 0.0000 0.0000	000000
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_	e a	1.23	0.71	0.36	0.88 0.83 0.75	0.33 0.50 0.50 0.50	44000000000000000000000000000000000000	24.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1	27.27.1.27.27.1.238.1.2.1.2.1.2.1.2.1.2.1.2.1.2.1.2.1.2.1.	0.49 0.83 0.57 0.60 0.69
ABLE 10	m	0.88	0.08	0.40	0 0 0 0 4 4 6 6 6 7 4 6 6	7.47 0.51 0.18 0.34 1.0		1.40 0.77 0.70 0.70 0.79 0.67	20000000000000000000000000000000000000	00000 00000 00000 00000
Ţ	3	0.18	0.08	0.93	0.25	1.59 9.57 5.39 7.33 2.72	0.000000000000000000000000000000000000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000000000000000000000000000000000000	000000
	S,	0.002	0.00.0	0.00.0	0000	0.002 0.003 0.003 0.001	000000000000000000000000000000000000000	0.000 0.000 0.000 0.000 0.000 0.000	000000000000000000000000000000000000000	0.000 0.000 0.000 0.000 0.000 0.000
	00	0.0016	.0043	.0010	.0023	.0045 .0039 .0039		.0033 .0033 .0036 .0036 .0035	.0028 .0028 .0044 .0027 .0028 .0026	.0033 .0028 .0029 .0029
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	TOWN	۵	2	۵	۵	ELD	¥ O	<b>E</b>	X O	E O
	5	ENFIELD	ENFIEL	ENFIELD	enfield	FAIRFIELD	Greenwich	Greenwich	greenwich	Greenwich
		m	m	ш	ក់ា	44	<b>ම</b> 60	<b>.</b>	<u> </u>	<b>.</b>

TABLE 10 (Continued)

NEOF	greenwich	Greenwich	Greenwich	GROTON	GROTON	НАООАМ	HARTFORD	HARTFORD
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A		000	***		000	000	0000	000
8	0.0000		0.0001	0.0000 0.0002 0.0001	0.0000 0.0000 0.0000	0.0000 4 0.0000 7 0.0000 2 0.0000	00000	4 w w
8	0.0038 0.0028 0.0037 0.0043 0.0022	0.0023 0.0031 0.0021 0.0028 0.0019	0.0033	0.0019 0.0022 0.0016 0.0016	0.0024	0.0016	0.0020	0.0027 0.0036 0.0036 0.0025 0.0027 0.0027 0.0027
S	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0000000 000000000000000000000000000000	0.007	0.0010 0.0023 0.004 0.007	0.006 0.007 0.003	0.003	0.003	0.000
5	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.22	4.00 6.00 6.00 6.00 6.00 6.00 6.00	0.10 0.10 0.04 0.04	0 0 0 0 0 0 0 0 0 0 0 0 0	0.22 0.11 0.05 0.26	14.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
쁘	0.43 0.43 0.25 0.72	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.78	2 - 0 0 0 0 4 2 4 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	0000 0000 0000 0000	00.28 0.39 0.39 0.44	0.78 0.79 0.83	7
9	0.83 0.83 0.65 0.65	1.7.1 1.46 1.42 1.11 1.11 1.10 0.85 0.85 0.77	1.11	1.20 0.81 0.97 0.97	0.61 0.47 0.56 0.48	0.9 44.0 44.0 64.4 64.4	0.94 1.01 0.89 0.87	4.0.00.4.c. 4.0.00.4.c.
NA NA	0.0024 0.0015 0.0015 0.0010 0.010	00.00 00	0.022	0.108 0.037 0.012 0.012 0.012	0.015 0.017 0.030 0.022	0.000	0.016 0.017 0.018	00.0000 8800000000000000000000000000000
M	0.055 0.017 0.018 0.011	0.000 0.001 0.000 0.000 0.000 0.000 0.000 0.000	0.019	0.088 0.058 0.019 0.018	0.019 0.015 0.025 0.016	0.006 0.009 0.005 0.007	0.012 0.013 0.013	00.000 00.000 00.000 00.000 00.000 00.000 00.000
>	0.00 0.00 0.00 0.03	000000000000000000000000000000000000000	0.0	6.000 8.000 8.000 8.000	0000	00000	0000 0000 4000	000000000000000000000000000000000000000
Z,	0.00 0.23 0.23 0.24 0.21	0.22 0.22 0.30 0.12 0.12 0.12	1.06	20.00 8.00 8.20 8.27 8.27	0000	00000 127 10000 10000	0000 2000 2000	-00000000 0444-004
E 03	0	- 2	1.80 4.04	04.00 K -	ຕະວ ສ.ຊ.ຕ. ວ ຊ.ຕ.∸ -	0.08 2.74 1.72 1.87 1.87	6.00 6.00 6.00 6.00 6.00 6.00 6.00 6.00	$\begin{array}{c} \bullet & \bullet & \bullet & \bullet & \bullet & \bullet & \bullet \\ \bullet & \bullet & \bullet &$
S04	7.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00	8.36 9.09 9.09 12.16 10.45 9.03	18.0 9.03	200 0 1 4 0 8 1 6 8 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.00 0.00 0.00 0.00 0.00 0.00	10.4 12.77 12.19 1.19 1.19	8.89 14.00 17.00	0.0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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8	0.0034 0.0040 0.0018 0.0023	0.0046 0.0031 0.0024	0.00	0.0019	000000000000000000000000000000000000000	0.0019 0.0015 0.0015 0.0015 0.0013	0.0009 0.0032 0.0044 0.0016	0.0029 0.0036 0.0031	0.0070
2	4 0.005 0 0.004 8 0.003 8 0.003	6 0.029 4 0.004 6 0.002	6 0.005 9 0.008 9 0.005	9 0.005 8 0.004 3 0.003	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.000000000000000000000000000000000000	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.001	0.007
3	0.63 0.26 0.21 0.17	0000	0.08 0.15 0.15	0.26 0.27 0.47	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.37 0.37 0.25 0.00 0.00 0.00 0.00	0.0000000000000000000000000000000000000	20000 40000 40000 74000	90.0
ir in	0.80 0.73 0.61 0.74	3.53 0.75 0.75	0 12.2 12.2 12.8	0 0.5 0 1.4 0 1.8	-0000000 00400000 048080044	00000000 0000000 00400404 740077		0000-	0.68
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Z	0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.043 0.013 0.012	0.018 0.025 0.026	0.012	0.038 0.011 0.0010 0.007 0.009 0.009	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.027 0.016 0.016 0.012 0.007	00000	0.130
Z	0.010 0.000 0.000 710	0.055 0.011 0.013	0.021 0.013 0.017	0.009	0.0030 0.0030 0.0007 0.007	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	.000000	00.00 47.00.00 7.00.00	0.082
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	4	0.72		0 0 0 0 4 8 0 0 0			0 4.0 7.0 7.0 0	
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) 2	Ω.	<ul><li>₩₩₩₩₩₩₩</li><li>₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩₩</li></ul>	0	722 720 720 740 740 750 760 760	73 0.74 0.79 0.50 0.50 0.50 0.50 0.50 0.50 0.50 0.5	9 4 3 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2888888 244888888 244888888888888888888	15 36 0.
Contin	E	71 0.0 662 0.0 336 0.0 23 0.0 93 0.0 14 0.0	322 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	83 0.0 30 0.0 00 0.0 00 0.0 05 0.0 74 0.0	90 0.0 96 0.0 61 0.0 81 0.0	28 0.0 81 0.0 83 0.0 34 0.0	54 0.0 69 0.0 21 0.0 85 0.0 99 0.0 07 0.0	47 0.0 39 0.0
uned)	Z	22 23 36 0 0 1 2 2 2 3 3 0 0 0 0 2 2 2 3 0 0 0 0 0 0 0	272 334 0.00 0.00 0.00	2222 2222 2222 2322 2422 2422 2422 2422	22 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8411119 841119 90000 90000	22 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	000
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	150	000000000000000000000000000000000000000	5 2 0 0 0 0 0 0 2 0 0 0 0 0	02777700 03777700 03777700	0000000 2744000	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	7 7 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	<b>6</b> 8

TABLE 10 (Continued)

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MG3	0.50	O - 4 6 4 6 4 4 4 6 6 6 6 6 6 6 6 6 6 6 6			0-04-0040 000000-00 000000-00	30 53 5 30 30 55 5	0 - 5 - 8 0 - 5 - 8
Z	0.38	1.000000000000000000000000000000000000	0.50 0.23 0.10 0.39 0.39 1.00 4.10	000000	0.4.0.0.0.0.0 0.4.0.4.0.0.0.0 0.4.0.0.0.0	2.45 0.24 1.00 1.00 1.00 1.00 1.00	00.20
>	0.03		0.0000 0.0000 0.00000 0.00000	00000 0000 0000 0000	00000000 0000000 000000000000000000000	00000 0000 1000 0000 0000	0000
Z	0.013	0.058 0.024 0.021 0.019 0.013 0.013	0.078 0.032 0.032 0.024 0.024 0.021 0.021	0.033 0.020 0.020 0.013 0.018	0.055 0.026 0.030 0.014 0.013 0.013	0.034 0.031 0.031 0.011	0.035 0.035 0.032 0.022
M	0.017	0.0037 0.0000 0.0000 0.0013 0.0013 0.0013	00000000000000000000000000000000000000	0.053 0.017 0.009 0.010	0.029 0.024 0.027 0.018 0.020 0.029 0.029	0.057 0.030 0.023 0.015 0.017	0.058 0.031 0.023
en o	0.23	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0 0 0 8 0 2 0 0 8 0 2 0 0 8 0 0 0 0 8 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		2 - 8 - 6 2 - 8 0 4 6 6 6 6
r m	0.32		00000000000000000000000000000000000000	-00000 0446400 887799-0	0000000 0000000 0000000000000000000000	0 0 1 1 0 0 1 1 0 0 0 1 1 0 0 0 0 0 0 0	2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4
CC	0.14	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0000000	000000000000000000000000000000000000000	0.0000 0.0000 4.00000	00000
S.	0.003	0.0007 0.0007 0.0007 0.0009 0.0009 0.0009	00000 00000 00000 00000 00000 00000	0.0011 0.0011 0.0002 0.0002 0.0006	0.000000000000000000000000000000000000	0.000 0.0015 0.0008 0.005 0.005	0.0052 0.007 0.007 0.005
8	0.0019	0.0033 0.0036 0.0036 0.0030 0.0033 0.0033	0.00028 0.00038 0.00038 0.00038 0.00038	0.0024 0.0027 0.0033 0.0030	0.0048 0.0058 0.0059 0.0046 0.0036 0.0047	0.0028 0.0041 0.0032 0.0023	0.00121 0.0044 0.0034 0.0034
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TOWN	MIDDLETOWN	MILFORD	MILFORD	MILFORD	NAUGATUCK	NEW BRITAIN	NEW BRITAIN

TABLE 10 (Continued)

Š	58		0446-00	4 n n n 4 n 0 u - 0 u 4	K 6 B Y	0 0 0 1 K	2 8 9 6 8 7 6 8 8 8 0 40 6 7 5 6 9 9	2222
BENZ	4.72	0 + 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	6.63	ඩ ය ග උ ග ම	0 m 4 m 4 m w 0 m 4 m 4 m w 0 m 7 0 0 m w 0 m 8 m w w	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
¥	8 8 8 8 8		00000000000000000000000000000000000000	4688646 646646 64668	0000 	00000 00040 40040	$4 \sim 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 $	0000 0407 67-06
2	7.24	8 6 4 8 4 6 7 4 4 0 10 4 0	9 F 6 6 M M M	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8			60 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	m - -
¥.	00.0	00.37	900	.00 .20 .00	9998	000 000 000	2.00 2.00 8.00 8.00 8.00 8.00	8
S04	9.07	0 8 9 8 9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.00 P B C C C C C C C C C C C C C C C C C C	9 8 9 7 9 4 9 8 9 7 9 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	11.51 14.40 14.50 15.00	9.57 9.47 7.57 7.58	15.60 9.68 9.98 6.84 13.77 10.63	0.7.0 0.4.0 0.4.0
<b>E</b>	2.26 6.12	- 0 4 4 4 4 0 0 0 0 0 0 0 0 0 0 0 0	000000000000000000000000000000000000000	0 0 0 0 4 ± 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	2.66 2.66 2.66 2.66	6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6		0.0000 0.0000 0.0000 0.0000
R	0.21	0.0000000000000000000000000000000000000	0.30 0.30 0.1.0 0.1.0 71.0	0.38 0.42 0.15 1.10 0.20	0000	0.29 0.22 0.15 0.15	0.36 0.26 0.26 0.25 0.27 0.27 0.20	0000 2.26 3.36 3.36
>	0.02	000000 -00000 0004000		00000 	0000 0000 1000	0.33 0.07 111 0.07	00000000000000000000000000000000000000	0000 00 647
Z	0.013	0.052 0.019 0.014 0.0014 0.0011 0.0011	0.070 0.022 0.018 0.020 0.016	0.057 0.017 0.015 0.011	0.009 0.013 0.009	0.039 0.024 0.027 0.025	0.039 0.039 0.047 0.017 0.026 0.016 0.015	0.024 0.016 0.020
Z	0.020	00.00 0.00 0.00 0.00 0.00 0.00 0.00 0.	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0.0000	0.017 0.019 0.020	0.018 0.020 0.025 0.025	0.023 0.023 0.023 0.023 0.016 0.019	0.00 410.00 10.00
60	1.05	22.158 22.158 24.173 1.145 1.146 1.156	00.1.00 00.00 00.00 00.00 00.00 00.00	2.00.8.1.0.2.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0	1.24 1.03 0.96	2	0.00 4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.85 0.85 0.71
ii.	1.92	7	6000000 - 70 70 70 70 70 70 70 70 70 70 70 70 70	600000 60000 74447 60000	0.84 0.71 0.83 0.72	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6.00 6.50 6.60 7.00 7.00 7.00 7.00 7.00 7.00 7.0
3	0.05	0000000 0000000 44400040	0000000 004444	00000 00000 00000 00000 00000	0.12 0.06 0.08 0.11	000000000000000000000000000000000000000	000000000000000000000000000000000000000	0.20
S.	0.003	0.008 0.008 0.003 0.002 0.003	0.001 0.000 0.000 0.000 0.000 0.000 0.000	0.003 0.003 0.003 0.003	0.008 0.006 0.009	0.000 0.000 0.002 0.002	0.005 0.009 0.009 0.005 0.007 0.007	00000
00	0.0021	0.0028 0.0028 0.0038 0.0031 0.0053 0.0053	0.0052 0.0020 0.0039 0.0036 0.0051	0.0069 0.0028 0.0028 0.0023	0.0023 0.0018 0.0015 0.0014	0.0044 0.0030 0.0038 0.0029	0.0096 0.0038 0.0050 0.0017 0.0030 0.0030 0.0020	0.0053 0.0057 0.0025 0.0031
8	00000.	000000	0.0001 0.0001 0.00001	0.0001 0.0000 0.0000	0.0000	0.0000	0000000	0.00 0.00 0.000 0.000
AL	0.720	00.00			0.34	0.72	0.00 4.0.0 0.00 0.00	
SITE YR #S	002 75 29 76 10	003 70 26 71 26 72 28 73 28 74 29 75 29 77 15	004 70 26 71 26 72 30 73 30 74 29 75 30 76 7	005 70 26 71 25 72 29 73 29 74 30 75 4	123 75 6 76 30 77 29 78 31	001 71 4 72 9 75 26 77 76 28 77 19	002 70 21 72 24 73 26 74 28 75 16 76 30 77 28	003 71 11 72 28 73 31 74 30
TOWN	new Britain	NEW BRITAIN	nee britair	NEW BRITAIN	NEW BRITAIR	NEW HAVEN	NEW TAVER	NEW MAVEN

S	n 4 0 0	£ 0 0 4 7 0 0 4 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	80000	F	8 N 4 4 8 N 4 4	0 0 0 0 0 0 1 L	700000000000000000000000000000000000000	8-80946-8
BENZ		0 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		•	6.4. 6.1. 8.1.	n4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1000-4	446446 4664 4664 4664 4664
Ŧ	8 9 9 9 9	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		დ დ 4 თ დ დ	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4,4460-0	0,50,000,000	4000000000-4
<b>Z</b>	7.05	ង ខា ង ៤	• •	ക മ ല പ ര സ	4 7 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		यं ज क व व	00049
Ť	0 0 0 0 0 0 0 0	0.29 0.30 6.30	0.20	0.0	00.00	(7) (7)	4.4.400	9 9 9 9
S04	12.52	10.00 9.36 4.68 10.47 8.23	10.00 8.60 7.02 7.91	9.17	7.35 9.44 10.50		เท่าหน่นเลอกาเม	ဝစ္စက္စက္မွစ္တန
80 80 80	2.44	3.83 2.27 7.77 6.98 1.89 83	6 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6 - 6	ຄ. ຜ ຜູ້ ໝໍ ດີ ໝໍ				
ĸ	0.21	0.34 0.67 0.25 0.16 0.16	0.00 0.20 0.24 0.24	0.22	0.01	00.00 00.00 00.00 00.00 00.00 00.00	00000000000000000000000000000000000000	
>	0.00	000000	00000	0.06	0000	00000 00000 00000	0-00000	00000000 
Z	0.010	0.030 0.034 0.017 0.018 0.013	0.030 0.037 0.015 0.023	0.018	0.005 0.005 0.005	0.057 0.011 0.016 0.015 0.009	00.000 00.0015 00.0012 00.0000 00000 00000	00000000000000000000000000000000000000
Ν×	0.014	0.018 0.016 0.017 0.013	0.00 0.00 0.00 0.00 4	0.027	0.013 0.013 0.015 4	0.0063 0.0018 0.0013 0.0013	0.055 0.024 0.024 0.020 0.020	0000000
9 B	0.75	2.1.26 1.26 0.93 0.86 0.83	2.90 1.06 1.15 1.01	6.53	0.27 0.28 0.22 0.24	0.044.00.00.00.00.00.00.00.00.00.00.00.0	2.26 1.32 1.30 1.40 1.19 1.19 1.77	60 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
ir.	0.75	1.08 0.79 0.95 0.95 0.83	00000 0000 0000 0000 0000	1.19	0.50 0.57 0.52 0.52	19.0 10.0 10.0 10.0 10.0 10.0 10.0	40.00.00.00.00.00.00.00.00.00.00.00.00.0	0.000000000000000000000000000000000000
3	0.09	0.35 0.122 0.00 0.23 0.33	0.21 0.028 0.12 0.13	0.04	0.17 0.07 0.07	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
S	0.004	0.004 0.007 0.005 0.005 0.003	0.001	0.010	0.004 0.002 0.001 0.005	0.000 0.000 0.000 0.000 0.000 0.000	00000000000000000000000000000000000000	0.005 0.005 0.005 0.005 0.005 0.005
8	0.0029	0.0098 0.0052 0.0033 0.0029 0.0026	0.0034 0.0038 0.0019 0.0021	0.0018	0.0010 0.0015 0.0009 0.0007	0.0043 0.0027 0.0036 0.0027 0.0039	00000000000000000000000000000000000000	0.0068 0.0015 0.0016 0.00018 0.00018 0.00018
9E	.0000	00000	00000	0000	0000	00000	0000000	000000000000000000000000000000000000000
AL	0.39	0.32	0000	0.64 0	00.28	00000		00.44 00.44 00.05
₩ W	28	- 12 12 12 13 - 12 12 12 13 13 - 12 13 13 13 13 13 13 13 13 13 13 13 13 13	22225	30	0000	4000000	000000000000000000000000000000000000000	4 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
<b>×</b>	75	71 73 74 75	722 732 75 75 75 75 75 75 75 75 75 75 75 75 75	77 78	74 75 76	07 12 12 14 15 16 17	0 - 0 0 4 0 0 0 0	0-0040000
SITE	003	000	6) 0 0	123	00	00	80 00 00	0
NMOL	NEW HAVEN	NEW HAVEN	NEW MAVEN	NEW HAVEN	NORTH CANALH	NORWALK	NORWALK	NORWICH

7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	O (Continued) PB MN NI V Z 2.29 0.015 0.021 0.04 0.148 0.017 0.012 0.044 0.1199 0.016 0.004 0.011 0.049 0.011 0.012 0.005 0.011 0.019 0.015 0.019 0.01	0 (Continued)  PB MN NI V ZN NG3 S  2.29 0.015 0.021 0.04 0.28 0.99 2  1.48 0.017 0.012 0.04 0.29 1.07 9  1.49 0.017 0.016 0.004 0.01 1.25 1.07 9  1.29 0.016 0.004 0.01 0.04 1.25 1.07 9  1.29 0.020 0.006 0.01 0.04 1.25 1.07 9  0.63 0.009 0.008 0.04 0.28 0.94 0  0.63 0.009 0.008 0.04 0.28 0.94 0  0.7 0.016 0.012 0.012 0.02 3.18 8  0.87 0.022 0.013 0.02 0.03 0.23 1.34 12  0.53 0.012 0.012 0.012 0.02 3.18 8  0.53 0.014 0.015 0.015 0.02 0.04 1.07 2.87 10  0.53 0.020 0.011 0.008 0.03 0.29 3.18 10  0.54 0.009 0.007 0.01 0.07 2.87 10  1.30 0.020 0.031 0.13 0.40 2.75 7  2.52 0.034 0.044 0.27 0.25 6.56 17  1.30 0.026 0.021 0.012 0.03 0.27 1.61 7  1.83 0.026 0.021 0.012 0.03 0.27 1.61 7  1.83 0.026 0.021 0.015 0.03 0.27 1.61 7  1.90 0.014 0.015 0.10 0.30 2.09 8  1.71 0.019 0.026 0.13 0.29 3.36 19  1.71 0.019 0.026 0.13 0.29 3.36 19  1.71 0.019 0.026 0.13 0.29 3.36 19	O (Continued)  PB MN NI V ZN NG3 S04 NH  2.29 0.015 0.021 0.04 0.28 0.99 2.61  1.48 0.017 0.012 0.04 0.29 1.07 9.79 0.38  1.19 0.010 0.006 0.01 0.014 2.75 11.74 0.11  1.29 0.010 0.006 0.01 0.07 2.95 7.62 0.09  0.91 0.017 0.006 0.01 0.07 2.95 7.62 0.09  0.92 0.009 0.008 0.04 0.28 0.94 0.98  0.93 0.015 0.0012 0.05 0.21 2.18 5.70  0.94 0.055 0.018 0.08 0.03 0.28 0.00 11.95 0.28  0.95 0.010 0.008 0.03 0.28 0.00 11.95 0.29  0.95 0.010 0.009 0.012 0.05 0.21 2.18 5.70  0.95 0.010 0.009 0.012 0.05 0.21 2.18 5.70  0.95 0.010 0.009 0.012 0.05 0.21 2.18 5.70  0.95 0.010 0.009 0.012 0.05 0.21 2.18 5.70  0.97 0.036 0.045 0.03 0.28 0.00 11.95 0.28  0.98 0.015 0.016 0.009 0.00 0.00 0.00 0.00 0.00 0.00 0.	0 (Continued)  PB MN NI V ZN NU3 SO4 NH4 NA 2.29 0.015 0.021 D.04 0.28 0.99 2.61 1.48 0.017 0.012 D.04 0.29 1.07 9.79 0.35 5.3 1.48 0.017 0.012 D.04 0.29 1.07 9.79 0.35 5.3 1.48 0.017 0.006 0.004 0.01 0.19 1.25 7.89 0.25 5.9 1.39 0.016 0.004 0.01 0.14 2.75 11.74 0.13 4.99 1.29 0.020 0.006 0.01 0.04 3.36 9.97 0.06 5.90 0.91 0.017 0.006 0.01 0.04 3.36 9.97 0.06 5.90 0.93 0.013 0.02 0.019 0.03 0.29 3.18 8.60 0.94 0.055 0.018 0.04 0.29 3.18 8.60 0.95 0.013 0.015 0.02 3.18 8.60 0.09 0.015 0.015 0.02 3.18 8.60 0.09 0.010 0.00 0.00 0.03 0.23 1.10 7.73 0.17 3.2 0.23 0.011 0.008 0.03 0.23 1.10 7.73 0.17 3.2 0.29 0.020 0.011 0.00 0.00 0.00 0.00 0.00 0.	0. (Continued)  PB MN NI V ZN NG3 SO4 MH4 NA PH B L48 0.015 0.021 D.04 0.28 0.99 2.61  1.48 0.017 0.012 D.04 0.28 0.99 2.61  1.48 0.017 0.012 D.04 0.29 1.07 9.79 0.30 5.32 6.16  1.19 0.010 0.006 D.01 0.91 1.26 7.99 0.26 6.90 8.31  1.29 0.016 0.004 D.01 0.91 1.26 7.95 0.06 5.96 9.33  0.91 0.017 0.006 D.01 0.91 1.26 7.95 0.06 5.96 9.33  0.91 0.017 0.006 D.01 0.01 0.29 3.18 8.60  0.93 0.015 0.008 0.04 0.28 0.94 0.98 6.60  0.93 0.015 0.021 D.11 0.29 3.18 8.60  0.94 0.055 0.018 D.08 0.04 0.28 0.94 0.98 6.60  0.95 0.015 0.009 0.00 0.04 0.28 0.94 0.98 6.60  0.95 0.015 0.009 0.00 0.00 0.00 0.00 0.00 0.00 0.
00000 00000 0 000000 0 00000 0 00000 0 0	V 00000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	NG N	NI V ZN NG3 SC4 NH4  221	NI V ZN NG3 SG4 NH4 NA NG4 0.221 D.04 0.29 1.07 9.79 0.30 5.30 0.04 0.29 1.07 9.79 0.30 5.30 0.04 0.09 1.07 9.79 0.25 6.99 0.001 0.01 1.26 7.89 0.25 6.99 0.006 0.01 0.07 2.95 7.62 0.01 8.39 0.25 6.99 0.006 0.01 0.07 2.95 7.62 0.01 8.39 0.006 0.01 0.07 2.95 7.62 0.01 8.39 0.006 0.01 0.07 2.95 7.62 0.01 8.30 0.008 0.03 0.28 0.94 0.98 0.98 0.04 0.28 0.94 0.98 0.00 0.03 0.23 1.34 12.56 0.00 0.03 0.23 1.10 7.71 14.95 0.20 4.7 3.50 0.03 0.03 0.03 0.03 0.03 0.03 0.00 0.07 2.87 10.98 0.00 0.03 0.11 0.70 9.76 0.27 3.50 0.00 0.00 0.00 0.00 0.00 0.00 0.00	121 D. 04 O. 28 O. 99 2. 61 O. 04. 0. 25 6. 96 6. 97 0
	441111 4 81188 8 200000 120000 14000 110000 110000 110000 110000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 110000 110000 110000 110000 110000 110000 110000 110000 1100000 1100000 1100000 1100000 1100000 1100000 1100000 1100000 11000000	A C C C C C C C C C C C C C C C C C C C	NG3 SO4 NH4  104 0.28 0.99 2.61  104 0.28 0.99 2.61  107 0.99 2.61  108 0.99 2.61  109 0.99 2.61  109 0.99 2.61  100 0.90 2.90  100 0.90 2.90	V ZN NG3 SO4 NH4 NA NG4 0.28 0.99 2.61 0.04 0.29 1.07 9.79 0.30 55.3 0.01 0.09 1.07 9.79 0.30 55.3 0.01 0.09 1.07 9.79 0.02 0.01 0.09 1.02 0.01 0.09 1.02 0.01 0.09 1.02 0.01 0.09 1.02 0.00 0.00 0.00 0.00 0.00 0.00 0.00	V ZN NO3 SO4 NH4 NA PH B 104 0.28 0.99 2.61 0.99 0.25 0.30 5.32 6.16 6.48 5.00 0.91 1.26 7.89 0.25 6.90 8.58 3.00 0.01 0.07 9.79 0.25 6.90 8.58 3.00 0.00 3.36 9.97 0.06 5.96 9.33 2.00 0.07 2.95 7.62 0.01 8.30 8.58 3.00 0.00 0.07 2.95 7.62 0.01 8.30 8.51 2.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0

TABLE 10 (Continued)

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BENZ	3.66 3.73	2.3	4.0.0.0.0.0 8.0.0.0.0.0 8.0.0.0.0.0 8.0.0.0.0	5.73 1.98	66.44 67.58 66.68	44460 00-460 00-60-60	0.04.0.4 8.40.0.4 8.0.4.0.0.1.	ଜ ଜ ଜ ଜ ଜ ଜ	9.49	40
E.	6.37 5.37	9.31 9.05	67.6688888 4.27.7.00 4.27.7.00 7.20.00 7.20.00 7.20.00 7.20.00	9.37	8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6.38 6.38 7.16 7.16 7.47	6.00 6.00 7.00 7.00 7.00 7.00 7.00 7.00	<b>૱</b> @@@ o ro co co ro co co co ro co co co ro co co ro co co ro co	6.40	0 W
Z		8 8 8 0 8 0	8.7.4.8.5 8.0.0 1.	·	0.7.00 7.7.00 7.00 7.00 7.00 7.00 7.00	6) 4 60 4 4 60	ພ ພ ພ ບ ພ ບ	8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8		\$
N N	0.17	0.00	0.000 0.000 1.000 1.000 1.000 1.000		00000 88400 88400	9.00 4.00	0.32	0000		0.23
<b>S04</b>	13.28 9.42 14.55	10.47 11.37 8.88	9.10 9.10 8.84 8.23 8.23 11.00 14.67 8.97	13.00 11.01 10.61	5.73 10.89 16.44 7.09 40.01	12.01 8.42 4.03 8.18 6.18	12.78 10.99 5.22 9.86 1.90	7.92 12.07 10.02 6.76	5.40	4.78 3.78
MO3	4 - 5 20 20 30 30 30 30 30 30 30 30 30 30 30 30 30	2.97 3.35 2.80	.01-12-12-12-12-12-12-12-12-12-12-12-12-12	1.03	2.70 3.76 3.76	87.5.0 87.00 1.00 1.00 1.00 1.00 1.00	0.00 2 0.00 4 8 7 0.00 8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	- 0 0 0 0 - 0 1 0 4 0 1 0	<i>ц</i> 2	0.85 0.87
z	0.20 0.40 0.43	0.24	00000000000000000000000000000000000000	1.80 0.52 0.43	0.30 0.24 0.23 0.13 0.13	3.09 2.17 1.06 0.61 0.59	3.25 0.20 0.13 0.22 0.36	 4	1.02	0.18
>	000	0.00	00000000 20000000 18048888	0.28 0.38	000000 00000 178244	0000 000 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	0 1 2 0 0 0 0 0 0 0 0 0	0000	0.10	0.0
Z	0.024 0.016 0.051	0.012	00000000000000000000000000000000000000	0.066 0.082 0.047	0.008 0.027 0.022 0.014 0.015	0.059 0.034 0.009 0.009	0.068 0.026 0.019 0.017	0.008 0.009 0.007 0.008	0.010	0.006
Z	0.024 0.013 0.048	0.014	00000000000000000000000000000000000000	0.077 0.016 0.020	0.00 0.00 0.00 0.00 7.00 7.00	0.063 0.023 0.0017 0.008 0.008	0.061 0.036 0.022 0.016 0.018	0.012 0.047 0.030 0.028	0.015	0.004
Ġ	1.96	1.04 0.86	63 2 4 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	2.40 1.06	0.12.1 1.20 1.21 0.98	0.96 0.83 1.21 0.71 0.80	2.1.1.65 2.43 2.43 2.43	0.08 0.98 0.98	9.81	0.21
ill Ill	0.89 0.71 2.51	0.67 1.50 0.76	00000000 8447700040 88677700040	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	00000 00000 00000 00000	00000 00000 00000 00000	10000 2000 1000 1000 1000 1000 1000 100	0	0.42	00 04 00
3	0.24	0.00	0 + 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.44 0.34	0.00 0.00 0.41 0.00 0.00 0.00 0.00 0.00	0.00 0.17 0.32 0.46 0.46	000000	0.26 0.13 0.12 0.25	0.09	0.40
S B	0.013 0.012 0.011	0.003 0.048 0.002	0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.0000 0.00000	0.010	0.003 0.006 0.005 0.005 0.010	0.008 0.0012 0.004 0.007 0.003	000000000000000000000000000000000000000	0.000 0.000 0.000 0.000 0.000	0.001	0.005
8	0.0065 0.0032 0.0048	0.0039	0.00412 0.0033 0.0033 0.0046 0.0042 0.0022 0.0022	0.0060 0.0039 0.0045	0.0022 0.0037 0.0027 0.0048 0.0026	0.0031 0.0038 0.0052 0.0025 0.0025	0.0020 0.0030 0.0021 0.0021	0.0019 0.0026 0.0007 0.0010	0.0005	0.0008
8E	0000	0000	000000	0000	000000	0.0000	0000	0000		.0000
AL	000	0.20	00.22	0			0000	0000		00
S *	25°	30 31	0000-0000	rv es ,	-00000 00000 00000	4 4 4 4 4 4 4 4	447000	- 00 kg	G	24 20 4 70
m X	73	3 76 77 78	07.000.000.000.000.000.000.000.000.000.	72 72	2 4 4 7 7 8 7 8	0 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	1 7 7 8 7 8 7 8 7	3 75 7 7 8 7 8 7 8	6 6	73
SITE	0 20	_ G	0	000	90 0	0	0	«	00	00
T N N	STAMFORD	STAMFORD	STRATFORD	STRATFORD	STRATFORD	THOMASTON	107710710NG10NG10NG10NG10NG10NG10NG10NG10NG10NG	Torrington	VERNON	VOLUNTOWN

									TABLE	3) 01	Continue	ed)									
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CONNECTICUT DEPARTMENT OF ENVIROMENTAL PROTECTION

CONNECTICUT DEPARTMENT OF EN	ENVIROMENTAL	PROTECTION	7						AIR COMP	COMPLIANCE EN	engineering
POLLUTANT TOTAL SUSPENDED PA	TI PARTICULATES	EN HIGHES	7 24 HR A	AVG TSP DAY	S 1978	WITH WET.	DATA				
				•					MICROGRAMS	S PER CUBIC	IC METER
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CONNECTICUT DEPARTMENT OF	ENVIROMENTAL	PROTECTIO	z		•				ATR COMP	COMPLIANCE EN	engineering
POLLUTANTTOTAL SUSPENDED	PARTICULAT	TEN HIGHEST		24 HR AVG TSP DAYS 1978		WITH MET.	DATA	units :	eicrograms	S PER CUBIC	IC METER
TOWN NAME	SITE SAMPLES	·	Ø	m	ব	ហ	ω	7	60	Ø	6
METEOROLOGICAL SITE BRIDGEPORT CONN		. С	a 4 0 4	0.1	4 8 5 5	0 m m	8 2.6	84.4	425	12°5°	9
TEOROLOGICAL RADLEY FIELD	DIR VEL SPD		3.3 3.3 5.0 665	6.7 7.0 7.0 9.954	0.888 3.14 3.14	0.4 20.0 0.8 3.6 0.0 2.0	0.770 310 3.6 8.2 444	6 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 2 2 4 4 6 6 6 6 7 7 8 7 8 7 8 7 8 7 8 7 8 7 8 8 7 8	>
METEOROLOGICAL SI'	SITE DIR (DEG) MASS. VEL (MPH) SPD (MPH) RATIO	. 0	$\phi \cdot \cdot \omega$	1000	9 9 9 9	សលល់	8 - 4 B	8 - n &	4	7.40	9 6 6 9
BRIDGEPORT METEOROLOGICAL SITI	m = G		# N N + N 0	VOV	$\omega$ $\omega$ $\omega$ $\cdot$ $\cdot$ $\omega$	12 14 14 14 14 14 14 14 14 14 14 14 14 14	2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	15 718 28 28 7.	±888°×8	200000	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~
METEOROLOGICAL SITE BRIDGEPORT CONN. METEOROLOGICAL SITE BRADLEY FIELD CONN.			2.20 2.20 2.00 3.00 6.20 7.20		280.0 280.0 30.55.0 300.0 9.0	0 1220 2220 1.0 10 1.0 106 2.1 106	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	6. 25 6. 25 6. 25 7. 29 7. 7. 9	0 280 7.20 310 5.20	6 224 422.4 422.4 700.0 700.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
METEOROLOGICAL SITI WORCESTER MASS	RATIO TE DIR (DEG) SS. VEL (MPH) SPD (MPH) RATIO		90 0	-0	∞ ⊷ • • • • • • • • • • • • • • • • • •	0.507 360 2.1 7.6	0.954 210 10.2 10.5 875	$m \circ \cdots m$	· · · · · · · · · · · · · · · · · · ·	~ m · · m	· · · · · · · · · · · · · · · · · · ·
BRISTOL METEOROLOGICAL SI NEWARK N.	1 .59 DATE ITE DIR (DEG) . J. VEL (MPH) DATT		5 2 2 2 2 2 2 3 2 3 3 3 3 3 3 3 3 3 3 3	~ ~ ~ ~ w .	- U - 12 00 C	8449.7.	~ w ~ w	7 32 32 19 19 19 1	444	7 5 6 5 5 5 5 5 5	7 50 60 5
METEOROLOGICAL SI BRIDGEPORT COI METEOROLOGICAL SI BRADLEY FIELD COI	SITE DIR (DEG) CONN. VEL (MPH) RATIO SITE DIR (DEG) CONN. VEL (MPH) SPD (MPH) RATIO	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	426.0 10.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.510 1.90 1.11.8 1.70 6.7	0.881 9.4.2 9.4.2 9.29 9.30 665	0.820 270 3.8 8.2 9.467 3.60 5.2	0.973 22.0 22.0 22.0 30.93 47.0 8.5	& @ W & A & P P D	0.01 0.01 0.01 0.03 0.03 0.03 0.03 0.03	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

CONNECTICUT DEPARTMENT OF ENVIRONENTAL PROTECTION

202	LUTANT	POLLUTANTTOTAL SUSPENDED F	PARTIC	TE PARTICULATES	TEN HIGHEST	T 24 HR A	AVG TSP DAY	YS 1978 WI	TH MET.	DATA		MICROGRAMS	s PER CUBIC	C METER	
	•	TOWN NAME	SITES	SAMPLES	-	a	M	4	ស	ဖ		60	( O)		
	-	METEOROLOGICAL SITE WORCESTER MASS.	S. VEL (1	(DEG) (MPH) (MPH)	260 5.7 6.2	270 7.4 8.3 0.889	230 1.9 5.3 65	210 10.2 10.5 0.975	60 5.5 6.2 0.888	340 3.9 6.8 8.72	310 20.5 20.5 9.9 7.9	6	70 4.1 5.2 0.791	0 .0 0 0 .0 0 .0 0 .0 0	
	BRISTOL	TEOROLOGICAL SIT	w n	45 DATE (DEG) (MPH)	•	.572.8	20 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	6. 20 7.	89 8/24/78 240 6.2 7.0	∞ r n · ·	(D) (N) (N) + +	83 6/ 1/78 310 7.4 9.1	004		
70		METEOROLOGICAL SITE BRIDGEPORT CONN. METEOROLOGICAL SITE BRADLEY FIELD CONN.	RATIC N. VEL (N. SPD (N. SPD (N. NET IC) RATIC SPD (N. VEL (N. SPD (N.	10 (MPH) (MPH) 10 (MPH)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.610 190 11.8 0.360 170 7.0	0.195 200 200 7.3 160 3.4		0.881 9.0 9.2 9.2 0.0 0.0 0.0	0.828 190 10.8 10.8 0.744 8.8	0.52 0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.820 270 8.89.89 6.23 8.09 8.09	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 864 0 72.0 1 2 2 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	
		METEOROLOGICAL SITE WORCESTER MASS.		(DEG) (MPH) (MPH)	0.872 270 7.4 8.3 0.889	r0 ← · · r~	W (1) * * U	~ ro · · or ~	$\omega \omega \cdot \omega$	o - · · 0	<u> </u>	0.754 3.40 6.8	00000	~ <b>* • • *</b>	
	BURLI	BURLINGTON METEOROLOGICAL SITE NEWARK N. J.		204 DATE (DEG) (MPH)	97 8/ 9/78 220 9.3 9.6	22.7.7.	25 45 7	228 7.89 9	7242	727	7 7 7 9 19 19 19 19 19 19 19 19 19 19 19 19 1	7 22 8 8 8 8	7.50	7 2 8 8 8 8 9	
		METEOROLOGICAL SITE BRIDGEPORT CONN.	N. VEL SPD	C (MPH)		280 1280 16.2 16.2 16.2		~ in · · O ii	100 • • 00 t	$00 \cdot \cdot 00$	-0.101	10 i0 · · N i	0 h · · 0 i	4 P · · · 00 (	
				VEL (MPH) SPD (MPH) SPD (MPH) DIR (DEG) VEL (MPH) RATIO	0.90 8.0 250 100.1 100.1	0.6 8.2 3.6 3.0 3.0 1.1 2.2 6.8 6.8	0 - 6 4 8 8 8 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	0.66.00 0.66.00 0.66.00 0.06.00 0.06.00 0.06.00	0.925 0.925 250 7.44 7.88	0.992 0.992 0.992 0.930 0.924	6 4 4 4 8 8 8 9 9 8 9 9 9 9 9 9 9 9 9 9 9	0 -	6 - 0 0 0 - 4 - 7 - 0 0 0 - 4 - 7 - 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 - 4 0 - 4 0 0 0 - 1 0 0 - 1 0 0 7 0 4 0 4	
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SUSPENDED PARTICULATES  ***CORRESTER MASS.** VEL (MPH)  ***CESTER MASS.** VEL (MPH)  ***CONN.** VEL (MPH)  ***CONN.** VEL (MPH)  ***CESTER MASS.** VEL (MPH)  ***CONN.** VEL (MPH)  ***CESTER MASS.** VEL (MPH)  ***CESTER	TSP DAYS 1978			30	, r	.365 0.98	135	/ 1/78 12/16/7	10	· o	820 0.93	270 24	.8	8.2	.467 0.77	19	n c	754 0 88	340		.8	.572 0.92	ų	715/78 5/20/7	180 210	6	0.0	170 0.9	5	8.0	.396	08	- u o a	ָרָים מיני	20° 4	9 4	· 0	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$
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ENGINEERING

AIR COMPLIANCE

ENVIRONENTAL PROTECTION

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CONNECTICUT DEPARTMENT

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IE PARTICULATES	TE SAMPLES	DIR (DEG) VEL (MPH) SPD (MPH) RATIO VEL (MPH) SPD (MPH) RATIO DIR (DEG) VEL (MPH) SPD (MPH) RATIO	5 84 DIR (DEG) VEL (MPH) SPD (MPH) RATIO DIR (DEG) VEL (MPH) SPD (MPH)	DATE DATE DIR (DEG) VEL (MPH) SPD (MPH) RATIO SPD (MPH) SPD (MPH) NATIO DIR (DEG) VEL (MPH) SPD (MPH) RATIO
POLLUTANTTOTAL SUSPENDED PAR	TOWN NAME SITE	METEDROLOGICAL SITE BRIDGEPORT CONN. METEOROLOGICAL SITE BRADLEY FIELD CONN. METEOROLOGICAL SITE WORCESTER MASS.	METEOROLOGICAL SITE NEWARK N. J. METEOROLOGICAL SITE BRIDGEPORT CONN. METEOROLOGICAL SITE BRADLEY FIELD CONN. METEOROLOGICAL SITE WORCESTER MASS.	METEOROLOGICAL SITE NEWARK N. J. METEOROLOGICAL SITE BRIDGEPORT CONN. METEOROLOGICAL SITE BRADLEY FIELD CONN.

1978 WITH MET. DATA UNITS : BICROGRAMS PER CUBIC METERS	Ø .	20 300 250 270 340 32	1.2 5.7 7.9 3.9 13	15.5 12.9 5.9 8.0 6.8 (3.	02 0.866 0.968 0.982 0.572 0.97	٠	4 92 85 84 84	78 7/ 7/78 10/23/78 2/13	10 200 330 220 270 24	.4 6.6 11.0 8.4 7.4 2.	9.1 7.8 11.4 8.9 11.2 5.	20 0.851 0.967 0.939 0.662 0.46	240 280 280 280 280 280 280 280 280 280 28	יים מיים דיים מיים מיים מיים מיים מיים מ	67 0.671 0.978 0.950 0.770 0.41	60 200 320 190 310 at	.9 4.6 9.5 6.9 3.0	5.2 5.3 10.1 7.6 8.2 5.	54 0.870 0.941 0.902 0.444 0.80	40 250 320 240 300 30	.9 5.7 13.3 7.7 11.2 6.	7.9 2.9 7.9 7.9 7.9	.5/2 U.958 Q.972 Q.969 Q.856 Q.81	127 124 105 104 1	9/78 6/19/78 3/21/78 12/16/78 7/ 7/78 4/1	00 250 180 210 220 3	.6 4.4 5.4 7.6 8.4 19.		.631 C.44C C.61O C.938 @.939 @.0	240 240 240 30 24 24 25 240 30		71 0.370 0.360 8.778 8.950 8.95	00 170 170 190 190 30	.6 2.1 6.7 3.1 6.9 16.	5.3 4.3 7.0 3.4 7.6 16.	70 0.494 0.954 0.888 0.902 0.99	50 260 210 260 240 29	.7 2.1 10.2 5.7 7.7 19.	5.9 5.0 10.5 6.2 7.9 20.	68 0.346 0.975 0.927 0.969 0.9	
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TEN HIGHEST	<b>F</b>	260		. 0	•		150	-		D (	0 0 0	200	14.8					700	000	0 4		Ö	)	150	œ	и п 5 5 6		. 0	)		თ თ	0.427	0 G		. 6				4 Q	)	
PARTICULATES	TE SAMPLES		SPD (MPH)	-	) - - -		£ 61				_	DIR (DEG)		(MdW) OdS	9		VEL (MPH)		DIP (DEC)			0	 	7 555	DA LE		SPD CREEK		DIR (DEG)	VEL (MPH)	SPD (MPH)	RATIO	(פוןט אוס				\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	SPD	-		
POLLUTANTTOTAL SUSPENDED PA	TOWN NAME SIT	METEOROLOGICAL SITE	0 4 E				OLD SAYBROOK	######################################	7 2				BRIDGEPORT CONN.			METEURULUGICAL SITE				MORCHES MASS.				VI AMPLIKO	1++0 -e0+00-000-445				METEOROLOGICAL SITE				10 10 10 10 10 10 10 10 10 10 10 10 10 1				WORCESTER MASS.				

### FOR LOUND STATE SAMPLES 1 2 3 4 5 5 6 7 7 8 9 9 10 10 10 10 10 10 10 10 10 10 10 10 10		Z.W.	EN HIGHEST	24 HR	AVG TSP DA	DAYS 1978 W	WITH MET.	DATA				
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FORTILITIES   FORTING   190   100	NAME		<del>Çer</del>	8	m	ব	ហ	Ø	7	<b>CO</b>	Ø	9
NEULOGICAL SITE DIR (DEG) 210 180 220 210 220 240 180 220 260 190 200 240 240 240 240 240 240 240 240 24	STAMFORD	83	152 5/20/78	130	128	109	109	104	103	97	90	9.4
NEW CONTINGENIES   S. C.		DIR	210	180	210	270	310	220	240	180	250	Ō
PRODUCICLE, SITE DIR (DEG) 2.924 0.610 0.293 0.662 0.956 0.851 0.105 0.440 0.8	• E	י אני אניר	ວ ແ ກ ຫ	υα 4. α		4.6	_ o	00 0 4. 0	0 r	- u	4 Q	in the second se
PRILICECTION. STEE IN (IDEG   220			0.924	•	. 6	- •	0.964	•	٠ œ	٠.	14	0.840
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SPECIAL SITE DIR FOLKS   STATE   17.5		· VEL	10.0	4 ;	ω (	12.5	ອ ອີ	Am .	4	4	₩ (	20 00 00 00 00 00
PROLUGICAL SITE DIR (DEC)   210   170   190   210			0.936	,	2,7	_ ,	9 6	P-17	D 4	ר ע	ໝ ຕຸ	ຫຼວ ຫຼວ ວ
MANCESTER MASS.   STATE   MASS.   STATE   ST		DIR			. C)	,	300	•		, ,	, 4	80
SEPECING		VEL		6.7		3.6	16.5	<b>6.</b> 9	ო ო	3.4	2.1	14.9
MORCESTER MASS. VEL (MPH) R. 21 2.0 2.0 3.0 0.990 0.990 0.900 0.665 0.586 0.494 0.944 0.991 0.000 0.200 0.200 0.905 0.90		SPD (MPH)			m		16.7		រេ	ហ	4	ມ. ໝໍ
## ORDINGESTER MASS. VEL (MPH) 2.70 2.00 5.77 11.2 29.0 2.40 6.2 5.3 6.0 13.7    ## ORDINGESTER MASS. VEL (MPH) 2.70 2.00 5.77 11.2 2.0 19.8 7.7 5.5 1.9 2.0 13.7    ## ORDINGESTER MASS. VEL (MPH) 1.2 10.2 5.7 11.2 2.0 19.8 7.7 5.5 1.9 5.3 6.0 13.7    ## ORDINGESTER MASS. VEL (MPH) 1.2 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0		RATI	0.872	•	8	•	066.0	•	φ	ທ່	4.	0.0 • 40. • 6.6
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NEWARK N. J. VEL (MPH)   10.8   6.9   8.4   9.0   10.7   130   240   270   310	410	6	5/26/7	/ 7/7	E,	/20/7	2/1	1/6/	2/1	/25/7	/13/7	68/
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BRIDGEPORT CONN. VEL (MPH) 15.2 8.0 14.7 10.0 10.2 4.0 12.2 9.8 9.8 16.3 17.4 17.4 17.4 10.6 13.5 7.3 12.6 11.2 12.9 17.4 17.4 10.8 18.1 10.6 13.5 7.3 12.6 11.2 12.9 17.4 17.4 17.4 0.936 0.757 0.550 0.961 0.874 0.754 0.936 0.901 0.904 0.992 0.774 0.936 0.957 0.560 0.961 0.874 0.754 0.936 0.961 0.874 0.754 0.936 0.961 0.874 0.754 0.936 0.961 0.874 0.754 0.936 0.961 0.874 0.754 0.936 0.961 0.904 0.992 0.499 0.872 0.703 0.586 0.961 0.613 0.621 0.977 0.970 0.904 0.992 0.499 0.872 0.703 0.586 0.961 0.613 0.621 0.977 0.970 0.904 0.992 0.499 0.872 0.703 0.586 0.961 0.613 0.621 0.977 0.970 0.904 0.992 0.499 0.872 0.703 0.586 0.961 0.613 0.621 0.977 0.970 0.904 0.992 0.499 0.872 0.703 0.986 0.961 0.613 0.904 0.992 0.907 0.904 0.906 0.907 0.904 0.908 0.872 0.889 0.676 0.965 0.981 0.981 0.987 0.966 0.995 0.907 0.904 0.992 0.907 0.904 0.908 0.676 0.905 0.981 0.987 0.966 0.995 0.907 0.908 0.907 0.908 0.907 0.908 0.907 0.908 0.907 0.908 0.907 0.908 0.907 0.908 0.907 0.908 0.907 0.908 0.907 0.908 0.907 0.908 0.907 0.908 0.907 0.908 0.907 0.908		DIR			•	22	3	EA		. 4	260	ခို
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DLEY FIELD CONN. VEL. (MPH) 7.5 8.7 1.7 5.15 4.9 3.4 13.15 2.8 5.3 13.5 5.9 5.7 11.5 4.6 8.5 13.8 8.8 8.4 6.3 6.9 5.7 11.5 4.6 8.5 13.8 8.8 8.4 6.3 6.9 5.7 11.5 4.6 8.5 13.8 8.9 8.0 0.872 0.703 0.586 0.961 0.613 0.621 0.977 0.977 0.006 0.961 0.613 0.621 0.977 0.977 0.006 0.961 0.613 0.621 0.977 0.977 0.978 0.872 0.889 0.676 0.965 0.961 0.613 0.621 0.977 0.977 0.936 0.921 0.732 0.889 0.676 0.365 0.881 0.982 0.886 0.950 0.950 0.950 0.950 0.950 0.950 0.881 0.981 0.982 0.886 0.950 0.95		DIP (DEG		•	ים פ		. ?	**	•	,	40,0	n (
SPD (MPH) 8.3 8.8 3.4 6.3 6.9 5.7 11.5 4.6 8.5 13.8 RATIC 0.904 0.992 0.499 0.872 0.703 0.586 0.961 0.613 0.621 0.977    OROLOGICAL SITE DIR (DEG) 60 210 110 270 300 230 300 270 250 300    NORCESTER MASS. VEL (MPH) 7.3 8.2 4.1 7.4 7.0 1.9 11.5 7.9 9.0 15.2    SPD (MPH) 7.3 8.9 5.6 8.3 10.3 5.3 13.1 8.0 10.3 16.0    RATIC 0.904 0.992 0.499 0.872 0.703 0.586 0.961 0.613 0.621 0.977    SPD (MPH) 7.3 8.9 5.6 8.3 10.3 5.3 13.1 8.0 10.3 16.0    SATIC 0.921 0.732 0.889 0.676 0.365 0.881 0.982 0.866 0.950    NEWARK N. J. VEL (MPH) 9.0 7.6 11.2 1.0 5.4 7.4 9.0 16.9 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8    SPD (MPH) 9.8 8.0 12.6 5.0 8.9 11.2 10.3 20.6 11.4 7.8 10.3 10.3 10.3 10.3 10.3 10.3 10.3 10.3		VEL (MPH		8.7	1.7	n n		- (c)		) (C	) in	- ) (*
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		$\mathbf{H}$		0.938	(O	ത	-	~	*-	œ	N	ø	เก
			(DEG)	240	ဗ္ဗ	0	20	LO.	o	28	22	ത	ന
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BRADLEY FIELD C	CONN	VEL C		- 6 - 0	ກ	ס י	_	ກ	~	Ω	_	V	Э 🗆
			(HdM)	- 4 - 4	•	•	•		٠			່ເ	•
	. 1	_		988	• 00	• 20	· w		• 15	٠.	٠.	· w	• [
	SITE	DIR (D	(DEG)		8	23	28	2	2	28	5	9	, cd
			(MPH)	5.7		•	8		Ö			•	5.2
		SPD (N	(Mbh)	9. 2	•	٠		•	•	•		•	•
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MATERBURY		<b>6</b> 0		416	~	- 1	150	4	0	130	103	000	-
			DATE 1.	1/10/78	11/4/78	സ	ω,	8/24/78	10/17/78	6/ 1/78	0	~	w,
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		-		0.421	0.973	• CC	• (*	٠ α	. 0	- c	0 0	ο α • C	n e
METEOROLOGICAL S	SITE	DIR (C	(DEG)	80	4	28	24	) 6	) (	2 5	, ,		. ~
	٠.		(MDH)	10.6	•	•							
	~•		(PH)	12.1	•			6.6	4			•	
		_		0.874	വ	~	~	2	œ	ഥ	ന	Q.	
METEOROLOGICAL	SITE		(DEG)	20	ഗ	-	ത	S	4-	ယ	*	<b>P</b>	
		VEL (N	(MPH)	٠. ف		•	•	•	•	•		•	
		SPD	(Hall		+ (	ω.	က်	ທີ່	ທ່	ທ່	ဖ်	ω	ហ
		מו שור	(0)	70.481	O 1	4 (	œι	ωι	91	ഗ	<b>~</b> 1	നം	0.586
, 16549010501-118 E GREATCOCA	1000	1		) • •	ດ	, ,	D.	o	N	4	•	~	
	_	SPD		- C	- c	10.0	. o	ນ ແ ໜໍເ	4 4	on a	4.0	N 0	ء ب س د
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CONNECTICUT	DEPARTMENT	OF ENV	ENVIROMENTAL	PROTECTION	Z		,	# <del>*</del>			AIR COMPLIANCE		engineering
POLLUTA	POLLUTANTTOTAL SUSPENDED		PARTICULATES	EN HIGHES	T 24 HR	AVG TSP DI	DAYS 1978 1	WITH MET.	DATA	UNITS:	MICROGRAMS	S PER CUBI	C METER
	TOWN NAME	SI	SITE SAMPLES	<b>400</b>	N	ო	4	ហ	ဖ	7	Ø	0	1
WA.	WATERBURY	₩.	123 122	259	949	245 745	•	v	. 0				
				1/5/78	t (C	rα	40/ 4/10	ກຸ່	9	201	197	197	188
		SITE	DIR (DEG)	200	210	280	30.	, ,	270	2/22/78	4/2/78	<b>3</b>	12/13/78
	NEWARK	х Э			7.6		) t	2 4 6	2 0	ט פ	320	9 (	230
÷			SPD (MPH)		0.8	10,	•	0 5	÷ u	กเ	18.7	5) (N	ó
				0.950	0.938	757 0	7 0	* C	'n	ח מ	_	ດ ເ	ed ed
	METEDROLOGICAL	SITE	DIR	,	? C	•	•	•	- C	0.80	0.973	.527	0.826
		CONN.	VEL		ω ω	10.6	, tu	o a	7 0	, co	9 6	, D	240
			SPD (MPH)	10.2	10.9	12.2		, t		ru	) V	4 (	\$ (
,			RATI	0	0.778	œ	O	0.761	, ני ני	າ	- 60	. 5	9
	ME EUROLOGICAL	SITE			ത	290	00				•	\$ C	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \
		CONN.	VEL		 1.	7.7	•	2.6		, , , ,	100	V	) (
	÷	,	SPD (MPH)	0. 9	'n	8.5		4.7	. o	ď	- c	? c	
			RATIC	0.983	ω	0.835	ហ	0.541	0.784	) 0	000	, c	
		SILE	DIR (DEG)	250	စ	280	7	S			•	- 6	
		MASS.	VEL	ص ه		0.1		9.9	) (		ว <u>เ</u>	n	) N
•				8	6.2	თ თ		6.5	'n	(C)	900		9 G
8			RATIO	0.943	a	S	m	0.722	0.980	0.971	0.00.0	0.784	0 0 0 0
19											•	)	)
AM	MATERFORD		4	Č		i	. 1						
			- H	100/10	4 (		67	99	ω	09	58	(N)	RU A
•		SITE	DIR (DEG)	7 / 60 / 7	9//8//	1 C	-	<b>o</b> n 1	6/13/78	~	7/13/78	7/ 1/78	2/ 7/78
	NEWARK	2	<u> </u>		000	2 '	_	250	270	220	a	320	0
			י ני זיי		ء د د	٠,	7.4	4.4	0.7	Ø.	•	11.6	0
	,			•	- (	_ (	0)	0)	4			2	0
		SITE	018 (086)	100	בה מ מ מ מ	0.662	0.820	0.440	0.637	0.939	0.938	0.961	0.020
	BRIDGEPORT	CONN	VEI (MPH)		200	2 2 2	270	180	260	240	ന	(.,	3
					t c	0.4	30 (P	M	თ დ	•	•	11.4	4
			2 T T C	C	0	6	90	œ	₩	11.6		12.6	26.6
		STTE	מיים (מיים מיים מיים מיים מיים מיים מיים	) ) ) ()	0.673	0.770	0.467	0.370	0.754	IJ	0	U	10000000000000000000000000000000000000
	BRADIEY FIFEID	120	•		200	310	360	170	240	ത	-	(v)	ď
		-			4. i	დ დ	თ თ	٠, د	ເນ	•		6	) (c
			C T T T T T T T T T T T T T T T T T T T	. •	ומו	œ ·	ល	4.3	ຜ	•		7. R.	0
	TACTOCIONO FINANCE	7.110	•	20.0	0.870	0.444	0.754	0.494	0.621	0	· C	022	י ע ס
		U U U	מונים אות	2.70	220	300	340	260	250	2	9		•
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				m (	រេ	12	<b>6</b> .8	0.0	9	6.		) G	i €
			KALIU	6.88 68 68 68	0.968	0.866		0.346	900	· cc		9 0 9 0 9 0	) e
									•	•		n	•

#### III. SULFUR DIOXIDE

#### Conclusions:

None of the air quality standards for sulfur dioxide (SO<sub>2</sub>) were exceeded in Connecticut in 1978. Measured concentrations were substantially below the 80  $\mu g/m^3$  primary annual standard, the 365  $\mu g/m^3$  primary 24-hour standard, and the 1300  $\mu g/m^3$  secondary 3-hour standard. Measured concentrations were closer to, but also below, the 60  $\mu g/m^3$  secondary annual standard and the 260  $\mu g/m^3$  secondary 24-hour standard.

According to the results from the Wilcoxon Test (which made use of sulfation rate data) there was a significant improvement in  $SO_2$  levels from 1977 to 1978 (see Table 3). This improvement was not evident in the data from DEP's monitors that measure  $SO_2$  directly, but this is probably due to the fact that there was insufficient data available in 1977 to compare with 1978. As with TSP, the general improvement in  $SO_2$  levels (shown by the Wilcoxon Test) was probably caused by the decreased frequency of southwest winds from 1977 to 1978 and the associated reduction in the transport of  $SO_2$  from the southwest.

The continued attainment of the SO<sub>2</sub> standards is primarily attributable to Connecticut's regulation which restricts the sulfur content in fuel to .5%.

#### Method of Measurement:

The DEP Air Monitoring Unit uses several types of instruments to continuously measure sulfur dioxide levels. The coulometric method is employed by Philips instruments; the flame photometric method is used by Bendix instruments; and the pulsed fluorescence method is used by Teco instruments.

Philips monitoring instruments were used at the following sites in 1978:

Bridgeport	001	Hartford 123	Milford	002
Greenwich		(1 month)	Stamford	123
		Meriden 001		

Bendix monitoring instruments were used at the following sites in 1978:

Bridgeport 123	Groton 123	New Haven 123
(2 months)	(2 months)	(4 months)
Danbury 123	Hartford 123	Waterbury 123
(3 months)	(2 months)	(2 months)
Derby 123	New Britain 123	•
(2 months)	(4 months)	

Teco instruments were used at the following sites in 1978:

Bridgeport 123	Groton 123	New Britain 123
(10 months)	(10 months)	(8 months)
Danbury 123	Hartford 123	New Haven 123
(9 months)	(9 months)	(8 months)
Derby 123	Middletown 123	Waterbury 123
(7 months)		(10 months)
Enfield 123		

#### Discussion of Data:

Monitoring Network - A total of 15 continuous SO<sub>2</sub> monitors recorded data in 14 towns in 1978 (see Figure 5). Ten of these sites telemetered the data to the central computer in Hartford on a real-time basis. Table 13 shows that sufficient data for valid annual means (at least 75% of the possible sampling hours) were recorded at 10 sites. The averages for the remainder of the sites represent 50-75% of the possible sampling hours.

Annual Averages –  $SO_2$  levels were below the annual standards at all sites in 1978 (see Table 13). The annual average  $SO_2$  levels decreased from 1977 to 1978 at 6 of the 15  $SO_2$  monitoring sites. The decrease at two of these sites exceeded 5  $\mu$ g/m³. On the other hand, annual average  $SO_2$  levels increased from 1977 to 1978 at 8 monitoring sites with two of the increases exceeding 5  $\mu$ g/m³. The annual average  $SO_2$  level remained the same at one site (Greenwich, site 004). These changes do not indicate any significant upward or downward trend since many of the annual averages (especially in 1977) were based on incomplete data.

Statistical Projections - A statistical analysis of the sulfur dioxide data is presented in Table 14. This analysis provides information to compensate for the loss of data caused by instrumentation problems. The format of Table 14 is the same as that used to present the total suspended particulate annual averages. However, Table 14 gives the annual arithmetic mean of the valid 24-hour SO<sub>2</sub> averages to allow direct comparison to the annual SO<sub>2</sub> standards. The 95% limits and standard deviations are also arithmetic calculations. Since the distribution of SO<sub>2</sub> data tends to be lognormal, the geometric means and standard deviations were used to predict the number of days the 24-hour standards of 260  $\mu \rm g/m^3$  and 365  $\mu \rm g/m^3$  would be exceeded at each site if sampling had been conducted every day.

It is important to note that these statistical tests require random data to be valid. This means that an equal number of samples must be collected in each season of the year and on each day of the week. The distribution and quantity of SO<sub>2</sub> data were far better in 1978 than in 1977 although there were some sites with gaps in the data during the winter months. Nonetheless, the data indicate, with reasonable assurance, that there were no violations of the secondary or primary SO<sub>2</sub> standards in Connecticut. The statistical prediction of one day exceeding the secondary 24-hour SO<sub>2</sub> standard (260  $\mu \text{g/m}^3$ ) at Hartford site 123 indicates that an increase in SO<sub>2</sub> emissions there might jeopardize the attainment of this standard. (Two days over the standard are required for the standard to be violated.)

24-Hour Averages - In 1978, no sites recorded SO<sub>2</sub> levels in excess of the 24-hour standards (see Table 15). The second high 24-hour concentrations increased from 1977 to 1978 at 14 of the 15 SO<sub>2</sub> monitoring sites. The increase exceeded 25  $\mu$ g/m³ at 9 of these sites. The second high 24-hour concentration decreased at only 1 site and that decrease was less than 25  $\mu$ g/m³. The increases noted above are largely attributable to the additional amount of data available in 1978 compared to 1977.

Although there has been some ambiguity in the past, the current EPA policy bases compliance with the primary 24-hour SO<sub>2</sub> standard on non-overlapping running averages. Running averages are averages computed for the 24-hour periods ending at every hour. Assessment of compliance is based on the value of the 2nd highest of the two highest non-overlapping 24-hour periods in the year. (Note that the highest 24-hour period in the year may overlap both of these two periods.) Thus, compliance assessment is based on the magnitude of the exposure encountered within any two distinct 24-hour periods and not on a calendar day exposure basis. However, there is some contention that compliance assessment for 24-hour SO<sub>2</sub> standards should be based on calendar day averages only. Table 16 contains the maximum 24-hour SO<sub>2</sub> readings from both the running averages and the calendar day averages for comparison. The maximum calendar day readings are roughly 10% lower than the maximum readings from the running averages.

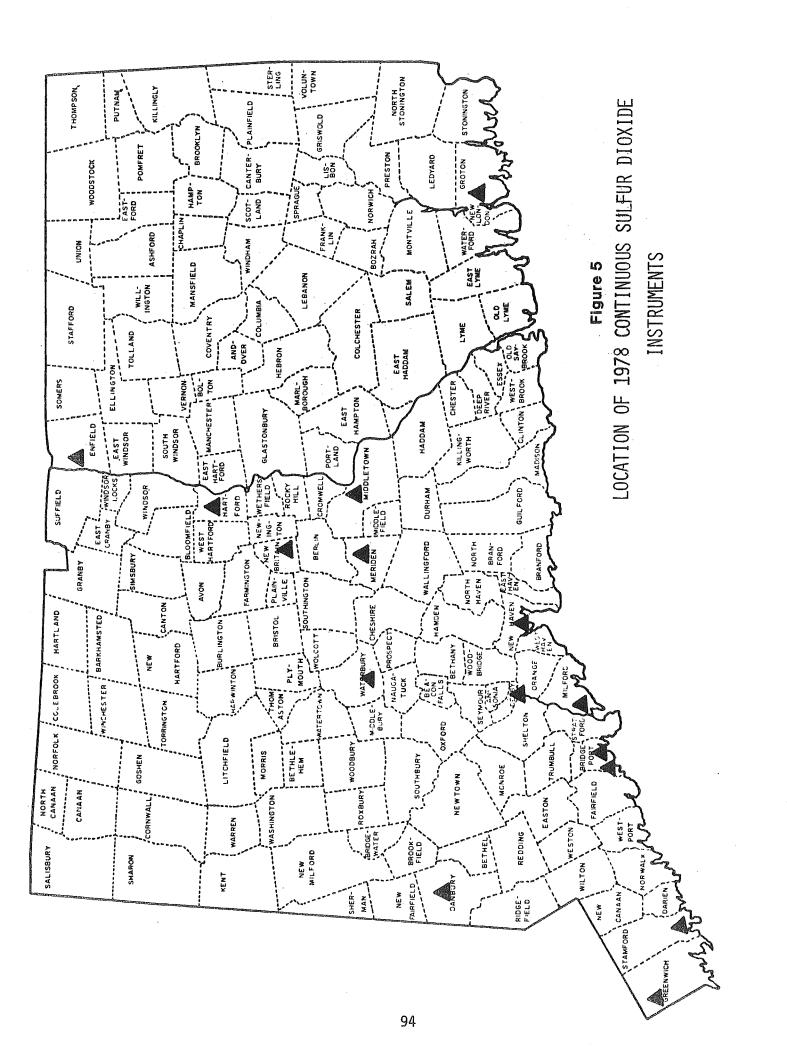
 $\frac{3-\text{Hour Averages}}{50_2}$  - Measured SO<sub>2</sub> concentrations were far below the 3-hour  $\frac{50_2}{50_2}$  standard at all DEP monitoring sites in Connecticut in 1978 (see Table 17).

10-High Days with Wind Data - Table 18 lists the 10 highest 24-hour calendar day  $SO_2$  averages (with the dates of occurrence) for each  $SO_2$  site in Connecticut for 1978. This table also shows the average wind conditions which occurred on each of these dates. (The origin and use of these wind data are described in the discussion of Table 12 in the TSP section.)

Once again, as with TSP, most of the highest  $SO_2$  days occur with southwesterly winds and most of those days have persistent winds. This relationship could be caused, at least in part, by  $SO_2$  transport; but this transport is limited by the chemical instability of  $SO_2$ . In the atmosphere,  $SO_2$  reacts with other gases to produce, among other things, sulfate particulates; so  $SO_2$  is not likely to be transported long distances. Previous studies conducted by the DEP have shown that, during periods of southwest winds, levels of  $SO_2$  in Connecticut decrease with distance from the New York City Metropolitan area. This relationship tends to support the transport hypothesis. On the other hand, these studies also revealed that certain meteorological parameters (most notably mixing height and wind speed) are more adverse on days with southwest winds than on other days.

Using the data in Table 18, a tally was made, by date, of the frequency of occurrence of high levels. If a given date recurred at 5 or more sites in this tally, the SO2 levels and associated meteorological conditions were investigated further (there were 12 such days). A close look at these 12 days revealed three important points. First, all 12 days occurred during the winter months. This can be attributed to more fuel being burned during the cold weather. Second, 5 of the 12 days had persistent southwest winds for that calendar day. Third, the other 7 days had persistent southwest winds for at least the 24 hours prior to the highest running 24-hour average on that date.

In summary, high levels of  $SO_2$  in Connecticut seem to be caused by a number of interrelated factors. First, Connecticut experiences its highest  $SO_2$  levels during the winter months, when there is increased fuel combustion. Second, the New York City Metropolitan area, a large emission source, is located to the southwest of Connecticut. Third, southwest winds occur relatively often in comparison to other wind directions. Fourth, adverse meteorological conditions are associated with southwest winds. The net effect is that during the winter months when a persistent southwest wind occurs, the air will pick up increased amounts of  $SO_2$  over the New York City area and transport this  $SO_2$  into Connecticut, where the  $SO_2$  levels will remain high because the relatively low mixing heights associated with the southwest wind will not allow for much dilution. The levels of transported  $SO_2$  eventually decline with increasing distance from New York City as the  $SO_2$  is dispersed and as it slowly reacts to produce sulfate particulates.



### TABLE 13

# ANNUAL ARITHMETIC AVERAGES OF SULFUR DIOXIDE AT SITES WITH CONTINUOUS MONITORS

## PRIMARY NAAQS 80 $\mu g/m^3$ SECONDARY SAAQS 60 $\mu g/m^3$ (a)

TOWN	SITE NAME	1978 ANNUAL AVERAGE
Bridgeport-001	City Hall	26
Bridgeport-123	Hallett Street	46
Danbury-123	Western Conn. State College	34
Derby-123	Dziadiz Street	(34) <sup>1</sup>
Enfield-123	Kosciuszko Junior High School	29
Greenwich-004	Bruce Golf Course	(34)
Groton-123	Fort Griswold State Park	23
Hartford-123	State Office Building	35
Meriden-002	Stoddard Building	(24)
Middletown-003	City Hall	(34)
Milford-002	Devon Community Center	3.1
New Britain-123	Lake Street	23
New Haven-123	State Street	41
Stamford-123	Health Department	(29) <sup>†</sup>
Waterbury-123	Bank Street	31

<sup>(</sup>a) State of Connecticut Air Quality Standard

<sup>1</sup> Estimate based on partial data (50-75%)

AIR COMPLIANCE MONITORING TABLE 14 1978 SO2, ANNUAL AVERAGES AND STATISTICAL PROJECTIONS CONNECTION PAGE 1

DISTRIBUTIONLOGNORMAL	D PREDICTED R DAYS OVER
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	95-PCT-LIMITS
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IOXIDE	0 L
ULFUR D	CITE VER
PULLUIANISULFUR DIOXIDE	TMAN NWCT

PREDICTED DAYS OVER 365 UG/M3															
PREDICTED DAYS OVER 260 UG/M3															
STD DEVIATION	15.720	26.200	20.960	15.720	20.960	20.960	15.720	31.440	20.960	23.580	23.580	20.960	34.060	28.820	20.960
95-PCT-LIMITS LOWER UPPER	25	84 8	35	36	30	35	25	35	<b>56</b>	34	34	23	. 43	26	32
95-PCT. LOWER	23	45	32	32	59	32	20	33	22	31	31	21	39	22	30
ARI. MEAN	24.0	46.6	3305	33.8	29.6	33°3	21.2	34.3	24.1	32.8	32.8	21.7	41.1	23.6	31.2
SAMPLES	279	305	288	172	327	255	264	333	226	252	282	276	289	247	321
YEAR	1978	1978	1978	1978	1.978	1978	1978	1978	1978	1978	1978	1978	1978	1978	1978
SITE	100	123	123	123	123	004	123	123	005	003	005	123	123	123	123
TOWN NAME	BRIDGEPORT	BRIDGEPORT	DANBURY	DERBY	ENFIELD	GREENWICH	GROTÓN	HARTFORD	MERIDEN	MIDDLETOWN	MILFORD	NEW BRITAIN	NEW HAVEN	STAMFORD	WATERBURY

The annual averages in Table 14 vary slightly from those in Table 13 because of the manner in which they were derived. Table 13 contains the annual averages of all the available hourly readings. Table 14 contains the annual averages of all the valid 24-hour averages. (At least 18 hours of valid data are required to produce a valid 24-hour average.)

TABLE 15
1978 MAXIMUM 24-HOUR SULFUR DIOXIDE CONCENTRATIONS

SITE	DATE* 1ST HIGH	DATE 2ND HIGH	0 100	ncentration 200	(µg/ 260	m <sup>3</sup> ) 300	365 400
Bridgeport-001	12/16/	11 01/24/18	142 130				
Bridgeport-123	01/06/	10 12/13/10	237- 196		_		.
Danbury-123	12/13/	01 12/16/23	154 133	-			
Derby-123	01/13/	06 <sup>a</sup> 01/12/14	149 139	-	1		1
Enfield-123	01/06/	18 02/17/24	146		1		
Greenwich-004	02/18/	20 09/16/11	151	<u>.</u>			
Groton-123	01/10/	18 02/18/07	131				
Hartford-123	01/24/	23 02/18/09	176 173	1999 Anni Milat (1979)			
Meriden-002	01/24/	23 01/06/11	166	COSP SEASO SEASO			İ
Middletown-003	02/18/	15b 02/18/05	20 170	07			
Milford-002	12/13/0	08 01/05/16	141				
New Britain-123	01/06/		150 149	<b>-</b>			
New Haven-123	01/06/	LO 12/07/09	2	-239 14	-		
Stamford-123	02/18/	ll 12/13/01	195	230			
Waterbury-123	02/18/0	02/18/23	156 155		}		
*	a/aa.		£	Se	conda	ary Pi	rimary

<sup>\*</sup> Date is month/day/ending hour of occurrence

Non-overlapping maximum on  $01/13/14 = 140 \mu g/m^3$  b Non-overlapping maximum on  $02/19/05 = 173 \mu g/m^3$  Non-overlapping maximum on  $02/17/23 = 156 \mu g/m^3$ 

TABLE 16

COMPARISONS OF 1978 FIRST AND SECOND HIGH RUNNING AND
CALENDAR DAY 24-HOUR SO<sub>2</sub> AVERAGES
units = µg/m<sup>3</sup>

Site	lst High <u>Running Avg.</u>	lst High <u>Calendar Day</u>	2nd High Running Avg.	2nd High Calendar Day
Bridgeport 001	142	122	130	106
Bridgeport 123	237	184	196	170
Danbury 123	154	153	133	133
Derby 123	149	145	139	130
Enfield 123	146	141	141	140
Greenwich 004	151	142	151	138
Groton 123	131	124	122	105
Hartford 123	176	176	173	157
Meriden 002	166	166	164	144
Middletown 003	207	195	170	144
Milford 002	141	136	124	118
New Britain 123	150	139	149	113
New Haven 123	239	196	214	189
Stamford 123	230	201	195	192
Waterbury 123	180	165	155	143

TABLE 17

1978 MAXIMUM 3-HOUR SULFUR DIOXIDE CONCENTRATIONS

SITE	DATE Ist HIGH	* 2ND HIGH	0 100 200		400 , , , 1300
Bridgeport-001	07/26/14	01/24/09	240		
Bridgeport-123	01/06/06	01/05/24	315		! ! !
Danbury-123	12/12/21	12/16/02	194 191		1
Derby-123	01/13/05 <sup>a</sup>	01/13/07	159 155		
Enfield-123	03/10/13	01/06/16	244	<b></b>	·   
Greenwich-004	12/13/10	12/07/16	273		
Groton-123	02/17/24 <sup>b</sup>	02/17/22	189 173		
Hartford-123	12/07/10	01/24/19	274		 
Meriden-002	01/24/17 <sup>c</sup>	01/24/19	218		
Middletown-003	02/18/11	02/18/08	258		
Milford-002	02/27/17	03/04/10	197	<b>-</b>	
New Britain-123	01/24/08 <sup>d</sup>	01/24/06	256	m en en en	1
New Haven-123	01/06/09 <sup>e</sup>	01/06/07	333		
Stamford-123	02/18/07 <sup>f</sup>	02/18/09	257 244		 
Waterbury-123	02/03/24	02/17/24	393 295		Soconday
* Date is month	/day/onding	hour of co	unnanca		Secondary Standard

<sup>\*</sup> Date is month/day/ending hour of occurrence non-overlapping maximum on 01/13/04 = 157  $\mu$ g/m³ non-overlapping maximum on 02/18/01 = 182  $\mu$ g/m³ non-overlapping maximum on 01/24/16 = 214  $\mu$ g/m³ non-overlapping maximum on 01/24/09 = 237  $\mu$ g/m³ non-overlapping maximum on 01/06/10 = 315  $\mu$ g/m³ non-overlapping maximum on 02/18/06 = 245  $\mu$ g/m³

CONNECTICUT DEPARTMENT OF ENVIROMENTAL PROTECTION

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CONNECTICUT DEPARTMENT OF ENVIRONENTAL PROTECTION

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POLLUTAN	POLLUTANTSULFUR DIOXIDE	# I	TEN HIGHES	T 24 HR AV	VG SDZ DAY	S 1978	WITH MET.	DATA	STIM	eicrograms	PER CUB	IC METER
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		SPD (MPH) RATIO DIR (DEG) VEL (MPH) RATIO RATIO RATIO	1.1 2.3 270 270 5.2 5.3	• • 00 00 • • 63	4	• • 0 0 • • 0	· · 4 10 · · -	4.4	• • 00 (0) • • • •	• • • • • • • • • • • • • • • • • • • •	4	•••••••
<b>3</b> <b>3</b>	BRITAIN METEOROLOGICAL SITE NEWARK N. J. METEOROLOGICAL SITE BRIDGEPORT CONN	DIR VEL SPD RATI DIR	o	113 1/5/78 200 5.2 5.5 0.950 9.5	109 12/12/78 250 7.3 7.8 0.936 6.9	12/16/78 210 7.6 8.0 0.938 240	95 1/17/78 40 6.0 7.0 7.0 854 40 7.2	91 12/31/78 160 3.3 9.3 0.776 4.5	1/23/78 260 7.55 8.6 8.6 300		~ NO NO N N N	11/29/78 200 200 6.3 225 8.4
		SPD RATI DIR VEL SPD RATI	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0.928 170 170 5.9 6.0 983	• • 420 • • 00	• • • • • • • • • • • • • • • • • • • •	0 0 0 1 0 0 0 1 0 0 0 0 0	0 0 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	• • • • • • • • • • • • • • • • • • • •	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 100 100 100 100 100 100 100 100 100 1	6 6 6 7 7 8 9 9 9 9 9 9 9 9 9 9 9 9 9

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										wits	MICROGRAMS	IS PER CUBI	IC METER
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		7	784	190	189	172	160	150	144	4	132	128	127
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	METEOROLOGICAL SITE	DIR	(DEG)	250	7	28		) )	) C	Λt	O) I	4 I	oo 🛚
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		SPD (M	(MPH)	4.7	4	•				•	•	•	•
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	BRIDGEPORT	X 14 X		) C	ΣO.	360	80	300	240	Ø	190		250
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CONNECTICUT DEPARTMENT OF ENVIROMENTAL PROTECT	ENVIROMENTAL	PROTECTION	7						AIR COMP	AIR COMPLIANCE ENGINEERING	Gineering
		TEN HIGHEST	24 HR	AVG SO2 DA	SD2 DAYS 1978 N	WITH MET.	DATA				
FULLUIANI SULTUR DIOXIDE	.,							crits	MICROGRAMS	S PER CUBIC	1C METER
TOWN NAME	SITE SAMPLES	₩.	Ø	ო	4	; m	ဖ	~	Ø	Ø	Ç
WATERBURY	123 321	165	143	11	113	109	105	103	102	0	<u>თ</u>
	DATE	2/17/78	2/18/78	2/ 3/78	12/12/78	12/16/78	12/13/78	11/29/78	12/15/78	12/ 6/78	1/5/78
METEOROLOGICAL SITE	SITE DIR (DEG)	230	290	340	250	210	230	200	220	240	200
NEWARK N	4. J. VEL (MPH)	4.0	1.7	თ ღ	7.3	7.6	10.6	2.1	11.6	7.6	ro G
	SPD (MPH)	4 0.	3.7	ດ ດ	7.8	8.0	12.8	න ග	11.6	8 0	w w
	RATIC	0.819	0.458	0.937	0.936	0.93B	0.826	0.325	0.992	Ø.939	0.950
METEOROLOGICAL SITE	SITE DIR (DEG)		360	320	280	240	240	270	250	250	260
BRIDGEPORT C	CONN. VEL (MPH)	လ ထ	<u>.</u>	12.5	დ. დ.	8 .s	12.4	4	17.8	<b>9</b> .0	ທຸ
	SPD (MPH)		4.6	13.1	7.3	10.9	13.7	7.2	18.4	40.5	, 0.
	RATIO	0.520	0.359	0.955	0.942	0.778	0.907	0.576	9966	9.039	0.028
METEDROLOGICAL SITE	SITE DIR (DEG)	170	210	330	190	190	180	180	190	210	170
BRADLEY FIELD C	CONN. VEL (MPH)	<u>ب</u> ص	8.0	0.9	g		6.1	ი ი	დ თ.	0.4	ຫ ເຄ
	(MAM) OdS	ო ო	ر ن	6.6	2.3	9. 4.	7.0	დ	7.5	4.7	o. 0
. !		0.840	0.365	0.907	0.488	0.888	0.871	0.846	0.922	6.079	0.983
METEOROLOGICAL SITE	OI R		250	320	270	260	230	220	250	270	250
MORCHSTER IN	VEL	4 6	2.5	13.2	.2	5.7	G	ო ო	œ G	เบ ญ	ໜ ໝຸ
	SPD (MPM)	4.7	0	13.4	5.3	6.2	ю Ф.	d.	œ evi	ю (9)	ō G
	RATIC	0.895	0.435	0.986	0.975	0.927	956.0	0.771	966.0	0.940	0.049

#### IV. OZONE

## Conclusions:

As in past years, Connecticut experienced very high concentrations of ozone in the summer months of 1978. At each of the twelve monitored sites, levels in excess of the new one-hour NAAQS of 0.12 ppm were frequently recorded, with one-hour average concentrations occasionally exceeding 0.20 ppm.

The frequency and magnitude of levels in excess of the 0.12 ppm ozone standard decreased from 1977 to 1978. Some of this difference is attributable to the loss of a large amount of data during July of 1978 due to instrument problems. The remainder of this apparent improvement in air quality may be real, but only temporary, because it can be attributed to year-to-year variations in weather conditions. Although the Federal emission controls on motor vehicles should be bringing about a yearly reduction in ozone precursor emissions, these emission reductions are not large enough to account for the improvement in ozone levels.

As noted in the TSP section, there was a significant reduction in the frequency of southwesterly winds between 1977 and 1978. The larger portion of the peak ozone concentrations in Connecticut is caused by the transport of ozone and/or precursors (e.g., hydrocarbons and nitrogen oxides) from the southwest. The decreased frequency of levels in excess of the ozone standard is at least partially attributable to the decreased frequency of the southwesterly transport winds. Likewise, the decreased magnitude of the high ozone levels can be associated with changes in meteorology. Ozone production is greatest at high temperatures. In 1978, temperatures averaged between 1.5°F and 2.7°F less than in 1977. More importantly, the daily high temperatures in the summertime were much lower in 1978 than in 1977, as exemplified by a drop in the number of days exceeding 90°F from 26 (in 1977) to 12 (in 1978) at the Bradley Airport National Weather Service station.

#### Method of Measurement:

The DEP Air Monitoring Unit uses chemiluminescent instruments to measure levels of ozone. These instruments measure and record instantaneous concentrations of ozone continuously by means of a fluorescent technique. Properly calibrated, these instruments are shown to be remarkably reliable and stable.

# <u>Discussion of Data:</u>

Monitoring Network - In order to gather information which will further the understanding of ozone production and transport, as well as to provide real-time data for the daily Pollutant Standards Index, DEP operated in 1978 a state-wide ozone monitoring network consisting of four types of sites (see Figure 6):

Urban - Bridgeport, Derby, Hartford, Middletown, New Haven Advection from Southwest - Danbury, Greenwich Suburban - Enfield, Groton . Rural - Eastford, Hamden, Morris. New NAAQS - On February 8, 1979 the EPA established a new ambient air quality standard for ozone of 0.12 ppm. This standard replaces the old photochemical oxidant standard of 0.08 ppm. The definition of the pollutant was changed along with the numerical value partly because the instruments used to measure photochemical oxidants in the air really measure only ozone. Ozone is only one of a group of chemicals which are formed photochemically in the air and are called photochemical oxidants. In the past the two terms have often been used interchangeably. This 1978 Annual Summary uses the term "ozone" in conjunction with the new NAAQS to reflect the changes in both the numerical value of the NAAQS and its definition.

1-Hour Averages - The new 1-hour ozone standard was exceeded at all the DEP monitoring sites in 1978. The 2nd highest 1-hour average ozone concentrations were lower in 1978 than in 1977 at 11 of the 12 DEP ozone sites in Connecticut. Eight of these decreases exceeded 0.04 ppm. The 2nd highest hourly average increased at the 1 other site from 1977 to 1978, but this increase was less than 0.04 ppm. As stated earlier, this general decrease in measured ozone levels appears to have been primarily caused by the loss of much of the July, 1978 ozone data (see Table 19) and the drops in maximum temperature and the frequency of southwest winds from 1977 to 1978.

Table 19 shows a comparison between the number of days in 1978 with a maximum hourly ozone reading of greater than the old 0.08 ppm standard and the new 0.12 ppm standard. This table shows that in 1978 there were only 1/3 as many days exceeding the new 0.12 ppm standard as there were exceeding the old 0.08 ppm standard.

The monthly high ozone concentrations for the summertime "ozone season", and a tally of the number of times the hourly standard was exceeded, are presented in Table 20 for each site.

Table 21 shows the year's high and second high concentrations at each site.

10 High Days With Wind Data - Table 22 lists the maximum 1-hour ozone averages (and date of occurrence) from the 10-highest days for each ozone site in Connecticut for 1978. The wind data associated with these high readings are also presented. (See the discussion of Table 12 in the TSP section for a description of the origin and use of these wind data.)

Even more of the high  $0_3$  levels occurred on days with southwest winds than was the case with TSP and  $SO_2$ . This is expected because there are no local sources of ozone; it is all produced by photochemical reactions in the atmosphere. Since the urban areas to the southwest of Connecticut produce more ozone precursor emissions than all of Connecticut, it is not surprising that ozone levels are higher on southwest wind days than on all other days. However, it should be noted that bright sunshine and high temperatures are also needed to produce ozone. These conditions occur most often on southwest wind days, so it is the combination of pollutant transport and adverse meteorological conditions that produce the maximum ozone levels in Connecticut.

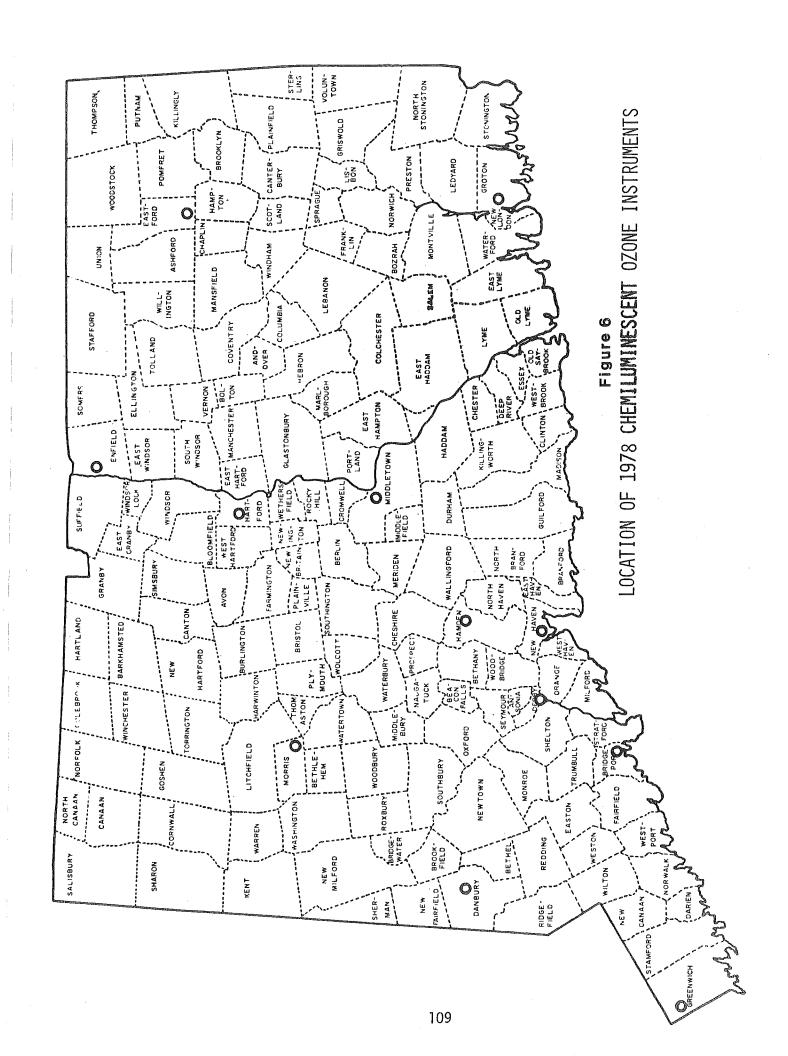


TABLE 19

NUMBER OF DAYS WITH 1 HOUR WHICH EXCEEDED THE OZONE STANDARDS (> 0.08 ppm/> 0.12 ppm)

1978

SITE	APRIL	МАҮ	JUNE	JULY	AUGUST	SEPTEMBFR	TOTA
Bridgeport-123	0/0	10/2	3/1*	4/3*	12/1	4/2	33/9*
Danbury-123	1	12/5*	4/1*	*0/0	10/3	5/1	31/10*
Derby-123	0/0	5/5	14/8	*0/1	*1/6	5/5	34/13*
Eastford-001	13/2*	17/4	15/2	4/2*	*0/1	4/1	54/11*
Enfield-123	2/0	18/4	9/01	-/-	3/2	2/1	35/13
Greenwich-004	2/0	8/3	*9/6	*9/8	11/3*	3/1*	42/18*
Groton-123	*0/0	*0/0	E	3/1*	8/4	8/1	*9/6[
Hamden-001	÷0/0	*1/1	15/7	-/-	*0/0	3/1*	*6/6
Hartford-123	1/0	8/2*	8/6	11/8	5/2	3/2	37/17
Morris-001	¥0/0	7/2*	*0/0	_/_	3/2*	4/0	14/4*
Middletown-003	*0/0	6/2	*2/9	1/1	2/1	5/3	22/8*
New Haven-123	*0/0	8/3	12/5*	7/4*	7.0	3/1	37/13

<sup>\* &</sup>lt; 75% of the data available

No data available

TABLE 20

1978 HIGHEST. 1-HOUR OZONE VALUES BY MONTH, PPM

# OF TIMES STANDARD EXCEEDED	28*	36*	41*	28*	48	×92	27*	37*	51	10*	<b>50</b> *	45
SEPTEMBER	.137	.150	.173	.188	.144	.130*	.135	.230*	.154	011.	.180	.132
AUGUST	.123	.159	.125	.115*	.133	.235*	190	*070*	.144	.150*	.138	.118
JULY	.203*	*690°	*087*	*150*	*	*500*	*149*	* *	.215	* *	* *	.225*
JUNE	.125*	*171*	.253	.130	.177	.250*	* *	. 245	.139	*070*	.147*	.230*
MAY	.201	.233*	.143	.209	.162	.200	.074*	*170*	.145*	.186*	.162	.183
APRIL	620.	`* *	020.	.155*	.105	.120	.054*	*690.	.110	*690.	*9/0	.064
SITE	Bridgeport-123	Danbury-123	Derby-123	Eastford-001	Enfield-123	Greenwich-004	Groton-123	Hamden-001	Hartford-123	Morris-001	Middletown-003	New Haven-123

r < 75% of the data available

<sup>\*\*</sup> No data available

TABLE 21

1978 MAXIMUM 1-HOUR OZONE CONCENTRATIONS

·	DATE	*	CONCENTRATION
SITE	1ST HIGH	2ND HIGH	(parts per million) .12 0 .100 .200 .300 .400
Bridgeport-123	7/21/15	5/20/16	203
Danbury-123	5/31/14	5/31/15	233
Derby-123	6/27/17	6/27/16	253 200
Eastford-001	5/20/20	5/20/19	209 193
Enfield-134	6/27/17	6/27/18	177 167
Greenwich-004	6/19/15	6/19/14	250 240
Groton-123	8/15/17	8/15/16	190 174
Hamden-001	6/27/17	9/21/16	245
Hartford-123	7/21/17	7/21/18	215 202
Morris-001	5/31/15	5/31/16	186 184
Miadletown-003	9/21/16	5/20/18	180 162
New Haven-123	6/19/14	7/21/15	230 225
			Primary Standard

<sup>\*</sup> Date is read as month/day/hour of occurrence

ENVIROMENTAL PROTECTION

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CONNECTICUT DEPARTMENT

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CONNECTICUT	DEPARTMENT OF	ENVIRONENTAL F	PROTECTION	Z						AIR COMP	COMPLIANCE ENG	engineering
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L. W	ENFIELD METEOROLOGICAL SIT	RATIO 123 165 E DIR (DEG) J. VEL (MPH)	0.889 0.177 6/27/78 4.6	0.974 0.162 5/20/78 210 9.0	8 7520	~ 4~ C ·		00 4.←U·	4 40W·	Q) ~~~~Q)	0.610 0.132 6/11/78 170 8.0	
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air compliance engineering

CONNECTICUT DEPARTMENT OF ENVIRONENTAL PROTECTION

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RATIO DIR (DEG) VEL (MPH) SPD (MPH) RATIO DIR (DEG) VEL (MPH) SPD (MPH) RATIC DIR (DEG) VEL (MPH) SPD (MPH) RATIC DIR (DEG) VEL (MPH) SPD (MPH) RATIO DATE
DIR (DEG)
VEL (MPH)
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VEL (MPH)
RATIO
DIR (DEG)
VEL (MPH)
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SPD (MPH)
RATIO SITE SAMPLES SITE S.TE SITE CONN. SITE CONN. SITE CONN. SITE CONN. SITE CONN. SITE MASS. SITE N. J. METEOROLOGICAL BRIDGEPORT METEOROLOGICAL NEWARK METEOROLOGICAL BRADLEY FIELD MET EOROLOGICAL WORCESTER METEOROLOGICAL BRADLEY FIELD METEOROLOGICAL WORCESTER MET EOROLOGICAL NEWARK METEOROLOGICAL BRIDGEPORT METEOROLOGICAL BRADLEY FIELD METEOROLOGICAL BRIDGEPORT POLLUTANT--OZONE MIDDLETOWN NEW HAVEN

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NGINEERI	R WILLIG	5	250 7.7 9.989
AIR COMPLIANCE ENGINEERING	UNITS : PARTS PER MILLION	മ	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
AIR COM	CALTS :	œ	0.88.57 88.55 88.55
		-	270 7.4 8.3 8.3
	DATA	ဖ	0.6 4.6 6.5 6.5 6.6
	TH MET.	ហ	0.52 0.50 0.50 0.00
	/S 1978 ₩	4	230 10.1 10.1
	AVG D3 DAY	์ M	270 2.7 6.2 0.440
N.	TEN HIGHEST 1 HR AVG 03 DAYS 1978 MITH MET. DATA	8	250 7.4 7.8 0.954
ROTECTION	EN HIGH	-	260
TALP	<b>}</b> —	PLES	M PH ()
ROMEN		SITE SAMPLES	DIR (C VEL (N SPD (N
ENVI		SIT	ITE ASS.
CONNECTICUT DEPARTMENT OF ENVIROMENTAL PROTECTION	POLLUTANTOZONE	TOWN NAME	METEOROLOGICAL SITE DIR (DEG) WORCESTER MASS. VEL (MPH) SPD (MPH) RATIO
8	5		

### V. NITROGEN DIOXIDE

## Conclusions:

Measured nitrogen dioxide levels at all sampling sites in Connecticut were lower than the National Ambient Air Quality Standard of 100  $\mu g/m^3$ , annual arithmetic mean. A statistical analysis of the data also demonstrates, with 95% confidence, that every site achieved the annual NAAQS for NO2.

A small improvement in  $NO_2$  levels took place between 1977 and 1978 (see Table 4). Since 60% of the  $NO_2$  emissions in Connecticut come from motor vehicles, some of this improvement could be attributable to the Federal emission control program for motor vehicles, but most of the improvement is probably due to the meteorological changes noted in the discussions of the other pollutants.

# Sample Collection and Analysis:

The DEP Air Monitoring Unit uses gas bubblers employing the NASN Sodium Arsenite method. These instruments sample for twenty-four hours every sixth day, the same schedule as the suspended particulate instruments. The samples are later chemically analyzed in the laboratory.

# Discussion of Data:

Monitoring Network - There were 23 nitrogen dioxide sites in 1978 as compared to 24 in 1977. The sites were distributed in a network which covers urban, residential and suburban locations (see Figure 7).

Historical Data - The DEP's historical file of annual average nitrogen dioxide data for 1973-1978 is presented in Table 23. The complete historical file is presented because some minor corrections have been made to some of the data published in earlier Annual Summaries. The data presented in this 1978 Annual Summary replace all previous compilations. Also, if minimum EPA sampling requirements were not met in a given year at a given site, an asterisk now appears next to the number of samples taken at that site.

Annual Averages - The annual average NO<sub>2</sub> standard was not exceeded in 1978 at any site in Connecticut. In 1978, of the sites that had sufficient data to compute valid arithmetic means, 5 sites showed higher annual means than in 1977, with 2 of these increases being greater than 5  $\mu g/m^3$ . In 1978, 14 sites showed lower annual means than in 1977, with 7 of these decreases being greater than 5  $\mu g/m^3$ . Thus, these results indicate that there has been a general statewide decrease in NO<sub>2</sub> levels. A continuation of this trend would enhance efforts to maintain the NAAQS for Nitrogen Dioxide.

Statistical Projections - The format of Table 23 is the same as that used to list the total suspended particulate data. Note that although the distribution of  $NO_2$  data tends to be lognormal, the annual arithmetic mean is shown for direct comparison to the NAAQS for nitrogen dioxide. The 95 percent limits and standard deviations are also arithmetic calculations, but the geometric means and standard deviations were used

to give accurate predictions of the number of days the levels of 100  $_{\mu g/m^3}$  and 282  $_{\mu g/m^3}$  would be exceeded at each site if sampling had been conducted on a daily basis. Although there is no 24-hour NAAQS for NO $_2$  the 282  $_{\mu g/m^3}$  level was selected for this presentation because at this level a 1st stage air pollution alert is to be declared according to the State of Connecticut's Administrative Regulations for the Abatement of Air Pollution. The 100  $_{\mu g/m^3}$  level was selected to provide an indication of how many days per year the annual NAAQS may have been exceeded if sampling was performed daily.

10 High Days With Wind Data - Table 24 contains the 10 highest daily  $NO_2$  readings for each site in 1978 along with the associated wind conditions. (See the discussion of Table 12 in the TSP section for a description of the origin and use of these wind data.)

As with the other pollutants,  $NO_2$  levels were high most often when the winds were southwesterly. But, more so than the other pollutants,  $NO_2$  levels were high on non-persistent southwest wind days. Although some  $NO_2$  is emitted directly by fuel burning sources, much  $NO_2$  is formed in the atmosphere. Once again, it appears that a combination of pollutant transport and otherwise adverse meteorological conditions tend to produce high  $NO_2$  levels on southwest wind days.

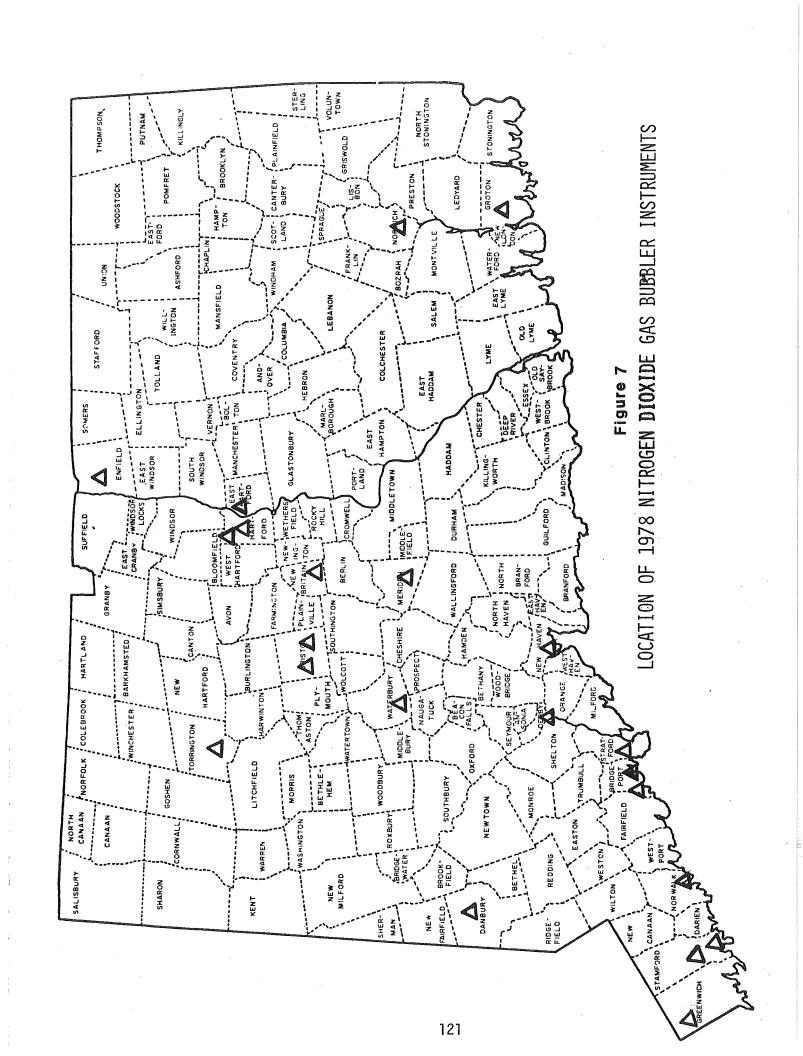


TABLE 23 1973-1978 NO-

		TABLE 23	3 1973-1978	NO2, ANNUAL	AVERAGES AND		STATISTICAL PROJECTIONS	, 01	
CONNECTICUT	DEPARTM	ENT OF	ENVIRONMENTA	L PROTECT	NOI	PAGE	1 AIR	COMPLIANCE	MONITORING
POLLUTANTNITROG	IITROGEN	OIXOIO	·					DISTRIBUTIOM-	LJGNDRMAL
					7 70 - 2	T + 47		REDICTE	REDICTE
TOWN NAME	SITE	YEAR	SAMPLES	ARI. MEAN		J.	STD DEVIATION		
0	ć	1							
וו איל ריי	TO	<u>ب</u> ا	<b>က</b> ် က	2			3.26	59	2
BERLIN	01	1974	55	17.3	17	17	15,498	4	
ER F	01	6	51	<b>°</b>			8.06	20	
E &	01	97	13*	6			4.30	24	
IDGEPUR	01	97	26*	4.			3.67		
BRIDGEPURT	01	1974	09	57.1	57	57	22.824	20	
IDGEPUR	01	16	56	ဆို			5.25		
IDGEPOR	01	26	57	9			1.26		2
IDGEPÜR	01	4	57	4.			6.27		
IDGEPOR	0.0	26	61	4			1.82		
IDGEPUR		76	*62	4			4.95		α
BRIDGEPURT	03	1975	45%	7.7	72	<b>~</b>	27.710	V 40	o
IDGEPUR		16	3	2.		63	0.21	29	
RIDGEPOR	7	97		2			3.05		
RIDGEPOR	2	16		o			16.6		
BRIDGEPORT	123	1977	58	72.5	7.2	72	26.607	. J.	
RIDGEPOR	2	26		• 9			ප <b>ි</b> ට න		
RISTO	10	97		51.9			9.45		
RISTO	01	25		3			3.63		2
BRISTOL	01	1975	47	47°1	47	47	21.087	16	
アント	T O	7		7			1.39		
RISTO	10	16		6			09.6		
K1510	01	9 /		ဆ			2.04		
BRISTOL	0.5	1973	19*	36.7	37		4.09		
RISTO		26		• 9	27	2.7	20.149	13	7
BRISTOL	03	1973	19*	43.2	43		2.40		
RIST		97		Q	59	58	19.652	13	. 1

CONNECTICUT DEPARTMENT	PARTM	ENT OF	ENVIRONMENTAL		TABLE 23 (CONTINUED PROTECTION	ED) PAGE	2	AIR	COMPL IANCE	MONITORING
POLLUTANTNITROGEN	ROGEN	DIOXIDE	)E			,	•	Q	ISTRIBUTION-	IBUTIONLOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES	ARI. MEAN	9.5-PCT- LOWER	LIMITS UPPER	STD DEVI	ATION	PREDICTED DAYS OVER 100 UG/M3	PREDICTED DAYS OVER 282 UG/M3
BRISTOL BRISTOI	04	1973	19%	54.0	43	6.5	اب ال	57	50	2
BRISTOL	040	1975	74	) (	7 4	5 6	7 0 7		+ v	,-
BRISTOL.	40	1976	14%		_	16	7 0 7			•
BURLINGTON	01	1973	*95	12.8	10		1 .4	99		
BURLINGTON	01	1974	58	12.3	6		3.2	14	2	
BURLINGTON	10	1975	51	18.0	71	22	7		. 7	
BURLINGTON	01	1976	*6	8 °6	w į		8			
COLCHESTER	01	1973	09	<b>†•†</b>	38	51	6.1	29	59	pisote
COLCHESTER	01	1974	09	reed	28	35	6.	37	~ <b>-</b>	ſ
COLCHESTER	0	1975	26	37.0	34	40	р-чі 0	21	7	
COLCHESTER	01	1976	10*	~	22	45	6.0		m	
DANBURY	01	97	25*	35.2	25	45	5 • 3	31	29	2
DANBURY	01	1974	52	45.0	38	55	æ	45	59	
DANBURY	10	1975	*6	5	31	100	5 . 4		29	m
DANBURY	123	1975	48*	44.0	39	64	7.2	94	4	
DANBURY	123	1976	57	41.1	35	47	23.1	55	24	
DANBURY	123	1977	61	Ŝ	21	59	7.2	84	8	
DANBURY	123	1978	57	55.8	51	19	1.2	47	20	
DANBURY 01/	123	1975	57	47.5	41	45	25.3	56	10	
DERBY	123	1976	56		46	58	3.0	71	24	
DERBY	123	1977	09		53	<b>64</b>	6	09	24	
DERBY	123	1978	444	53.7	48	65	8 .9	92	K)	
EAST HARTFORD	01	1.974	43%	7	52	63				
EAST HARTFORD	01	1975	56	63.2	25	69	24.6	17	35	
<u></u>	10	1976	13%	o	56	26	s S			<b>-</b> 4
EAST HARTFORD	05	1973	20*	61.3	20	72	24.4	460	53	

CONNECTICUT DE	DEPARTMENT	O P	ENVIRONMENTAL	TABLE 23 PROTECT	(CONTINUED) ION	ED) PAGE	m	AIR	COMPLIANCE	MONITORING
POLLUTANTNITROGEN	rrogen	DIOXID	·		. •			O	STRIBUTION-	-LOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES	ARI. MEAN	95-PCT- LOWER	-LIMITS UPPER	STD DEVIA	TION	PREDICTED DAYS GVER 100 US/M3	PREDICTED DAYS OVER 282 UG/M3
EAST HARTFORD EAST HARTFORD	02	1974	61	52°3 54°6	4 4 8 8	57	19.25	9 1	0 4	
ST HAR	02	16					7.46	2		
ST HAR	02	161		6			1.15	6		
N HAH	02	16		<b>~</b>			2.46	0		
EAST WINDSOR	01	1975	33*	4.			8.13	2		
AST WIND	01	16		60.2	44	76	26.74	0	29	
ENFIELD	$\sim$	1975	45%	46.6	41	53	0.27	gament.	α	
ENFIELD	7	1976	61	4.	,40	20	1.36	ı v	) [~	
ENFIELD	123	1977	65	55.0	50	9	90	6	16	
ENFIELD	2	1978		2 °	47	58	2.77	6	20	
GREENWICH	01	~		4		125	1.01	9	139	α
GREENWICH	01	6	58	ς, e		Ç	8.56	2	9	10
GREENWICH	01	1975	54	36.5	29	<b>55</b>	(1)		10	
GREENWICH	01	6		3		82	6.32	7	7.7	2
GREENWICH	01	97	45%	ις N		16	0.32	3		end
GREENWICH	04	16	*65	2.	56	89	1 .2	9		4
GREENWICH	04	16	59	9	3,4	46	3.5	5		· m
GREENWICH	04	1975	22	53.4	47	9	25.23	3	35	
GREEN¥ICH	40	97	57	3	48	09	6.3	3		
GREENWICH	40	1977	59	ထ	43	54	2.6	<b>-</b>		
GREENWICH	40	97	09	6	35	44	8 .0	2	80	
GREENWICH	08	1976	54	35.9	32	40	5 8	6	2	
EENWIC		16	14%	ိ		38	11.79	6		
GROTON	01	1973	57	44.5		55	9.51	9	35	2
GROTON	01	1974	61	0	32	41	13.64	4	~	
GROTON	01	97	24%	38.4		46	7.54	S	'n	
GROTON	123	1975	34%	44.8	40	. 50	15,73	<b>\$</b>	æ	

CONNECTICUT DE	DEPARTMENT		OF ENVIRONMENTAL	<b></b> Δ-	ABLE 23 (CONTINUED) RCTECTION	D) PAGE	4 AIR	COMPLIANCE	MONITORING
POLLUTANTNITROGEN	rROGEN	DIOXID	)E				Q	ISTRIBUTION-	LOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES	ARI. MEAN	95-PCT- LOWER	-LIMITS UPPER	STD DEVIATION	PREDICTED DAYS OVER 100 UG/M3	PREDICTED DAYS OVER 282 UG/M3
GROTON GROTON GROTON	123 123 123	1976 1977 1978	58 60 61	41.6 49.7 46.2	38	45 54 51	14.171 18.152 21.707	4 10 16	
GROTON 01/	123	1975	58	42.1	38	94	16.808	2	
HARTFORD HARTFORD	02	1973	35* 60	63.1	59	67	13.293	4 C	^
HARTFORD	. 02	97	56	Ö		67	5.48	29	J
HARTFORD	05	76	58			64	2.12	35	
HARTFORD HARTFORD	02	1977	54 45*	56°1 49°1	50 41	62 58	23.461	29 80 80	Ŋ
HARTFORD	03	1978	*6	81.6	55	108	35.261	88	
HARTFORD	123	1975	34%	76.5	67 50	85	27.038	rv r es es	
HARTFORD	123	1977	70	را ال 6 و	69	101	7 0 0 7 7	2001	, policy
HARTFORD	123	1978	61		69	84		19	•
KENT	01	1973	27*	16.1	12	. 21	0		
KENT	01	1974	57	40	12	7	0.47	r=4	
KENT	01	1975	4	19.4	9=	23	0.		
LITCHFIELD	01	1973	÷65	2	34	50	30.297	24	<b>, rd</b>
LITCHFIELD	01		65	30.3	26	35	8.1	13	
LITCHFIELD	01	1975	55	ις e	30	41	.05	4	
LITCHFIELD	01	16	13*	ထိ		48	5 0	4	
MANSFIELD	01	1974	32*	28.7	24	34	3.94	4	
MANSFIELD	10	1975	57	31.6	28	35	S.	2	•
MANSFIELD	01	1976	*	35.1	54	47	.43	2	
MANSFIELD	02	1973	÷L5	32.2	26	38	.89	10	
EL		97	20*	9			1 • 62	;==4	

CONNECTICUT DEPARTMENT	EPARTM		OF ENVIRONMENTAL	TABLE 23 PROTECT	(CONTINUED)	D) PAGE	9	AIR	COMPLIANCE	MONITORING
POLLUTANTNITROGEN	TROGEN	DIOXID	· W					Q	ISTRIBUTION-	LOGNORMAL
TOWN NAME	SITE	YEAR	SAMPLES	ARI. MEAN	95-PCT- LOWER	-LIMITS UPPER	STD DEV	DEVIATION	PREDICTED DAYS OVER 100 UG/M3	PREDICTED DAYS OVER 282 UG/M3
NEW HAVEN	10	1977	39*	75.3	68	83	24.	377	58	
NEW HAVEN NEW HAVEN NEW HAVEN	123 123 123	1976 1977 1978	57 58 61	78.6 78.6 82.1	71 71 74	86 86 90	200 000 000 000 000	813 706 306	67 77 88	
NORWALK	05	1973	54		94 72		4 ~	647	168	2
NORWALK	0 0 0	5161	) <u>(</u>	j m,	7		e.e 4.√0⊔	901		LN P
NORWALK NORWALK NORWALK	000	1977	55 61	74°1 76°1	99 26 26	83 73	31.	750 159 445	67 67 50	<b>∞4</b>
NORWICH NORWICH NORWICH NORWICH	01 01 01	1973 1974 1975 1976	54 61 58 59	62.9 45.0 43.0 51.0	5 4 4 4 4 6 9	488 50 50 50 50 50	35. 18. 17. 18.	295 562 119 365	58 10 2 8	<b>2</b>
NORWICH OLD SAYBROOK OLD SAYBROOK OLD SAYBROOK OLD SAYBROOK	01 01 01 01	1978 1973 1974 1975	59 19* 61 59 11*	8. 0. 0. 0.	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	54 75 76 76 64	0 00 6	09 49 65 09 93	13 . 67 58 8	<b>4 4</b>
PUTNAM PUTNAM PUTNAM	02 02 02 02	1973 1974 1975 1976	44* 61 55 13*	42.8 28.3 39.1 34.2	35 25 34 22	51 31 44 46	28. 12. 21.	029 870 028 858	32 - 23	2
STAMFORD STAMFORD	03	1973	51 10*	83.1 60.1	65 48	101	67° 17°	849	100	10
STAMFORD STAMFORD	07	1974	<b>49</b> *	29.0 52.3	20	38	33° 8° 8° 8° 8° 8° 8° 8° 8° 8° 8° 8° 8° 8°	094	20	5

TABLE 23 (CONTINUED) CONNECTICUT DEPARTMENT OF ENVIRONMENTAL PROTECTION PAGE	Ë	7	AIR COMPLIANCE MONITOR
POLLUTANTNITROGEN DIOXIDE			

CONNECTICUT DE	DEPARTMENT	J.	ENVIRONMENTA	L PROTEC	TION	D) PAGE	7 AIR	R COMPLIANCE	MONI TORING
POLLUTANTNITROGEN	ROGEN	DIOXID	w				_	OISTRIBUTION-	
TOWN NAME	SITE	YEAR	SAMPLES	ARI. MEAN	95-PCT-LOWER	-LIMITS	STO DEVIATION	PREDICTED DAYS OVER	PREDICTED DAYS OVER
( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( )					) ; )	J	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7		82 U6/M
SIAMFURU	0.	1976	26	3,			4.87		-
- タゴトロスト	0 \	26	57	6*59	58		9.73		4
I AMFUR	0 2	26	19	0	53	89	31.198	200	<b>d</b> p=4
	0	0	C	r					
	1 (	- 1		6		72	0.79		
N-AMFOKO N-AMFORO	123	\$	57	71.6	49	4	\$	19	
- ASTOX				0		68	3.37		
1 A 2 T D X	7	<u>_</u> 6		-4			2.22		~
APPLOR	V	6		ίζ.			8.53		ł
TRATFOR		1973	52%	. 4	44	0.7	,	;	
TRATFOR		97	ıç	) }	3 5	- ( 1 0	1000	<i>}</i> }	
TRATEOR		, ,		e - (	70	5	7/00	35	
		) (	00	2	65	78	7.51	58	
	ς Σ (	9161	58	69.1	62	76	7.55	58	
LKALTUK HOAHROO		6	56	ري ه	47	09	7.49	42	-
IKAIFUR	0 2	97	19	က္	51	99	33,257	50	
								•	4
TORRINGTON	01	16	÷05	•		62	7.72		-
RR	0.	1974	61	37.0	33	41	8.66		₩.
R.R.		26	29%	9	41	57	21.674	5 7	
. 0	C	7	(						
TORRINGTON	122	1975	/ C &	40°V	40 ()	53	18.413	∞	
	<b>J</b> (	7 (	70	•	43		8.25	'n	
	7	1767	09	•	50		8.47		
Y Y	V	<u></u>	ر 8	ထိ	44		8 • 30	10	
TORRINGTON 1/	123	1975	57	47.8	43	53	20.180	10	
VOLUNTOWN		76	24	ις.		2.3	,		
ZOLUCION		0.7	- ca	- 1	<b>,</b> 4	7 0	700	C .	
N3CHNI ICA	5 2	1075	0 0	e	) .	7,0	11.103		
		- F	V I	<b>O</b>	16	56	6.76		
N O L O L O N O		<u>~</u>	*Z T	2		28	•88		
WATER BURY	01	1973	28*				3.19		
WATERBURY	01	16		63.7	57	70	25.709	52	2
									l

	CONNECTICUT DEPARTMENT	)EPARTM	ENT OF	OF ENVIRONMENT	TABLE 23	(CONTINUED ION	D) PAGE	8 AIR	COMPLIANCE	MONITORING
	POLLUTANTNITROGEN	I TROGEN	DIOXIDE	ш					ISTRIBUTIONLOGNORMAL	LOGNORMAL
	TOWN NAME	SITE	YEAR	SAMPLES	ARI. MEAN	95-PCT- LOWER	-LIMITS UPPER	STD DEVIATION	PREDICTED DAYS OVER 100 UG/M3	PREDICTED DAYS OVER 282 UG/M3
	WATERBURY	01	1975	18*	46.8	36	57	21.562	20	
	WATERBURY	05	1974	20*	30.4	24	37	14.789	20	П
	WATERBURY	02	1975	28	47.1	45	55	1.13	20	
	WATERBURY	05	1976	13*	57.7	44	72	3.54	24	
	WATERBURY	03	1975	20	56.3	64	49	9 • 33	42	
	WATERBURY	03	1976	13*	61.4	37	86	41.355	50	~
	WATERBURY	123	1975	40%	68.1	63	73	7.78	20	
	WATERBURY	123	1976	9	65.6	9	7.1	3	50	
	WATERBURY	123	1977	61	71.9	19	11	1.07	42	
	WATERBURY	2	1978	09	0	64	75	3.68	50	
	WILLIMANTIC	01	1973	50%	54.5	47	61	26.9	29	
~ ~	WILLIMANTIC	01	1974	61	42.0	37	47	19.570		
	WILLIMANTIC	01	1975	59	43.3	40	47	5.86	2	
	WILLIMANTIC	01	1976	10*	41.9	30	53	16.208	80	

SAMPLING NOT RANDOM OR OF INSUFFICIENT SIZE FOR REPRESENTATIVE ANNUAL STATISTICS.

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	<b>С</b> Ж	<b>o</b> n	~ o.ru	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	77 0	84.0.0	0 4 4 0 0	0 6	<b>ωω • ο</b> ο	2/13/78 240 2.5 5.5 6.465
	MICROGRAMS	. 60	← 4 Cl	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	ល្យល • • ០	± + 9.€	0 0 0 0	•	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0/11/70 0.00 0.00 0.00 0.00 0.00 0.00
	WITS :	. ~	272	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	94.00	24 7. 96	$- \circ \circ \circ \circ \cdot \circ \circ$	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	W	8/ 5/78 330 330 3.5 3.5 3.5 3.5 3.5 3.5 3.5 3.5 4.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5
DATA		ω	<b>UWU</b>	0.0 0.938 0.030 0.01	0 4	4	. O - 00 · · -		n ← · · /~	3/21/78 180 180 5.4 8.9
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CONNECTICUT DEPARTMENT OF ENVIROMENTAL PROTECTION

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CONNECTICUT DEPARTMENT OF ENVIROMENTAL PROTECTION

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CONNECTICUT DEPARTMENT OF ENVIROMENTAL PROTECTION

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3 2	METEOROLOGICAL WORCESTER HAVEN	MASS.	DIR VEL SPD RATI	MPH)	· • • ·	.92. 65. 82.	12 - 3 t . 4 5	2 w w o r		2 4 2 C		20000 - 7		. war
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5/20/78 11/10/78 210 90 24 HR AVG NOZ DAYS 1978 WITH MET. DATA 230 8.0 8.0 200 200 7.3 0.870 0.870 0.870 5.3 'n 114 2/13/78 240 123 3/21/78 180 23 61 134 126 DATE 10/23/78 12/16/78 DIR (DEG) 270 210 240 8.5 0.778 0.778 3.1 3.4 0.888 0.888 5.7 0.927 N TEN HIGHEST CONNECTICUT DEPARTMENT OF ENVIROMENTAL PROTECTION VEL (MPH)
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METEOROLOGICAL SITE NEWARK N. J. METEOROLOGICAL SITE BRIDGEPORT CONN. METEOROLOGICAL SITE BRADLEY FIELD CONN.	OATE (DEG) (MPH) (MPH) (MPH) (MPH)	10/23/78 270 11.2 0.662 12.5 16.5 16.2 310 310 3.6 0.444	12/16/78 210 7.6 8.0 0.938 240 8.5 10.9	3/21/78 180 5.4 8.9 0.610	2/13/78 240 2.5	5/20/78 1 210 9.0	11/10/78 90 2.3	9/11/78 220	7/19/78 200 6.6	8/24/78 240	6/13/78 270	
SITE SITE CONN.	DIR (DEG) NEL (MPH) SPD (MPH) RATIO DIR (DEG) VEL (MPH) SPD (MPH) DIR (DEG) VEL (MPH) SPD (MPH) SPD (MPH)		210 7.6 8.0 8.0 240 8.5 0.9	180 5.4 8.9 0.610	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	9.0		10.4	8 8 6	240	270	
SITE CONN.	VEL (MPH) SPD (MPH) RATIO DIR (DEG) VEL (MPH) SPD (MPH) AATIO RATIO		7.6 8.0 9.938 2.40 8.5 10.9	5.4 8.9 610	2.0	0.6		10.4	9	c	i t	
SITE CONN. SITE CONN.	SPD (MPH) RATIC DIR (DEG) VEL (MPH) SPD (MPH) RATIC DIR (DEG) VEL (MPH) SPD (MPH) RATIC	0.0562 1.2.05 1.6.2.2 1.0.05 1	8.0 .938 240 8.5 10.9	8.9 0.610	c					¥.	חי. י	
SITE CONN.	RATIC DIR (DEG) VVEL (MPH) SPD (MPH) RATIC NVEL (MPH) SPD (MPH) SPD (MPH)	0.662 2.67.0 3.77.0 3.8 3.0 6.8 4.2 6.8 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0 6.0	0.938 240 8.5 10.9	0.610	ŋ.	8.6		10.6	7.8	7.0	4.2	
SITE CONN.	DIR (DEG) VEL (MPH) SPD (MPH) RATIC DIR (DEG) VEL (MPH) SPD (MPH) RATIC	2.50 2.77 3.60 3.60 2.444 2.60 2.60 2.60 2.60 2.60 2.60 2.60 2.60	240 8.5 10.9 0.778		0.465	0.924		0.977	0.851	881	0.637	
SITE CONN.	VEL (MPH) SPD (MPH) RATIC DIR (DEG) VEL (MPH) SPD (MPH) RATIC	2.5.0 3.00.0 3.00.0 444.0 0.00.0	8.5 10.9 0.778	190	230	220		220	230	06	260	
SITE CONN.	SPD (MPH) RATIO DIR (DEG) VEL (MPH) SPD (MPH) RATIO	0.77.0 0.470 0.83.0 0.84.2	10.9 0.778	4.2		10.0		15.8	n 4	4	ි <b>ග</b>	
SITE CONN.	RATIO DIR (DEG) VEL (MPH) SPD (MPH) RATIO	0.00 0.00 0.00 0.00 0.00 0.00 0.00	0.778	11.8	7.6	10.6		16.1	0.0	თ. თ	12.0	
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CONN.	VEL (MPH) SPD (MPH) RATIO	0 8 4 4 6 8 .0 0 0 0 4 4 2 0 0	190	170	310	210		190	200	20	240	
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		300 200	0.888	0.954	0.803	0.872		0.925	0.870	0.665	0.621	
SITE	DIR (DEG)	C	260	210	300	270		230	250	9	250	
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	SPD (MPH)	12.9	6.2	10.5	7.5	ლ ლ		8.6	ற ம	8	10.0	
	RATIC	0.866	0.927	0.975	0.812	0.889		0.955	9969	<b>6.888</b>	0.866	
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		9:638	0.924		0.939	0.440	0.637	0.493	0.881	9.938	0.414	
SITE	DIR (DEG)	240	220		240	180	260	200	06	230	260	
BRIDGEPORT CONN.			10.0		4.4	3.1	ю. В	2.5	4.2	6.5	8.8	
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SITE	DIR (DEG)	190	210		190	170	240	180	50	210	360	
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	RATIO	0.888	0.872		0.902	0.494	0.621	0.835	0.665	0.826	0.316	

CONNECTICUT DEPARTMENT OF ENV	ENVIROMENTAL PROTECT	AL PR	OTECTION	· <b>7</b> 2	•					AIR COMP	COMPLIANCE EN	engineering
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### VI. CARBON MONOXIDE

### Conclusions:

The eight-hour NAAQS of 9 ppm was exceeded at eight of the nine carbon monoxide monitoring sites in Connecticut (Bridgeport 004, Greenwich 001, Hartford 012, New Britain 002, New Haven 007, Norwalk 005, Stamford 020, and Waterbury 004) in 1978. The number of times the 8-hour standard was exceeded ranged from twice each at the Greenwich 001 site and the New Haven 007 site up to 104 times at the New Britain 002 site and 366 times at the Stamford 020 site. Hartford 009 was the only site that did not exceed this standard. No site, except Stamford 020, violated the one-hour standard of 35 ppm. The one-hour standard was exceeded seven times at the Stamford 020 site in 1978.

No significant change in carbon monoxide levels took place between 1977 and 1978.

In order to put the monitoring data into proper perspective, it must be realized that carbon monoxide concentrations vary greatly from place-toplace. More than 95% of the CO emissions in Connecticut come from motor vehicles, so concentrations are greatest in areas of traffic congestion. The magnitude and frequency of high concentrations observed at any monitoring site are not necessarily indicative of widespread CO levels. Thus, most locations in New Britain, Norwalk and Stamford are probably not experiencing CO levels as high as those observed at the monitoring sites in those towns. On the other hand, there are probably locations in Bridgeport, Greenwich, Hartford, New Haven, and Waterbury where CO levels are higher than those observed at the monitoring sites in those towns. The CO standards are likely to be exceeded in any city in the State where there are areas of traffic congestion. As Federally-mandated controls reduce emissions from new motor vehicles (and as Connecticut's SIP control strategies are implemented) there should be a decrease in the number of such areas; and the remaining areas should be shrinking in territory and have levels which are less in excess of the standards.

#### Method of Measurement:

The DEP Air Monitoring Unit uses instruments employing a non-dispersive infrared technique to continuously measure carbon monoxide levels. The instantaneous concentrations are recorded on strip charts from which hourly averages are extracted. The instruments are fairly insensitive to sampling line length. Concentrations vary dramatically with inlet exposure and proximity to traffic lanes.

## Discussion of Data:

Monitoring Network - The network in 1978 consisted of 9 carbon monoxide monitors (see Figure 8). The Hartford 009 site was replaced by the Hartford 012 site in November and two other sites were discontinued in 1978 (Greenwich 001 and Waterbury 004).

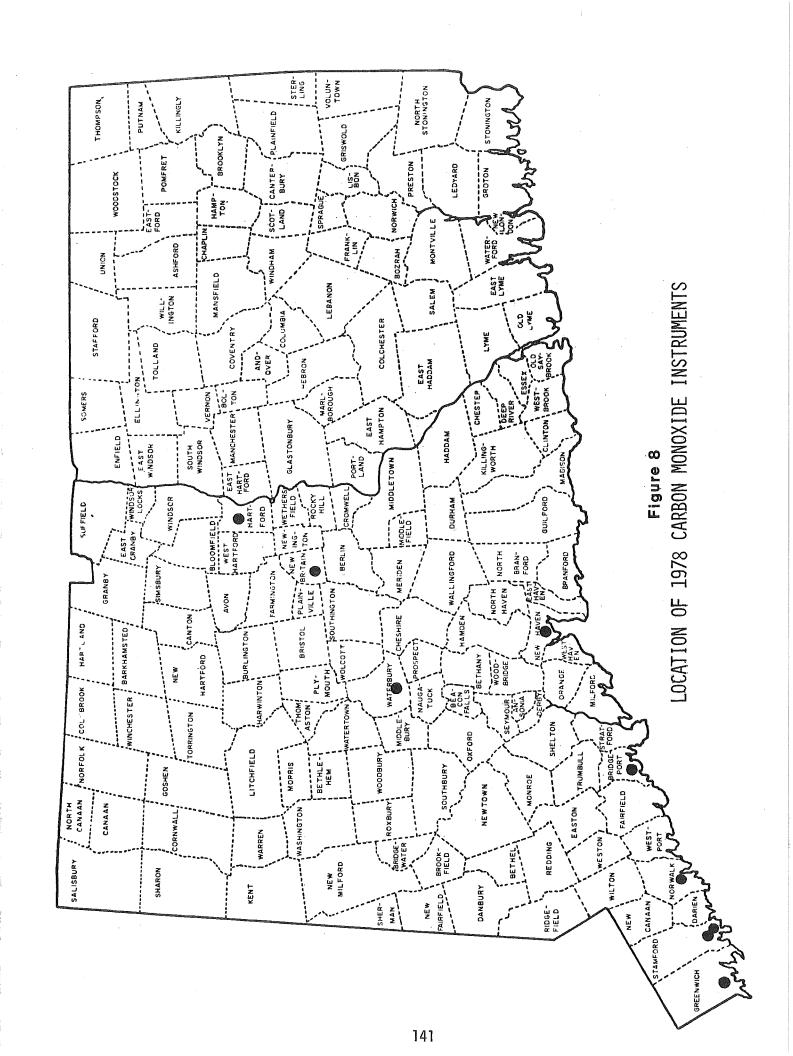
8-Hour and 1-Hour Averages - In general, CO levels recorded in 1978 were not significantly different from those recorded in 1977. Most sites recorded CO levels which exceeded the 8-hour standard while only 1 site (Stamford 020) recorded CO levels higher than the 1-hour standard. Table 25 gives the high and 2nd high 8-hour and 1-hour CO readings (and time of occurrence) for each site. Four sites recorded higher second high 8-hour average concentrations, while 3 sites recorded lower second highs, in 1978 compared to 1977. The second high 8-hour average at one site (New Britain 002) didn't change. The second high 1-hour average concentration increased at 3 sites and decreased at 5 sites between 1977 and 1978.

Table 26 presents monthly first highs and a tally of the number of times the standards were exceeded at each site. Seasonal variations in CO levels can be observed using this table.

10-High Days With Wind Data - Table 27 lists the maximum 1-hour CO averages (and dates of occurrence) from the 10-highest days for each CO site in Connecticut for 1978. The wind data associated with these high readings are also presented. (See the discussion of Table 12 in the TSP section for a description of the origin and use of these wind data.)

At the 9 CO sites in Connecticut, the high CO levels tend to occur on southwest wind days. Adverse atmospheric mixing or other meteorological conditions may be part of the reason CO levels are high on southwest wind days, but, in this case, another explanation appears more viable. A noteworthy feature of the high CO days is that the winds tend to be more persistent from all directions than on the high days for the other pollutants. Since 95% of the CO emissions in Connecticut come from motor vehicles, it is likely that the high CO levels are caused when persistent winds are blowing CO emissions from the direction of nearby roads toward the monitors. Such appears to be the case especially with the Norwalk OO5, Stamford O2O, and Waterbury OO4 sites, where the most heavily traveled roads are to the southwest of the monitors.

Another feature of the high CO days is that rarely does more than one site record a high level on the same day. There were no days in 1978 where CO levels were high across the state. This is the opposite of the behavior exhibited by all the other pollutants and demonstrates that high levels of CO are much more dependent on local effects than the other pollutants.



1978 CARBON MONOXIDE STANDARDS ASSESSMENT SUMMARY, UNITS = PPM

	MAXIMUM	TIME OF	2ND HIGH	TIME OF	MAXIMUM	TIME <sup>2</sup> OF	2ND HIGH	TIME <sup>2</sup> OF
TOWN-SITE	8-HUUK AVERAGE	MAX IMUM 8-HOUR	8-HOUR AVERAGE	2ND HIGH 8-HOUR	1-HOUR AVERAGE	MAXIMUM 1-HOUR	1-HOUR AVERAGE	2ND HIGH 1-HOUR
Bridgeport-004	17.8	1/9/1	13.5	2/4/14	27.5	1/5/22	25.0	2/3/18
Greenwich-001*	16.6ª	1/9/1	10.1	1/6/04	32,5	1/5/19	26.0	1/24/08
Hartford-009*	9.6	3/9/12	8.9	3/8/18	17.0	2/9/09	14.0	3/8/05
Hartford-012	12.6	12/8/24	12.1	11/28/20	25.0	11/28/14	21.0	12/04/18
New Britain-002	16.8	7/17/14	15.4	12/16/24	29.0	7/17/08	24.0	1/19/20
New Haven-007*	15.8 <sup>b</sup>	11/4/03	12.3	11/3/22	21.5	11/3/24	17.5	11/3/23
Norwalk-005*	16.2	12/16/4	15.3	5/20/02	25.5	10/23/08	23.5	12/6/09
Stamford-020	27.9	11/30/18	27.5	1/5/20	40.0	10/18/08	39.0	11/9/09
Waterbury-004*	11.7	8/4/21	11.4	8/3/17	21.5	8/4/15	20.0	1/24/18

month/day/hour (EST), specifying the end of the 8-hour average period month/day/hour (EST), specifying the end of the 1-hour average period time of 8-hour averages is reported as follows: time of 1-hour averages is reported as follows: partial year non-overlapping maximum on 01/05/20 of 12.1 ppm non-overlapping maximum on 11/04/06 of 13.4 ppm ν.

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TABLE 26

1978 CARBON MONOXIDE SEASONAL FEATURES, UNITS = PPM

TOWN-SITE		JAN.	FEB.	MAR.	APR.	MAY	JUNE	JULY	AUG.	SEPT.	OCT.	NOV.	O S DEC. E	NUMBER OF TIMES STANDARD EXCEEDED	
Bridgeport-004	Max-1 hr. Max-8 hr.	27.5	25.0	14.0 8.6	13.0	19.0	9.0	9.0	9.0	13.0 8.2	10.0* 7.6*	14.1	19.0* 8.3*	0 27	
Greenwich-001	Max-1 hr. Max-8 hr.	32.5 16.6	8.0	3.5	23. 88.	3.5*	1 1			1 1 1 1 1 1	[ ] 1 ]		! !	0 7	
Hartford-009	Max-1 hr. Max-8 hr.	13.0	17.0	14.0 9.6	9.0	11.0	14.0 8.0	10.0	12.0	6.3 ***		1 1 1 1 1 1		0	
Hartford-012	Max-1 hr. Max-8 hr.	!!!	!!!		     		I ! I ! I I	! ! ! ! ! !	1 t 1 t	!!!	}   } 	25.0* 12.1*	21.0 12.6	0	
 New Britain-002	Max-1 hr. Max-8 hr.	24.0 13.4	16.2	18.5 10.9	13.5	11.5*	18.0 14.2	29.0 16.8	17.2	18.0	14.0	14.9	23.0	0 104	
New Haven-007	Max-1 hr. Max-8 hr.	7.0* 4.7*	7.0* 3.9*	11.0* 7.6*	13.0	16.1 6.9	9.0	13.0 5.4	10.0* 4.6*		[	21.5* 15.8*	10.0* 6.1*	5 0	
Norwalk-005	Max-1 hr. Max-8 hr.	21.0	19.2 14.4	     	14.0	18.0* 15.3*	14.0* 9.9*	11.5* 9.8*	17.0	14.2* 11.5*	25.5* 12.3*	16.0	23.5 16.2	0 85	
Stamford-020	Max-1 hr. Max-8 hr.	36.0* 27.5*	34.0 23.4	30.0* 20.3*	33.0	28.0	28.5* 19.0*	27.0	29.0	34.0 19.0	40.0	39.0	38.0 26.1	7 366	
Waterbury-004	Max-1 hr. Max-8 hr.	20.0	4.0*	15.0* 7.9*	11.0	14.0	15.5	11.8*7.7	21.5	12.0* 7.0*	i I i i	     		0 11	

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AIR COMPLIANCE ENGINEERING

CONNECTICUT DEPARTMENT OF ENVIROMENTAL PROTECTION

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DIR (DEG)
VEL (MPH) 7.4

SPD (MPH) 11.2

RATIO 0.662

DIR (DEG) 280

VEL (MPH) 12.5

SPD (MPH) 12.5

RATIO 0.770

DIR (DEG) 310

VEL (MPH) 3.6

SPD (MPH) 8.2

RATIO 0.444

DIR (DEG) 300

VEL (MPH) 11.2

SPD (MPH) 11.2

SPD (MPH) 11.2 7 162 21.5 DATE 11/3/78 DIR (DEG) 20 VEL (MPH) 2.1 SPD (MPH) 4.3 RATIC 0.488 320 2.2 500 RATIC DIR (DEG) VEL (MPH) SPD (MPH) RATIC DIR (DEG) DIR (DEG) VEL (MPH) SPD (MPH) RATIO DIR (DEG) VEL (MPH) SPD (MPH) VEL (MPH) SPD (MPH) SITE SAMPLES ເດ SITE CONN. SITE MASS. SITE CONN. SITE MASS. SITE N. J. SITE CONN. SITE CONN. SITE MASS. SITE N. J. POLLUTANT -- CARBON MONDXIDE MET EDROLOGICAL WORCESTER MET EDROLOGICAL WORCESTER METEOROLOGICAL NEWARK METEOROLOGICAL WORCESTER METEOROLOGICAL BRIDGEPORT METEOROLOGICAL BRADLEY FIELD METEOROLOGICAL BRIDGEPORT METEOROLOGICAL BRADLEY FIELD METEOROLOGICAL TOWN NAME HAVEN NORWALK Z

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	SITE	DIR (DEG)		, N	6	7		16	0	, 4	7	S
BRIDGEPORT	CONN.	VEL (MPH)	3.0	7.1	4.2	დ	შ	0.6	8.0	m	15.6	ຫ
		SPD (MPH)			თ. თ	•	•		•	•		10.2
		RATIO	0.298	0.838	N	0.584	~	N	ო	ဗ္ဗ	ω	0.928
METEOROLOGICAL	SITE	DIR (DEG)	_	160	50	50	4	80	œ	~	Θ	170
	CONN.	VEL (MPH)	2.9	4.4	•	•	2.3	•	•		7.1	ຫ ໜ້
		SPD (MPH)		4.7	5.0	4.2	•	•		•	•	0.0
		RATIO	0	0.938	Φ	0	4	0.154	ന	œ	ທ	0.983
METEOROLOGICAL	SITE			260	ω	04	m	ഥ	A-0	a	ဖွ	250
	MASS.	_	_	9. 9	ທ ທ	2.4		٠		٠	7.3	ທ
		SPD (MPH)		0.1	٠	•				٠	•	o G
		RATIO	0.902	0.954	œ	(7)	ത	0.351	œ	600	w	0.943
												٠

#### VII. LEAD

#### Conclusions:

The newly promulgated NAAQS for lead (1.5  $\mu$ g/m<sup>3</sup>, calendar quarter average) was exceeded at 16 sites in 1978.

No significant change in measured concentrations of lead occurred between 1977 and 1978.

The monitoring sites where the lead standard was exceeded were generally in urban locations in areas of moderate to heavy traffic. In Connecticut, the primary source of lead concentrations in the atmosphere is emissions from the combustion of leaded gasoline in motor vehicles. Atmospheric concentrations of lead should decline as the combustion of leaded gasoline decreases because more new cars require unleaded gasoline.

#### Sample Collection And Analysis:

The Air Monitoring Unit uses hi-vol and lo-vol samplers to obtain ambient concentrations of lead. These samplers are used to collect particulate matter onto fiberglass filters. The particulate matter collected on the filters is subsequently analyzed for its chemical composition. Wet chemistry techniques are used to separate the particulate matter into various components. The lead content of the TSP is determined using an atomic absorption spectrophotometer. (The use of these sampling devices and the chemical analysis techniques were fully described in the TSP section.)

### Discussion of Data:

Monitoring Network - In 1978, both hi-vol and lo-vol samplers were operated in Connecticut (see Figure 4). Because the Federal EPA does not recognize the lo-vol instrument as an equivalent to the reference (hi-vol) method of sampling for lead, only hi-vol data are analyzed for compliance with NAAQS.

New NAAQS - On October 5, 1978, the EPA established a new ambient air quality standard for lead of 1.5  $\mu g/m^3$  for a calendar quarter-year average. The standard is attained only if the quarterly averages of all four calendar quarters in a year do not exceed 1.5  $\mu g/m^3$ .

Quarterly Averages – The calendar quarter lead standard was exceeded at 16 sites in 1978, 4 less than in 1977. The quarterly averages (and the annual averages) for lead in 1978 are presented in Table 28. The maximum quarterly lead level was higher in 1978 than in 1977 at 21 of the 32 hivol sites where the minimum EPA sampling criteria were met. At 5 of these sites the increase exceeded 0.5  $\mu g/m^3$ . The maximum quarterly lead level decreased at 10 sites from 1977 to 1978, while 2 of those decreases exceeded 0.5  $\mu g/m^3$ . The maximum quarterly level at one site (Stratford 005) was unchanged. (Annual average lead concentrations decreased at 29 sites and increased at only 3 sites from 1977 to 1978. The annual average lead levels for 1970-1978 can be found in Table 10.)

TABLE 28  $\underline{\text{1978 QUARTERLY AND ANNUAL AVERAGE LEAD (Pb) LEVELS BY SITE, } \mu\text{g/m}^3}$ 

<sup>\*</sup> Weighted average based on number of filters analyzed in each quarter

#### VIII. CLIMATOLOGICAL DATA

Weather is often the most significant factor influencing short term changes in air quality and may also have an affect on long-term trends. In Tables 29 and 30 monthly and annual averages of the 1978 climatological data from National Weather Service Stations located at Bradley International Airport in Windsor Locks and at Sikorsky Memorial Airport near Bridgeport are compared to "normal" or "mean" values. These comparisons show that 1978 was considerably colder than a "normal" year, but that wind speed and precipitation were slightly above average in Bridgeport and below average in Windsor Locks. Tables 31 and 32 contain climatological data from Windsor Locks and Bridgeport, respectively, for 1977. More discussion of the meteorological data is included in the discussions of each pollutant in the earlier sections of this 1978 Annual Summary.

Wind roses for Bradley Airport, Sikorsky Airport, and Newark Airport have been developed from 1978 National Weather Service surface observations and are shown in Figures 9, 10 and 11. Wind roses from these stations for 1977 are shown in Figures 12, 13, and 14. The differences between 1977 and 1978 wind roses were discussed earlier in the trend analysis section.

TABLE 29 1978 CLIMATOLOGICAL DATA BRADLEY INTERNATIONAL AIRPORT

AVERAGE TEMP. EX  TEMPERATURES °F  1978 Normal <sup>a</sup> 1978 M  23.6 24.8 0
0
0 0
*
_
3 4
7 8
5
0
*
0 0
0
12 20
Extracted From:

TABLE 30 1978 CLIMATOLOGICAL DATA SIKORSKY MEMORIAL AIRPORT

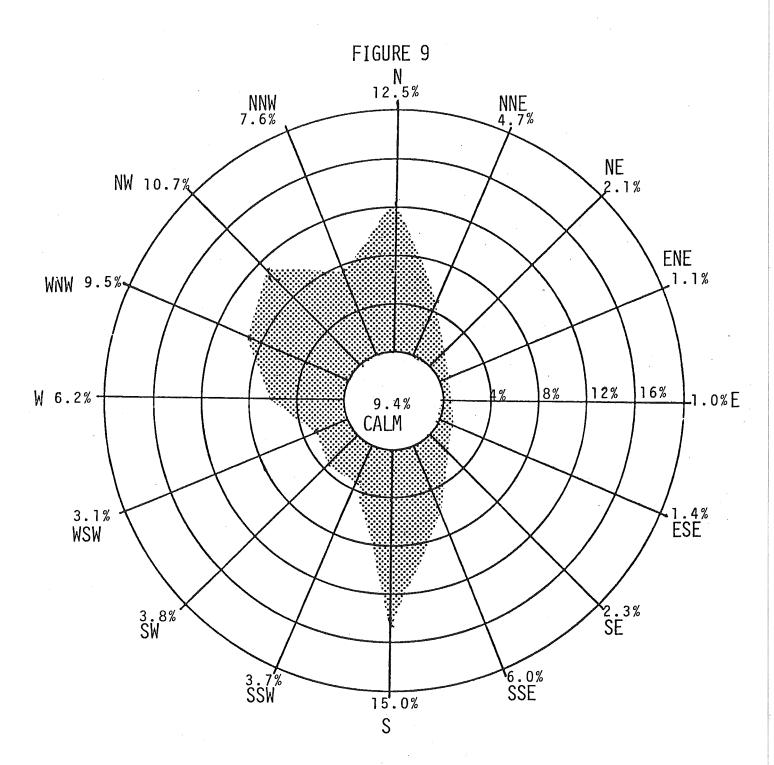
		Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	YEAR	
WIND MPH)	Meand	13.0	13.5	13.5	13.0	11.7	10.5	10.0	10.0	11.11	11.8	12.7	13.0	12.0	
AVERAGE WIND SPEED (MPH)	1978 M	15.1	11.7	12.8	13.9	12.6	9.01	11.4	10.3	11.4	12.3	11.7	14.3	12.3	
7371															
R OF WITH AN .01 S OF TATION	Mean	<u>_</u>	10	Ξ			· 6	ω	10	့တ	7	10	Ξ	118	ri on
NUMBER OF DAYS WITH MORE THAN .01 INCHES OF PRECIPITATION	1978	13	7	7	7	10	Ξ	7	13	10	ω	Ξ		112	inistra
	er i	·									•				Local Climatological Data Charts U.S. Department of Commerce National Oceanic and Atmospheric Administration Environmental Data Service
ECIPITATION IN INCHES WATER QUIVALENT	Normal <sup>a</sup>	2.71	2.71	3.49	3.39	3.57	2.56	3.44	3,80	2.88	2.79	3.83	3.44	38.61	ata Cha merce tmosphe
PRECIPITATION IN INCHES WATER EQUIVALENT	1978	7.91	1.34	3.95	1.97	5.12	1.59	2.59	5.90	3.75	2.54	1.74	4.76	43.16	gical Dom of Com c and A ata Ser
•															imatolo artment Oceani ental D
DEGREE DAYS	Normal <sup>a</sup>	1079	955	840	498	225	24	0	0	42	261	570	296	5461	Local Climatological Data Charts U.S. Department of Commerce National Oceanic and Atmospheric Environmental Data Service
DEGRE	1978	1181	1136	904	536	265	43	4	0	35	290	524	888	5864	
															Extracted From:
R OF ON MAX. XCEEDED	Mean	0	. 0	0	0	*	<b></b> -	ო	7	*	0	0	0	9	Extre
NUMBER DAYS WHICH TEMP. EX	1978	0	0	0	0	0	0	2	2	0	0	0	0	4	
															1941-1970 1966-1978 1949-1978 1958-1978
RAGE TURES °F	Normala	30.2	30.9	37.9	48.4	58,3	6.79	73.8	72.7	66.5	56.8	46.0	33.8	51.9	<b>ଟ</b> ଠର ଜ
AVERAGE TEMPERATURES	1978	26.6	24.1	35.6	46.9	56.8	66.4	73.2	75.0	64.2	55.4	47.2	36.2	50.7	
															Less than 1/2
	٠	January	February	March	April	May	June	July	August	September	October 0	November	December	YEAR	* Less t

TABLE 31
1977 CLIMATOLOGICAL DATA
BRADLEY INTERNATIONAL AIRPORT

O 1	i .	Jan.	Feb.	Mar.	Apr.	May	June	July	Aug.	Sept.	Oct.	Nov.	Dec.	YEAR	
AVERAGE WIND SPEED (MPH)	Meand	9.4	9.8	10.4	10.6	9.3	8.4	7.8	7.6	7.6	8.1	8.7	8.9	8.0	
AVERAGE	1977	8.3	8.6	9.2	8.8	8.1	7.4	6.3	5.6	6.1	6.8	7.2	7.4	7.5	
NUMBER OF DAYS WITH MORE THAN .01 INCHES OF PRECIPITATION	Mean	hara faces	F	<u>د -</u>	=	12	15	10	10	10	8	h	13	129	ion
NUMBER O DAYS WIT MORE THAN INCHES O PRECIPITAT	1977	10	10	12	_	<b>σ</b> 1	14	10	01	11	13	13	13	142	ministrat
TATION CHES ER LENT	Normala	3.28	3.17	3.82	3.75	3.50	3.53	3.41	3.94	3.55	3.03	4.33	4.06	43.37	imatological Data Charts t. of Commerce Oceanic and Atmospheric Administration ental Data Service
PRECIPITATION IN INCHES WATER EQUIVALENT	1977	2.41	2.81	6.57	4.89	3.70	3.99	3.37	2.44	8.17	5.45	4.38	5.68	53.86	logical Data Commerce nic and Atmos Data Service
DAYS	Normala	1246	1070	116	519	226	24	0	12	106	384	711	1141	6350	Local Climatological Data Charts U.S. Dept. of Commerce National Oceanic and Atmospheric Environmental Data Service
DEGREE DAYS	N 7261	1429	1038	684	419	130	45		∞	112	399	610	1141	6016	•
NUMBER OF DAYS ON WHICH MAX. TEMP. EXCEEDED 90 °F	Meanb	0	0	0	₩.	<b></b>	4	œ	ĸ	<b></b> -	*	0	Ö	21	Extracted From:
NUMBER OF DAYS ON WHICH MAX TEMP. EXCEE	1977	0	0	0	· -	4	0	14	9	_	0	0	0	56	
<b>!</b> -	Normala	24.8	26.8	35.6	47.7	58.3	67.8	72.7	70.4	62.8	52.6	41.3	28.2	49.1	a 1941-1970 b 1960-1977 c 1955-1977 d 1955-1977
AVERAGE TEMPERATURES	1977	18.7	27.6	42.9	51.2	63.6	68.0	74.5	72.8	64.0	52.0	44.4	28.0	50.6	1/2
		January	February	March	April	Мау	June	July	August	September	October .	November	December	YEAR	* Less than 1/2

TABLE 32 1977 CLIMATOLOGICAL DATA SIKORSKY MEMORIAL AIRPORT

	AVE	ERAGE	NUMBER DAYS WHICH TEMP EX	NUMBER OF DAYS ON WHICH MAX. TEMP. FXCEFDED			PRECIPITATION IN INCHES	TATION	NUMBER OF DAYS WITH MORE THAN .O	NUMBER OF DAYS WITH RE THAN .OT	6		
	TEMPER	TEMPERATURES °F	90	° F	DEGRE	DEGREE DAYS	EQUIVALENT	LENT	INCHES OF PRECIPITATION	TATION	AVERAGE WIND SPEED (MPH)	E WIND (MPH)	
	1977	Normala	1977	Meanb	1977	Norma1 <sup>a</sup>	1977	Normal <sup>a</sup>	1977	MeanC	1977	Meand	
January	23.7	30.2	0	0	1274	1079	2.43	2.71	10		15.0	12.9	Jan.
February	31.2	30.9	0	0	940	955	1.74	2.71	10	10	13.7	13.6	Feb.
March	41.9	37.9	0	0	710	840	7.74	3.49	10	1	14.7	13.5	Mar.
April	49.1	48.4		0	470	498	3.60	3,39	∞	<u></u>	13.1	12.9	Apr.
Мау	60.4	58.3	0	* `	160	225	2.07	3,57	7	Ξ	12.1	11.6	May
June	65.1	6.79	0	-	62	24	2.75	2.56	10	6	11.9	10.5	June
July	72.6	73.8	4	က	4	0	1.03	3.44	. 7	&	10.5	o.	July
August	74.1	72.7	<b></b>	<b>'</b> 2	က	0	4.69	3.80	13	თ	10.1	10.01	Aug.
September	67.8	66.5	0	÷	52	42	7.26	2.88	12	Ø	12.1	11.1	Sept.
October	56.9	56.8	0	0	248	261	3.94	2.79	12	7	12.6	11.8	Oct.
November	50.0	46.0	0	0	442	570	4.93	3.83	15	10	14.3	12.7	Nov.
December	33.5	33.8	0	0	026.	. 967	5.17	3.44	12	_	1	12.9	Dec.
YEAR	52.2	51.9	S.	y	5335	5461	47.35	38.61	126	118	12.7	12.0	YEAR
* Less than 1/2	<b>2</b> .	a 1941-1970 b 1966-1977 c 1949-1977 d 1958-1977	iп	Extracted From:	Local Cl U.S. Dep National		Data Chommerce Atmosplervice	imatological Data Charts artment of Commerce Oceanic and Atmospheric Administration ental Data Service	ration				



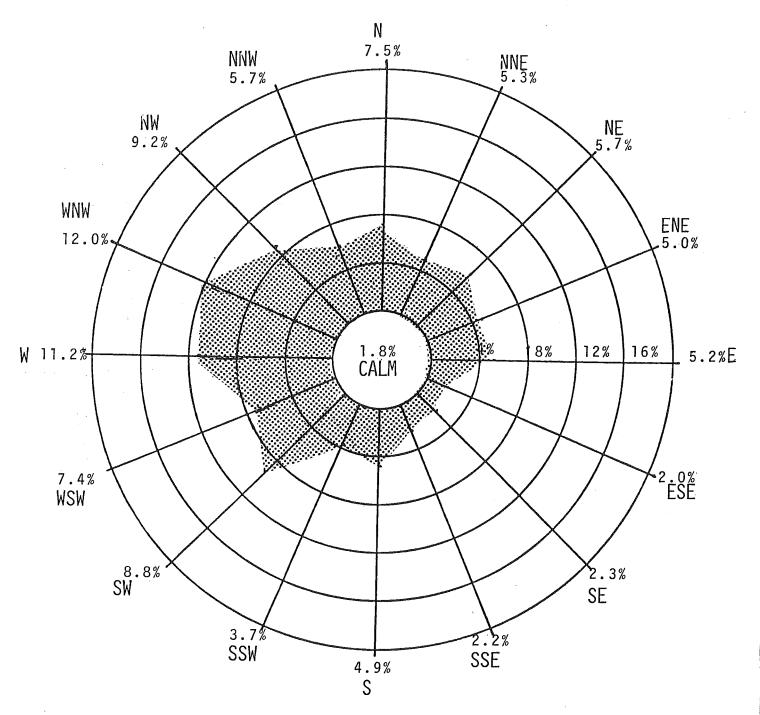
ANNUAL WIND ROSE 1978

BRADLEY INTERNATIONAL AIRPORT

WINDSOR LOCKS, CONNECTICUT

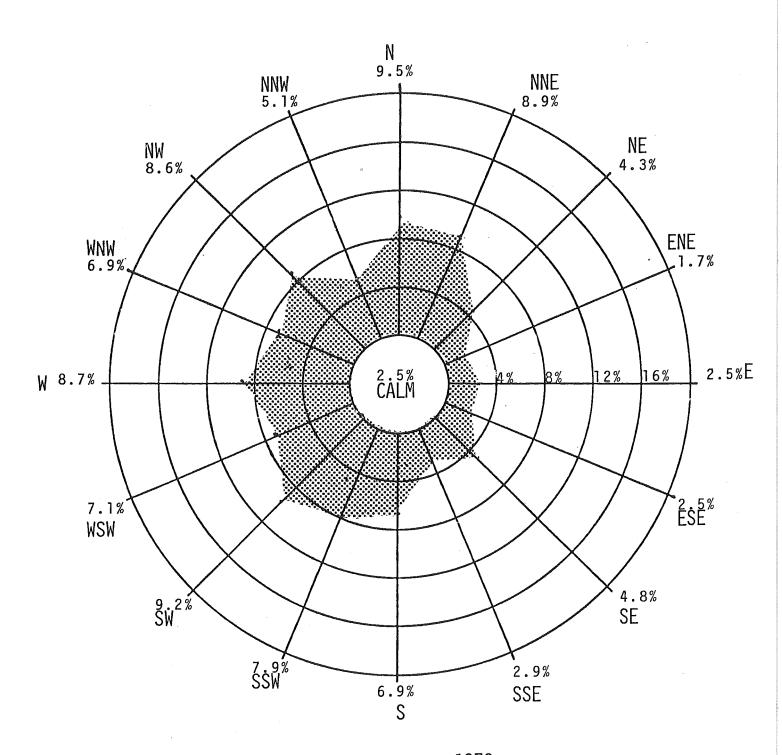
WIND FREQUENCY APPEARS NEXT TO EACH DIRECTIONAL ABBREVIATION

### FIGURE 10



ANNUAL WIND ROSE 1978
SIKORSKY MEMORIAL AIRPORT
STRATFORD/BRIDGEPORT, CONNECTICUT
WIND FREQUENCY APPEARS NEXT TO EACH DIRECTIONAL ABBREVIATION

FIGURE 11

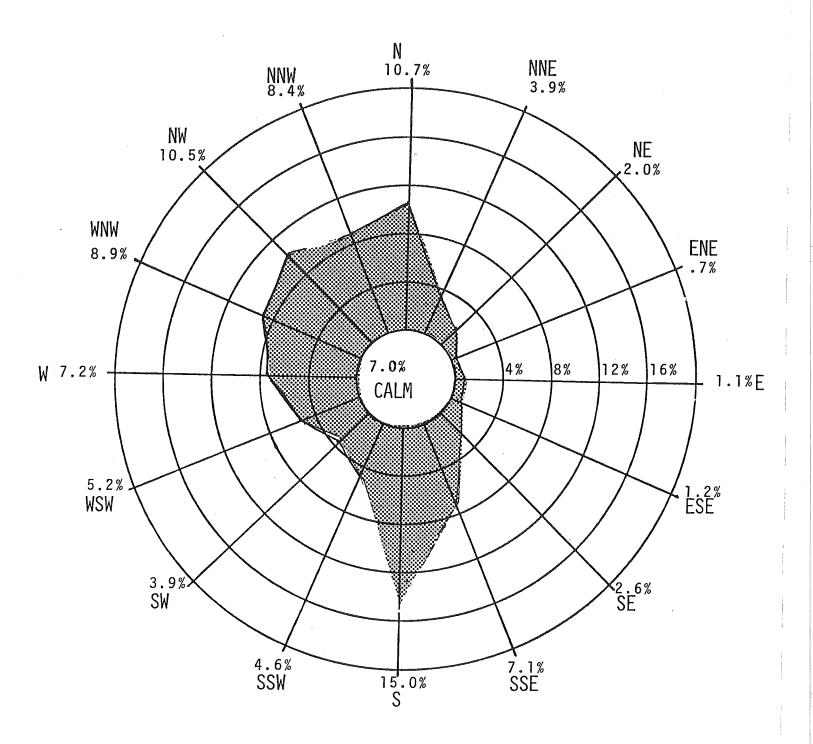


ANNUAL WIND ROSE 1978

NEWARK INTERNATIONAL AIRPORT

NEWARK, NEW JERSEY

WIND FREQUENCY APPEARS NEXT TO EACH DIRECTIONAL ABBREVIATION



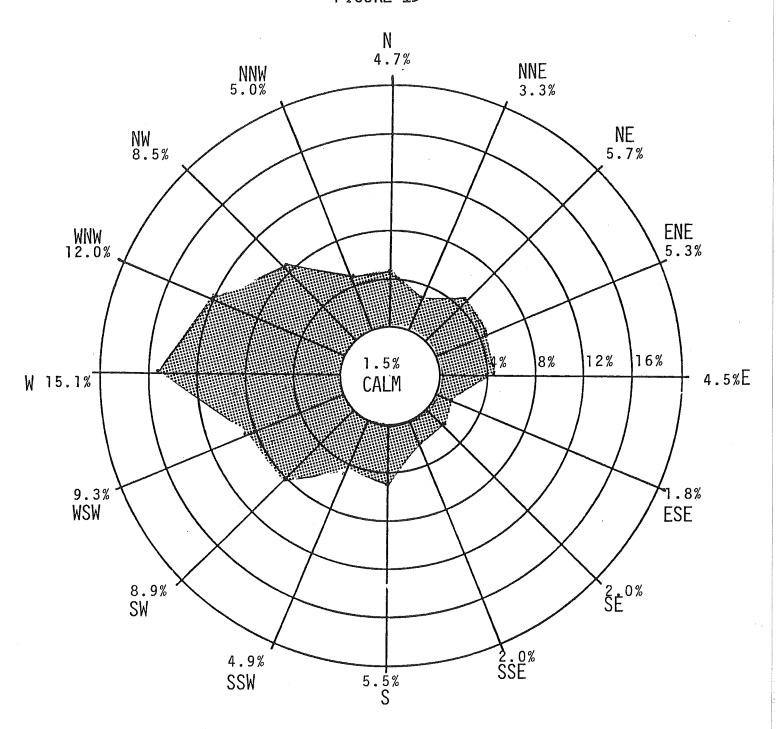
ANNUAL WIND ROSE 1977

BRADLEY INTERNATIONAL AIRPORT

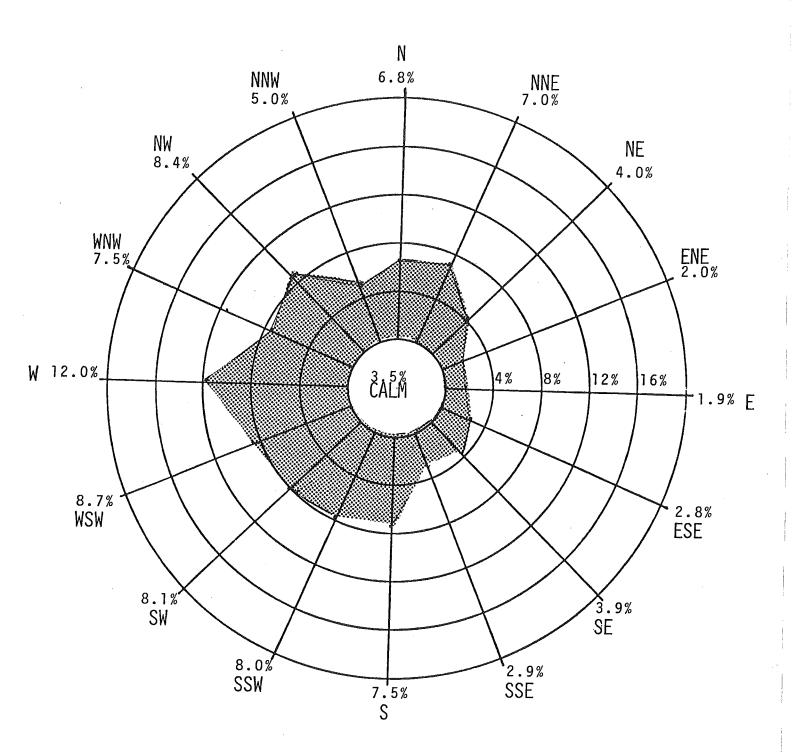
WINDSOR LOCKS, CONNECTICUT

WIND FREQUENCY APPEARS NEXT TO EACH DIRECTIONAL ABBREVIATION

# FIGURE 13



ANNUAL WIND ROSE 1977
SIKORSKY MEMORIAL AIRPORT
STRATFORD/BRIDGEPORT, CONNECTICUT
WIND FREQUENCY APPEARS NEXT TO EACH DIRECTIONAL ABBREVIATION



ANNUAL WIND ROSE 1977
NEWARK INTERNATIONAL AIRPORT
NEWARK, NEW JERSEY
WIND FREQUENCY APPEARS NEXT TO EACH DIRECTIONAL ABBREVIATION

# IX. ATTAINMENT AND NON-ATTAINMENT OF NAAQS IN CONNECTICUT'S AQCR'S

Connecticut's four Air Quality Control Regions (AQCR's, see Figure 15) have been analyzed for attainment status of National Ambient Air Quality Standards (NAAQS) for the following pollutants: 1) Total Suspended Particulates (TSP); 2) Sulfur Dioxide (SO<sub>2</sub>); 3) Ozone (O<sub>3</sub>); 4) Nitrogen Dioxide (NO<sub>2</sub>); 5) Carbon Monoxide (CO); and 6) Lead (Pb). Table 33 shows the attainment/non-attainment status for the NAAQS's for each pollutant in each AQCR. The regions are classified as attainment, non-attainment or unclassifiable. Regions are non-attainment if the region, or any portion thereof, was in violation of any NAAQS at any time during 1976, 1977, or 1978. Unclassifiable regions are ones in which there were no monitors with which to determine attainment or non-attainment.

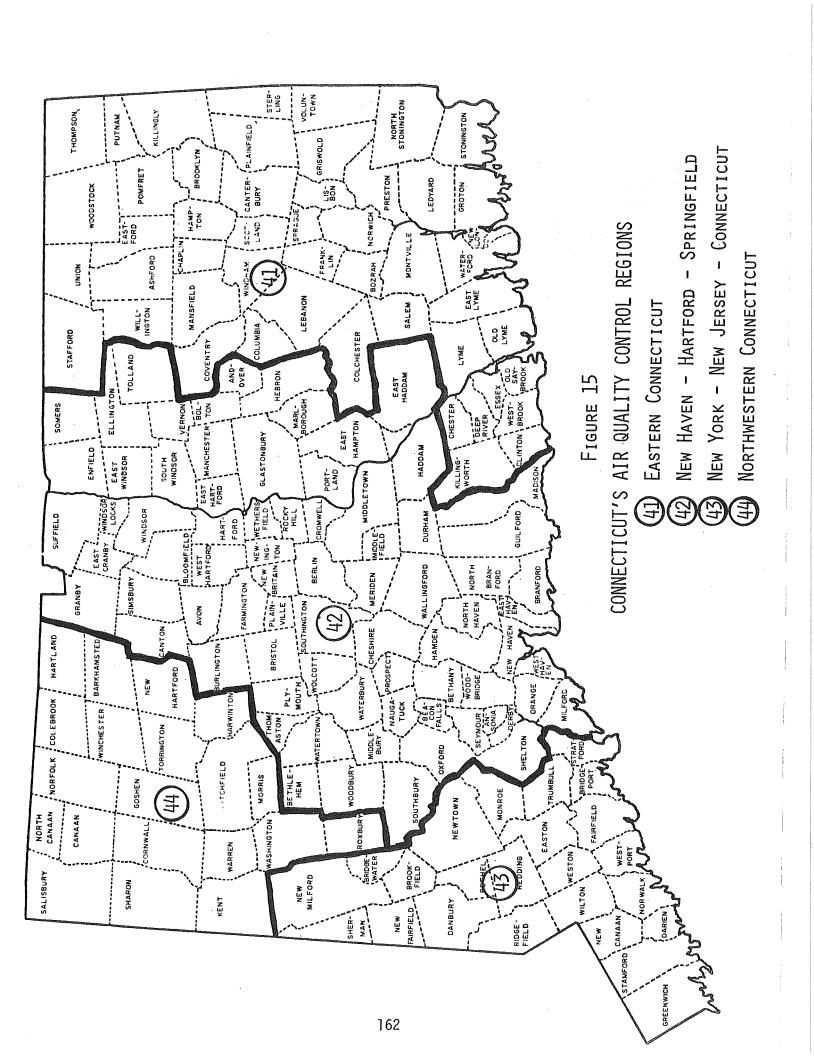


TABLE 33 CONNECTICUT'S COMPLIANCE WITH THE NAAQS (BY AQCR)

	PRIMARY OR SECONDARY	NAAQS	AQCR 41	AQCR 42	AQCR 43	AQCR 44
TSP	Primary	Annual 24-Hour	A A	χ* χ*	A X**	A A
	Secondary	Annual 24-Hour	X	X	X. X	X X
s0 <sub>2</sub>	Primary	Annual 24-Hour	A A	A A	A A	A A
	Secondary	Annual 24-Hour 3-Hour	A A A	A A A	A A A	A A A
03	Primary	1-Hour	Х	X	Х	Х
	Secondary	1-Hour	Χ	X	Х	X
NO <sub>2</sub>	Primary	Annual	A	A	A	A
	Secondary	Annual	А	А	Α	Α
CO	Primary	1-Hour 8-Hour	U U	A X	X	U U
	Secondary	1-Hour 8-Hour	U U	A X	X X	U U
Pb	Primary	Calendar Quarter	Х	Х	Х	X
	Secondary	Calendar Quarter	X	Χ .	Х	Х

X = Non-Attainment
U = Unclassifiable

A = Attainment

Town of Waterbury only Town of Greenwich only (based on additional monitoring conducted by EPA)

#### X. SPECIAL STUDIES

### A. STATIONARY SOURCE STACK HEIGHT GUIDELINE

This document presents a simple technique through which one can calculate the appropriate stack height for a source of pollution in order to avoid an adverse ambient impact. A reasonable worst case meteorology is assumed and dispersion calculations are presented in graphical form.

The Stationary Source Stack Height Guideline has been incorporated into Connecticut's new source review procedure and is being used in determining the minimum stack height required for a new source of pollution to enable it to meet certain air quality criteria. The operation of a new source must not prevent or interfere with the attainment and/or maintenance of any applicable ambient air quality standards, including "Prevention of Significant Deterioration" (PSD) limitations. The guideline was developed with the smaller sources in mind. It applies to pollution sources which require a State of Connecticut permit to construct and/or operate (Section 19-508-3 of the Connecticut Regulations for the Abatement of Air Pollution) and have actual emissions after control equipment of either sulfur dioxide (SO2) or total suspended particulates (TSP) of 15 tons per year or less. Larger sources will be subjected to a more intensive ambient impact analysis. This guideline also applies only to sources with SO2 or TSP emissions.

The guideline is designed so that the minimum stack height can be determined prior to the construction of a new point source. This will allow for consideration of ambient air quality impacts in the economic analysis of a proposed source or modification (i.e., which is the least expensive - control equipment, cleaner fuel, or a higher stack). In most cases, the stack height derived by following this guideline should be sufficient to enable a source to avoid becoming the cause of local air quality violations. Copies of the guideline are available from this Department.

#### B. AMBIENT IMPACT ANALYSIS GUIDELINE

The Ambient Impact Analysis Guideline describes the method employed by the Connecticut Department of Environmental Protection to analyze the ambient air quality impact (i.e., the increase in pollutant concentration) of a new source of pollution. It is possible for a permit applicant to follow this procedure and perform his own analysis. However, the document is intended to be a description rather than an instruction book. Most permit applicants do not have the computer facilities or staff to perform the analysis. The primary purpose of this document is to eliminate the prevalent concept that our ambient impact analysis is an unreliable incomprehensible "black box" procedure. In this guideline, we explain the input to the analysis, how it operates, and the meaning and significance of the results.

The Ambient Impact Analysis Guideline makes it possible to conduct New Source Review under the provisions of the Clean Air Act Amendments of 1977 without having to use a computer resource-intensive model and one year of actual hourly meteorological data.

The Guideline employs a modified version of the atmospheric dispersion model PTMTP. This version allows direct input of x, y and z coordinates of up to 25 point sources and 30 receptors and automatically handles the effects of topography independently for each source-receptor alignment by making specified adjustments to the plume flow (i.e., the distance from the plume centerline to the ground). These adjustments depend upon the magnitude of the terrain differences and the atmospheric stability conditions.

Since directionally persistent winds often produce the greatest impacts from a single source or group of sources, the PTMTP revisions include an automated technique developed to account for reasonably expected wind persistency for use when actual historical meteorological data are not available.

Historical ambient data are used to quantify the ambient levels caused by existing area sources and transport. The average of annual second high monitored levels (sites were grouped by source influence - sites significantly impacted by existing local point sources were excluded) are used to create a catalog of existing "bad-day" ambient levels for each town in the State.

The modeled "bad-day" ambient impact(s) of the new source(s) and existing local point sources are added to the existing "bad-day" ambient level in the town to determine if the new source will cause the NAAQS to be exceeded.

### C. LEAD (Pb) AND SULFATE (SO<sub>4</sub>) STUDY

The purpose of this study was to examine Total Suspended Particulates (TSP), lead (Pb), and sulfate (SO4) concentrations at several sites in Connecticut for trends from 1970 to 1978. All data were obtained from the monitoring network operated by the Connecticut Department of Environmental Protection. The lead and sulfate data were from quarterly composites, in which pieces of several hi-vol filters from a given quarter are chemically analyzed for constituents. In order to ensure representativeness of the quarterly averages, a minimum of five samples per quarter were required.

The sites examined in this study were selected to include a range of geographical, meteorological, and local emission source diversity. These sites represent the various conditions encountered throughout the State, allowing conclusions concerning statewide trends to be drawn. The sites also have a sufficiently lengthy historical record to allow the examination of trends with time.

The examination of data in this study involved linear regression analysis for time trends and relationships between TSP and lead or sulfate, and analysis of variance for quarterly and site-to-site variation. The three categories of interest (TSP, Pb, and  $SO_4$ ) were analyzed individually. Each site was examined for the above trends as well as the combination of all sites for statewide trends.

The analysis of TSP data revealed that statewide levels have dropped significantly since 1970. This is most likely due to the application of various air pollution control measures over that time span, both in Connecticut and elsewhere. Changes in TSP levels with calendar quarter were quite significant, with the first and second quarters (January through June) exhibiting the highest concentrations. The high levels observed in the first two calendar quarters could be due to a reduction in ventilation (reduced mixing height) and increased emissions. Ten sites showed a decrease in levels with time, while the change in levels was indeterminate at the remaining twenty eight sites. The overall site-to-site variation was significant, explaining 39% of the total variation in TSP levels. This indicates that the geographic location of a site is important.

Concentrations of lead also showed a marked decline since 1970. The concurrent decline in lead and TSP levels indicates that the control of particulate emissions may have, directly or indirectly, helped reduce lead levels. However, contrary to the TSP trend, the fourth quarter shows the highest Pb concentrations, while the second quarter has the lowest. Site-to-site variation was less pronounced than with the TSP data, indicating that lead concentrations are more widespread in nature. Lead levels have decreased with time at eight sites, and have not changed at the other thirty.

Analysis of the sulfate data indicate that levels have changed very little since 1970. Connecticut's sulfur-in-fuel regulation has been successful in reducing SO<sub>2</sub> concentrations, but has had little effect on sulfate. This is probably due to the fact that most sulfates are generated by photochemical reactions in the atmosphere, and are transported long distances into Connecticut. (This is similar to the ozone scenario.) The importance of the transport phenomena is demonstrated by the fact that the highest levels of sulfate measured occurred in 1976, coincident with an abnormally high incidence of winds from the southwest. Sulfates are a widespread problem, indicated by the fact that, over the 9 year period studied, only 8% of the variation in levels can be attributed to changes in site. Quarterly variation shows the fourth quarter to be the cleanest with respect to SO<sub>4</sub>, but there is no difference among the other three quarters.

The results of this study are preliminary, and indicate the general trends of the three subject pollutants. More extensive analysis is currently underway, and hopefully, those results will be published in the 1979 Air Quality Summary.

#### D. PASSIVE SAMPLING ERROR

The current Federal EPA reference method for the determination of Total Suspended Particulate matter (TSP) in the atmosphere is the high volume method (hi-vol). The hi-vol sampler is normally operated for a 24-hour period by drawing air through an 8 x 10 in. glass fiber filter at an air sampling flow rate of between 40-60 cfm (cubic feet per minute). Normally, an expended collection filter is picked-up and replaced with a clean filter some time after each 24-hour sampling interval. Most TSP samples are presently collected in this manner every 6th day (61 samples per year). This sampling schedule allows the filter to remain in the hi-vol for up to 5 days prior to the intended sampling date (the only day when the hi-vol motor is operating) and for up to 5 more days after sampling is completed. Although sheltered from above, these filters are exposed to the air and are therefore able to pick-up material by deposition or chemical reaction (with acid gases such as SO<sub>2</sub> and NO<sub>2</sub>) or lose material due to wind erosion.

In 1975, as Connecticut was developing the low volume sampling device, an investigation was begun to determine the significance of the potential errors associated with the partial sampling schedule used by the hi-vol. This study involved a simple experiment: filters were installed in a shelter and exposed to the air as in normal sampling, but no motor was used and no active sampling took place. Material was found to collect on the filters, thus demonstrating the existence of a "passive sampling error". Eight samples were collected in this manner and were compared to co-located regular hi-vol samples. The results indicated that 5% to 28% of the material found on the regular hi-vol samples was collected during the period when the regular hi-vol motor was inoperative. However, this study did not address the entire period in which passive sampling takes place. This study only involved the passive sampling error which takes place prior to the operation of the hi-vol motor; the potential for error after the hi-vol motor is again turned off was not investigated.

In 1976, the passive sampling error study was continued with the analysis of fourteen passive samples. In order to account for the entire passive sampling period, the passive sample filter was mounted in the field and collected under the same schedule as an adjacent hi-vol running under the every-sixth-day sampling schedule. Thus, passive and hi-vol samples produced matched pairs of data for analysis. The percentage of each hi-vol sample that can be attributed to the passive sampling error was determined for each sampling period by dividing the weight of the material collected on the passive filter by the total weight of material collected on the adjacent active hi-vol filter. The above percentages were normalized by multiplying by [(N-1)/N] to reflect that the hi-vol only sampled passively for (N-1) of the N sample days. The results implied that the passive sampling error was responsible for 10% to 20% of the TSP concentration measured on the active hi-vol.

The 1976 study also included an analysis of passive sample filters installed on an inverted hi-vol. These filters collected considerably less material than the filters obtained from adjacent hi-vols installed in the normal, upright manner. This study enabled the DEP to conclude that particle settling is the most important mechanism for adding material to the passive filter.

In 1977, the passive sampling error study was expanded to include a full year's worth of data (58 samples). The passive samples and active hivelength his samples were again collected on the same schedule, producing matched pairs of data for analysis. The sampling was conducted at the Hartford 003 (Hartford Library) site. Once again, a normalized passive sampling portion of each TSP sample was determined as described above. The individual sample percentages were then averaged for the year to give an annual average passive sampling error. This error was 12.4% at the Hartford 003 site in 1977 (see Table 34).

The 1977 passive sampling data were also analyzed for monthly and seasonal patterns. While the size of the passive sampling error oscillated from month to month, there was a general decline in the size of the error from the beginning to the end of the year.

In 1978, the passive sampling error study was extended to two additional monitoring sites. This was done because there was some concern that the results obtained at the Hartford 003 site would not be typical of the entire state. The additional sites used were Berlin 001 and Waterbury 123. The sampling was conducted in the same manner as before and normalized annual average passive sampling error percentages were derived. Since the passive sampling error was previously found to vary considerably by season, this 1978 Annual Summary includes data obtained in early 1979 in order to provide reliable and comparable annual averages for each of the sites studied. The passive sampling error amounted to 7.9% at Berlin 001, 12.5% at Waterbury 123 and 14.2% at Hartford 003 (see Table 34). These results indicate that the passive sampling error is smaller at a rural site than at urban sites, but even at the rural site the error is of significant size.

All the analyses conducted so far indicate that a substantial positive bias exists in the hi-vol sampling method, but, one aspect of the passive sampling problem has not been adequately addressed in these studies. The experimental method described above does not account for the possibility of wind erosion from the active hi-vol filter. The effect of wind erosion cannot be discerned from these experiments because both the active and passive samples are exposed to the air all the time. Even though both samples are susceptible to wind erosion, the active sample will have more material available to be lost. Thus, wind erosion has the potential to introduce a negative bias to the hi-vol sampling method, perhaps partially compensating for the positive bias caused by particle deposition. In any event, the standard hi-vol sampling method (and schedule) is susceptible to measurement biases which can result in incorrect data for the dates being sampled.

As a result of these passive sampling error studies, the DEP has purchased an accessory device for each DEP hi-vol which is expected to eliminate the passive sampling error. These devices consist of a retractable lid which covers the filter paper except when the hi-vol motor is operating. Actually, the lid retracts just prior to the start of the hi-vol sampling period and returns to cover the filter paper when sampling is completed. The cover, in its retracted position, is stored beneath the top plate of the hi-vol shelter and thus does not obstruct normal air flow during the scheduled hi-vol sampling period. With these devices no particle deposition can occur before sampling and no particle deposition or loss can occur after sampling. The first such device was installed early in 1979 on a hi-vol next to the regular hi-vol at the Hartford 003 site. The data obtained at this site will be included in the 1979 Annual Summary. These retractable lid devices were installed at all DEP monitoring sites by January 1, 1980.

### TABLE 34 PASSIVE SAMPLING DATA

### HARTFORD 003, 1977

	# OF DAYS	PASSIVE WEIGHT	TOTAL PASSIVE		CORRECTED PASSIVE	ACTIVE	PASSIVE + HI-VOL
SAMPLING PERIOD	<u>(N)</u>	<u>(g)</u>	$\mu g/m^3$	$\frac{((N-1) \div N)}{((N-1) + N)}$	μg/m <sup>3</sup>	HI-VOL	<u></u> %
12/28/76-1/5/77 1/5-1/12 1/12-1/18 1/18-1/24 1/24-1/28 1/28-2/3 2/3-2/9 2/9-2/17 2/17-2/23 2/23-3/1 3/1-3/7 3/7-3/11 3/11-3/18 3/18-3/24 3/24-3/31 3/31-4/6 4/6-4/12 4/12-4/18 4/18-4/21 4/21-4/26 4/26-5/5 5/5-5/12 5/12-5/16 5/16-5/23 5/23-5/26 5/26-6/1 6/1-6/10 6/10-6/13 6/13-6/22	87664668666476766635974736939	.024 .014 .009 .018 .014 .030 .014 .035 .030 .022 .039 .025 .038 .019 .033 .020 .023 .040 .013 .013 .013 .022 .022 .022 .022 .025 .016	13 7 4 9 7 16 7 18 16 11 20 13 19 10 17 10 11 21 7 7 17 11 13 9 18 15 4 13	7/8 6/7 5/6 5/6 5/6 5/6 5/6 5/6 5/6 5/6 5/6 5/6	11.4 6.0 3.3 7.5 5.3 13.3 5.8 15.8 15.8 15.8 16.7 9.8 16.3 8.3 14.6 8.3 14.6 8.3 14.7 5.6 15.1 9.4 8.3 11.1 6.0 15.0 13.3 2.7	23 62 55 24 57 122 41 74 220 58 158 121 48 64 57 74 64 178 92 55 97 72 127 67 105 88 59 41 87	49.5 9.7 6.1 31.3 9.2 10.9 14.2 21.3 6.1 15.8 10.5 8.1 25.6 11.3 9.8 5.1 10.2 15.6 13.1 6.5 16.6 5.7 17.0 22.6 6.5 13.3
6/22-6/28 6/28-7/5 7/5-7/11 7/11-7/15 7/15-7/22 7/22-7/26 7/26-8/3 8/3-8/10 8/10-8/15 8/15-8/22 8/22-8/24 8/24-9/2 9/2-9/21 9/21-9/27 9/27-9/30 9/30-10/6	7 6 4 7 4 8 7 5 7 2 9 -6 3 6	.023 .013 .014 .023 .016 .022 .018 .008 .012 .004 .020	14 8 8 13 9 13 10 4 7 2 10 - 4 6 7	6/7 5/6 3/4 6/7 3/4 7/8 6/7 4/5 6/7 1/2 8/9 - 5/6 2/3 5/6	12.0 6.7 6.0 11.1 6.8 11.4 8.6 3.2 6.0 1.0 8.9	85 73 32 73 80 46 80 63 52 70 92 - 39 69 40	14.1 9.1 18.8 15.3 8.4 24.7 10.7 5.1 11.5 1.4 9.7 - 8.5 5.8 14.6

### HARTFORD 003, 1977

SAMPLING PERIOD	# OF DAYS	PASSIVE WEIGHT (g)	TOTAL PASSIVE µg/m3	CORRECTION RATIO ((N-1) ÷ N)	CORRECTED PASSIVE µg/m <sup>3</sup>	ACTIVE HI-VOL	PASSIVE ÷ HI-VOL
10/6-10/12 10/12-10/18 10/18-10/24 10/24-11/1 11/1-11/8 11/8-11/14 11/14-11/17 11/17-11/22 11/22-11/29 11/29-12/5 12/5-12/14 12/14-12/20 12/20-12/23 12/23-12/29	6 6 8 7 6 3 5 7 6 9 6 3 6	.010 .003 .010 .013 .011 .011 .006 .006 .008 .008 .031 .012 .006	5 2 5 6 6 6 3 3 4 4 16 6 3 10	5/6 5/6 5/6 7/8 6/7 5/6 2/3 4/5 6/7 5/6 8/9 5/6 2/3 5/6	4.2 1.7 4.2 5.3 5.1 5.0 2.0 2.4 3.4 3.3 14.2 5.0 2.0 8.3	39 60 79 62 75 39 66 59 32 54 75 52 34	10.7 2.8 5.3 8.5 6.9 12.8 3.0 4.1 10.7 6.2 19.0 9.6 5.9 7.8
12/28/76-12/29/77 Avg. N =	5.98 da	ys	Av	g. N-1 = 4.98	Avg. %	Passive =	12.35
		HAR	TFORD 00:	3, 1978			
1/18/78-1/24/78 1/24-1/26 1/26-2/6 2/6-2/9 2/9-2/14 2/14-2/24 2/24-3/1 3/1-3/7 3/7-3/13 3/13-3/20	6 2 11 3 5 10 5 6	.006 .026 .018 .017 .010 .042 .016 .026	3 14 9 5 22 9 13 12	5/6 1/2 10/11 2/3 4/5 9/10 4/5 5/6	2.5 7.0 8.2 6.0 4.0 19.8 7.2 10.8 10.0	27 53 71 20 62 92 80 75 151	9.3 13.2 11.5 30.0 6.5 21.5 9.0 14.4 6.6
3/20-3/22 3/22-3/28 3/28-4/3 4/3-4/10 4/10-4/19 4/19-4/24 4/24-5/1 5/1-5/3 5/3-5/10 5/10-5/16 5/16-5/22 5/22-5/31 5/31-6/6 6/6-6/12 6/12-6/14 6/14-6/21 6/21-6/27 6/27-7/6	2 6 7 9 5 7 2 7 6 6 9 6 6 2 7 6 9	.012 .029 .038 .015 .040 .013 .024 .012 .015 .033 .018 .030 .023 .018 .010 .025 .019	6 15 19 8 22 8 14 7 9 20 9 17 13 11 6 15	1/2 5/6 5/6 6/7 8/9 4/5 6/7 1/2 6/7 5/6 8/9 5/6 1/2 6/7 5/6	3.0 12.5 15.8 6.9 19.6 6.4 12.0 3.5 7.7 16.7 7.5 15.1 10.8 9.2 3.0 12.9 9.2 17.8	100 47 114 54 103 64 74 44 81 27 98 81 107 81 53 87 42 49	3.0 26.6 13.9 12.7 19.0 10.0 16.2 8.0 9.5 61.7 7.7 18.7 10.1 11.3 5.7 14.8 21.8 36.3

# HARTFORD 003, 1978

SAMPLING PERIOD	# OF DAYS	PASSIVE WEIGHT (g)	PASSIVE	ORRECTION RATIO (N-1) : N)	CORRECTED PASSIVE µg/m <sup>3</sup>	ACTIVE HI-VOL	PASSIVE + HI-VOL
7/6-7/11 7/11-7/17 7/17-7/21 7/21-7/26 7/26-8/4 8/4-8/8 8/8-8/14 8/14-8/21 8/21-8/25 8/25-8/31 8/31-9/7 9/7-9/13 9/13-9/19 9/19-9/25 9/25-10/3	5 6 4 5 9 4 6 7 6 6 6 8	.018 .015 .017 .020 .028 .010 .018 .016 .013 .021 .046 .016 .008 .007	12 8 11 11 18 6 12 16 6 11 23 8 4 3 6	4/5 5/6 3/4 4/5 8/9 3/4 5/6 6/7 3/4 5/6 5/6 5/6 5/6	9.6 6.7 8.3 8.8 16.0 4.5 10.0 13.7 4.5 9.2 19.7 6.7 3.3 2.5 5.3	92 76 101 39 54 45 48 67 95 75 47 63 28 35 49	10.4 8.8 8.2 22.6 29.6 10.0 20.8 20.5 4.7 12.2 41.9 10.6 11.9 7.1
1/18/78-10/3/78 Avg. N =	5.98		Avg. (N-1)	= 4.98	Avg. % i	Passive =	15.69
10/6/77-10/3/78 Avg. N =	6.02		Avg. (N-1)	= 5.02	Avg. % I	Passive =	14.24
		<u>B</u>	ERLIN 001,	1978			
4/10/78-4/17/78 4/17-4/21 4/21-4/29 4/29-5/3 5/3-5/10 5/10-5/16 5/16-5/24 5/24-5/31 5/31-6/5 6/5-6/8 6/8-6/15 6/15-6/22 6/22-6/28 6/28-7/5 7/5-7/12 7/12-7/17 7/17-7/21 7/21-7/26 7/26-8/3 8/3-8/7 8/7-8/15 8/15-8/22 8/28-8/31 8/31-9/7	7484768753776775458487637	.006 .003 .006 .009 .003 .017 .020 .014 .012 .012 .013 .008 .010 .009 .005 .006 .011 .006 .010 .009 .012	3 2 4 5 3 0 1 1 8 7 7 7 7 5 6 5 3 3 6 3 5 5 6 6 3 3 4 3 4 3 4 3 4 3 4 3 4 3 4 3 4 3	6/7 3/4 7/8 3/4 6/7 5/6 7/8 6/7 4/5 6/7 6/7 4/5 3/4 4/5 3/4 7/8 6/7 5/6 3/4	2.6 1.5 3.8 2.6 3.6 9.6 9.6 4.7 4.3 5.4 4.5 4.4 4.3 5.6 5.6 2.6 4.3 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6 2.6	40 26 40 23 35 40 90 37 50 54 29 55 29 28 57 46 70 20 24 29 30 27 60 27 30	6.4 5.8 8.8 16.3 7.8 10.7 18.5 11.2 20.7 17.3 5.4 17.3 5.4 12.9 17.5 9.2 11.1 8.6

### BERLIN 001, 1978

SAMPLING PERIOD	# OF DAYS (N)	PASSIVE WEIGHT (g)	TOTAL PASSIVE µg/m <sup>3</sup>		CORRECTED PASSIVE µg/m <sup>3</sup>	ACTIVE HI-VOL	PASSIVE ÷ HI-VOL	
9/7-9/13 9/13-9/18 9/18-9/25 9/25-10/3 10/3-10/6 10/6-10/12 10/12-10/19 10/19-10/24 10/24-10/31 10/31-11/7 11/7-11/13 11/13-11/17 11/17-11/24 11/24-11/30 11/30-12/6 12/6-12/12 12/12-12/18 12/18-12/27 12/27/78-1/2/79	6 5 7 8 3 6 7 5 7 7 6 6 6 6 6 9 6	.006 .001 .003 .007 .002 .006 .002 .007 .004 .003 .008 .002 .004 .003 .002	3 <1 3 1 3 1 3 1 2 1 1 2 1 1 2	5/6 4/5 6/7 7/8 2/3 5/6 6/7 4/5 6/7 5/6 3/4 6/7 5/6 5/6 5/6 5/6	2.5 < 0.8 0.9 2.6 0.7 2.5 0.9 2.4 1.7 0.9 0.8 2.3 0.9 1.7 0.8 0.8 0.8	43 20 19 34 26 47 26 60 18 50 48 19 25 21 24 15 59 27	5.8 < 4.0 4.5 7.7 2.6 5.3 3.3 4.0 9.5 1.7 11.8 3.4 7.9 3.5 5.6 1.4 6.6 6.9	
4/10/78-1/2/79 Avg. N =	6.07		Av	g. N-1 = 5.07	Avg.	% Passive	= 8.70	
		BE	RLIN 001	, 1979	-			
1/2/79-1/4/79 1/4-1/10 1/10-1/16 1/16-1/23 1/23-1/31 1/31-2/7 2/7-2/13 2/13-2/15 2/15-2/22 2/22-3/1 3/1-3/8 3/8-3/13 3/13-3/19 3/19-3/26 3/26-3/30 3/30-4/4 4/4-4/10	2 6 7 8 7 6 2 7 7 7 5 6 7 4 5 6	.000 .004 .007 .000 .002 .012 .002 .003 .005 .005 .001 .000 .008 .005 .004 .002	0 2 3 0 1 5 1 2 2 <1 0 4 2 2 1 3	1/2 5/6 5/6 6/7 7/8 6/7 5/6 1/2 6/7 6/7 6/7 4/5 5/6 6/7 3/4 4/5 5/6	0.0 1.7 2.5 0.0 0.9 4.3 0.8 0.5 1.7 1.7 < 0.9 0.0 3.3 1.7 1.5 0.8 2.5	23 38 27 18 13 30 27 18 60 13 24 45 37 35 34 22	0.0 4.4 9.3 0.0 6.7 14.3 3.1 2.8 2.9 13.2 < 3.6 0.0 9.0 4.9 4.4 3.6 14.7	
4/10/78-4/10/79 Avg. N =	5.98		_	J. N-1 = 4.98	Avg.	% Passive	= 7.86	
WATERBURY 123, 1978								
4/12/78-4/17/78 4/17-4/24 4/24-5/1	5 - 10	.030	15 - 16	4/5 - 9/10	<b>554</b>	151	7.9	
5/1-5/3 5/3-5/9	2 6	.031	16 4 11 174	9/10 1/2 5/6	14.4 2.0 9.2	94 48 72	15.3 4.2 12.7	

# WATERBURY 123, 1978

SAMPLING PERIOD	# OF DAYS	PASSIVE WEIGHT (g)	TOTAL PASSIVE µg/m <sup>3</sup>	CORRECTION RATIO ((N-1) ÷ N)	CORRECTED PASSIVE  µg/m <sup>3</sup>	ACTIVE HI-VOL	PASSIVE + HI-VOL
5/9-5/15 5/15-5/22 5/22-5/30 5/30-6/2 6/2-6/8 6/8-6/14 6/14-6/20 6/20-6/26 6/26-7/3 7/3-7/10 7/10-7/17 7/17-7/20 7/20-7/26 7/26-8/2 8/2-8/8 8/8-8/14 8/14-8/21 8/21-8/29 8/29-9/1 9/12-9/18 9/18-9/26 9/26-10/2 10/2-10/6 10/6-10/12 10/12-10/19 10/12-10/19 10/12-10/19 10/12-10/19 10/12-10/19 10/12-10/19 10/12-10/19 10/12-10/19 10/12-10/19 11/6-11/13 11/13-11/17 11/17-11/27 11/27-11/29 11/29-12/5 12/11-12/18 12/11-12/18 12/18-12/26 12/26-12/29	678366667773676678356686467657740266783	.032 .023 .033 .022 .037 .020 .023 .023 .023 .014 .022 .013 .016 .016 .017 .018 .013 .015 .019 .012 .010 .004 .007 .011 .019 .012 .011 .019 .012 .011 .019 .012 .011	18 15 18 12 20 11 13 12 7 9 12 10 11 18 8 11 17 4 2 3 5 9 6 3 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5/6 6/7 7/8 5/6 5/6 5/6 5/6 5/6 6/7 5/6 5/6 5/6 5/6 5/6 5/7 5/6 6/7 5/6 7/8 3/10 5/6 6/7 5/8 5/8	15.0 12.9 15.8 8.0 16.7 9.2 10.8 10.3 6.0 10.3 6.7 7.5 10.3 6.7 8.3 13.7 9.3 4.7 5.4 9.2 7.5 2.4 4.3 7.5 9.3 2.7 2.3 2.7 2.3 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7 2.7	93 116 88 138 49 59 84 57 82 91 64 42 44 56 83 42 47 67 54 43 52 91 64 43 59 81 64 43 64 64 64 64 64 64 64 64 64 64 64 64 64	16.1 17.9 34.0 15.9 19.0 12.5 17.1 11.7 24.5 14.9 11.0 13.9 4.1 11.0 13.9 4.1 14.1 14.1 14.1 15.1 14.1 15.1 14.1 15.1 16.3 16.3 17.1 17.1 17.1 17.1 17.1 17.1 17.1 17
4/12/78-12/29/78 Avg. N =	5.98		Avg. N-	-1 = 4.98	Avg. %	Passive =	10.97
WATERBURY 123, 1979							
12/29/78-1/4/79 1/4-1/11 1/11-1/16 1/16-1/22	6 7 5 6	.030 .055 .035 .021	13 25 15 9	5/6 6/7 4/5 5/6	10.8 21.4 12.0 7.5	152 174 127 33	7.1 12.3 9.4 22.7

TABLE 34 (continued)

### WATERBURY 123, 1979

SAMPLING PERIOD	# OF DAYS	PASSIVE WEIGHT (g)	TOTAL PASSIVE µg/m <sup>3</sup>	CORRECTION RATIO ((N-1) + N)	CORRECTED PASSIVE µg/m <sup>3</sup>	ACTIVE HI-VOL	PASSIVE + HI-VOL
1/22-1/29	7	.024	11	6/7	9.4	87	10.8
1/29-2/4	6	.054	23	5/6	19.2	48	39.9
2/4-2/9	5	.029	13	4/5	10.4	78	13.3
2/9-2/15	6	.030	13	5/6	10.8	74 74	14.6
2/15-2/21	6	.028	12	5/6	10.0	146	6.8
2/21-3/2	9	.063	28	8/9	24.9	44	56.6
3/2-3/5	3	.003	1	2/3	0.7	35	1.9
3/5-3/12	7	.017	8	6/7	6.9	95	7.2
3/12-3/19	7	.044	20	6/7	17.1	117	14.7
3/19-3/26		=		=			* 1 0 7
3/26-3/29	3	.014	6	2/3	4.0	62	6.5
3/29-4/4	=	-	not .			-	-
4/4-4/10	6	.017	7	5/6	5.8	28	20.8
4/10-4/16	6	.017	7	5/6	5.8	31	18.8
4/12/78-4/16/79							
Avg. N =	5.97		Avg. 1	N-1 = 4.97	Avg.	% Passive	= 12.46

#### E. PUBLICATIONS

The following is a partial listing of technical papers and study reports dealing with various aspects of Connecticut air pollutant levels and air quality data.

- 1. Bruckman, L., <u>Asbestos: An Evaluation of Its Environmental Impact in Connecticut</u>, internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, March 12, 1976.
- 2. Lepow, M.L., L. Bruckman, R.A. Rubino, S. Markowitz, M. Gillette and J. Kapish, "Role of Airborne Lead in Increased Body Burden of Lead in Hartford Children," Environ. Health Perspect., May, 1974, pp. 99-102.
- 3. Bruckman, L. and R.A. Rubino, "Rationale Behind a Proposed Asbestos Air Quality Standard," paper presented at the 67th Annual Meeting of the Air Pollution Control Association, Denver, Colorado, June 9-11, 1974, J. Air Pollut. Cntr. Assoc., 25: 1207-15 (1975).
- 4. Rubino, R.A., L. Bruckman and J. Magyar, "Ozone Transport," paper presented at the 68th Annual Meeting of the Air Pollution Control Association, Boston, Massachusetts, June 15-20, 1975, J. Air Pollut. Cntr. Assoc., 26: 972-5 (1976).
- 5. Bruckman, L., R.A. Rubino and T. Helfgott, "Rationale Behind a Proposed Cadmium Air Quality Standard," paper presented at the 68th Annual Meeting of the Air Pollution Control Association, Boston, Massachusetts, June 15-20, 1975.
- 6. Rubino, R.A., L. Bruckman, A. Kramar, W. Keever and P. Sullivan, "Population Density and Its Relationship to Airborne Pollutant Concentrations and Lung Cancer Incidence in Connecticut," paper presented at the 68th Annual Meeting of the Air Pollution Control Association, Boston, Massachusetts, June 15-20, 1975.
- 7. Lepow, M.L., L. Bruckman, M. Gillette, R.A. Rubino and J. Kapish, "Investigations into Sources of Lead in the Environment of Urban Children," Environ. Res., 10: 415-26 (1975).
- 8. Bruckman, L., E. Hyne and P. Norton, "A Low Volume Particulate Ambient Air Sampler," paper presented at the APCA Specialty Conference entitled "Measurement Accuracy as it Relates to Regulation Compliance," New Orleans, Louisiana, October 26-28, 1975, APCA publication SP-16, Air Pollution Control Association, Pittsburgh, Pennsylvania, 1976.
- 9. Bruckman, L. and R.A. Rubino, "High Volume Sampling Errors Incurred During Passive Sample Exposure Periods," J. Air Pollut. Cntr. Assoc., 26: 881-3 (1976).
- 10. Bruckman, L., R.A. Rubino and B. Christine, "Asbestos and Mesothelioma Incidence in Connecticut," J. Air Pollut. Cntr. Assoc., <u>27</u>: 121-6 (1977).

- 11. Bruckman, L., <u>Suspended Particulate Transport in Connecticut: An Investigation Into the Relationship Between TSP Concentrations and Wind Direction in Connecticut, internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, December 24, 1976.</u>
- 12. Bruckman, L. and R.A. Rubino, "Monitored Asbestos Concentrations in Connecticut", paper presented at the 70th Annual Meeting of the Air Pollution Control Association, Toronto, Ontario, June 20-24, 1977.
- 13. Bruckman, L., "Suspended Particulate Transport", paper presented at the 70th Annual Meeting of the Air Pollution Control Association, Toronto, Ontario, June 20-24, 1977.
- 14. Bruckman, L., "A Study of Airborne Asbestos Fibers in Connecticut," paper presented at the "Workshop on Asbestos: Definitions and Measurement Methods" sponsored by the National Bureau of Standards/U.S. Department of Commerce, July 18-20, 1977.
- 15. Bruckman, L., "Monitored Asbestos Concentrations Indoors," paper presented at The Fourth Joint Conference of Sensing Environmental Pollutants, New Orleans, Louisiana, November 6-11, 1977.
- 16. Bruckman, L. "Suspended Particulate Transport: Investigation into the Causes of Elevated TSP Concentrations Prevalent Across Connecticut During Periods of SW Wind Flow," paper presented at the Joint Conference on Applications of Air Pollution Meteorology, Salt Lake City, Utah, November 28 December 2, 1977.
- 17. Bruckman, L., E. Hyne, W. Keever, "A Comparison of Low Volume and High Volume Particulate Sampling," internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, 1976.
- 18. "Data Validation and Monitoring Site Review", (part of the Air Quality Maintenance Planning Process), internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, June 15, 1976.
- 19. "Air Quality Data Analysis", (part of the Air Quality Maintenance Planning Process), internal report issued by the Connecticut Department of Environmental Protection, Hartford, Connecticut, August 16, 1976.
- 20. Bruckman, L., "Investigation into the Causes of Elevated SO<sub>2</sub> Concentrations Prevalent Across Connecticut During Periods of SW Wind Flow," paper presented at the 71st Annual Meeting of the Air Pollution Control Association, Paper #78-16.4, Houston, Texas, June 25-29, 1978.
- 21. Anderson, M.K., "Power Plant Impact on Ambient Air: Coal vs. Oil Combustion," paper presented at the 68th Annual Meeting of the Air Pollution Control Association, Paper #75-33.5, Boston, MA, June 15-20, 1975.

- 22. Anderson, M.K., G.D. Wight, "New Source Review: An Ambient Assessment Technique," paper presented at the 71st Annual Meeting of the Air Pollution Control Association, Paper #78-2.4, Houston, TX, June 25-29, 1978.
- 23. Wolff, G.T., P.J. Lioy, G.D. Wight, R.E. Pasceri, "Aerial Investigation of the Ozone Plume Phenomenon," J. Air Pollut. Control Assoc., <u>27</u>: 460-3 (1977).
- 24. Wolff, G.T., P.J. Lioy, R.E. Meyers, R.T. Cederall, G.D. Wight, R.E. Pasceri, R.S. Taylor, "Anatomy of Two Ozone Transport Episodes in the Washington, D.C., to Boston, Mass., Corridor," Environ. Sci. Technol., 11:506-10 (1977).
- 25. Wolff, G.T., P.J. Lioy, G.D. Wight, R.E. Meyers, and R.T. Cederwall, "Transport of ozone associated with an air mass," In: Proceed. 70 Annual Meeting APCA, Paper #77-20.3, Toronto, Canada, June, 1977.
- 26. Wight, G.D., G.T. Wolff, P.J. Lioy, R.E. Meyers, and R.T. Cederwall, "Formation and transport of ozone in the Northeast Quadrant of the U.S.," In: Proceed. ASTM Sym. Air Quality and Atmos. Ozone, Boulder, Colo., Aug. 1977.
- 27. Wolff, G.T., P.J. Lioy, and G.D. Wight, "An overview of the current ozone problem in the Northeastern and Midwestern U.S.," In: Proceed. Mid-Atlantic States APCA Conf. on Hydrocarbon Control Feasibility, p. 98, New York, N.Y., April 1977.
- 28. Wolff, G.T., P.J. Lioy, G.D. Wight, R.E. Meyers, and R.T. Cederwall, "An investigation of long-range transport of ozone across the Midwestern and Eastern U.S.," Atmos. Environ. 11:797 (1977).